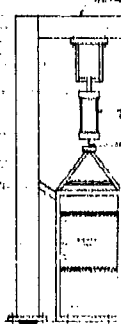
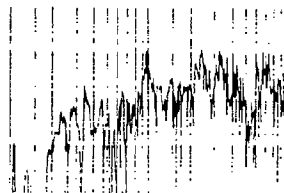
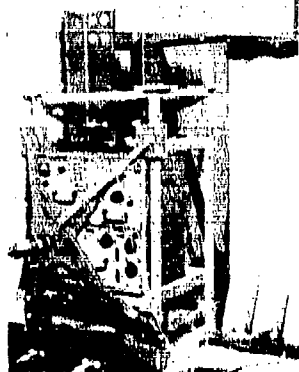




US Army Corps
of Engineers



AD-A162 421



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TECHNICAL REPORT SL-85 6

FORCE-PULSE TESTS OF TACTICAL COMMUNICATION EQUIPMENT

by

Roger D. Crowson

Structures Laboratory

DEPARTMENT OF THE ARMY
Waterways Experiment Station, Corps of Engineers
PO Box 631, Vicksburg, Mississippi 39180-0631

and

Frederick Safford

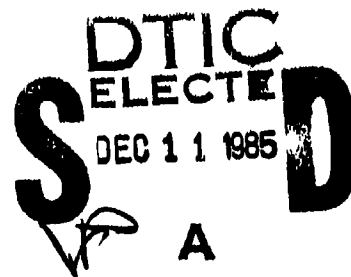
Agbabian Associates
250 North Nash Street
El Segundo, California 90245



September 1985

Final Report

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PREFACE

This data report covers developmental work on the force-pulse generator and all pulse tests on the communication equipment through December 1980. Calibration test data have been previously reported. Overall program management for the sponsors was provided by Dr. William Schuman, U. S. Army Ballistic Research Laboratory, and Mr. Robert Freiberg, U. S. Army Electronics Research and Development Command. Project Engineers were Dr. Frederick Safford, Agabian Associates, and Mr. Roger D. Crowson, Structural Mechanics Division (SMD), Structures Laboratory (SL), U. S. Army Engineer Waterways Experiment Station (WES). Instrumentation support was provided and data processing was performed by Messrs. James L. Pickens and Cary B. Cox, Instrumentation Services Division, WES.

Commanders and Directors of WES during the work and preparation of this report were COL Nelson P. Conover, CE, COL Tilford C. Creel, CE, and COL Robert C. Lee, CE; Mr. F. R. Brown was Technical Director, Mr. Bryant Mather was Chief, SL. At the time of publication of this report, COL Allen F. Grum, USA, was Director of WES and Dr. Robert W. Whalin was Technical Director.



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CONVERSION FACTORS, NON-SI TO SI (METRIC)
UNITS OF MEASUREMENT

Non-SI units of measurement used in this report can be converted to SI (metric) units as follows:

<u>Multiply</u>	<u>By</u>	<u>To Obtain</u>
acceleration of gravity (g's)	9.80665	metres per second squared
cubic feet	0.02831685	cubic metres
cubic inches	16.387064	cubic centimetres
feet	0.3048	metres
g's per pound (force)	2.20462243	metres per second squared per newton
gallons (U. S. liquid)	0.00378541	cubic metres
gallons (U. S. liquid) per minute	0.00006309	cubic metres per second
horsepower (electric)	746.0	watts
inches	2.54	centimetres
inches	0.0254	metres
inches per second	0.0254	metres per second
kips (1000 lb force)	4448.222	newtons
ounces (mass)	28.34952	grams
pounds (force) per square inch	6894.757	pascals
square inches	6.4516	square centimetres
tons (2000 lb mass)	907.18474	kilograms

FORCE-PULSE TESTS OF TACTICAL COMMUNICATION EQUIPMENT

PART I: INTRODUCTION

BACKGROUND

1. Mobile tactical communication systems used by the U. S. Army are housed in a shelter typically mounted on a 2-1/2-ton* truck. Air-blast generated by high-explosive or nuclear weapons loads the shelter, thereby inducing transient vibrations to the communication equipment. Shelters containing the equipment have been tested in Events DICE THROW and MISERS BLUFF, and the shelters were scheduled to be part of the MILL RACE Event during 1981. Acceleration of various individual pieces of equipment as well as the equipment racks are typically measured in the field events.

2. The transient loadings and resulting motion of the equipment, as measured in the field events, are quite severe. However, due to the nature of the tests, it has not been possible to determine operational characteristics of the equipment before, during, and after the tests. A laboratory simulation device capable of generating specified force-time histories could be used to subject individual pieces of equipment to similar motions as measured in the actual field events. Such laboratory testing would be highly desirable in terms of cost-effectiveness and data obtainable and could be used to determine the vulnerability/survivability of the different classes of equipment. A program was initiated to develop such a simulation device and subject various components of the communication system to loadings as might be encountered in a battlefield environment. Program management is being provided by the U. S. Army Electronics Research and Development Command (ERADCOM) and the U. S. Army Ballistic Research Laboratory (BRL). The simulation system is being developed and implemented jointly by the U. S. Army Engineer Waterways Experiment Station (WES) and Agbabian Associates (AA).

* A table of factors for converting non-SI units of measurement to SI (metric) units is presented on page 3.

SCOPE

3. The simulation device, or force-pulse generator, is hydraulically driven. This report covers the design of the hydraulic power supply and discusses tests conducted on the communication equipment through December 1980. Design and operation of the pulse generator were previously described in the test plan (Reference 1), and calibration tests were reported in Reference 2.

PART II: HYDRAULIC POWER SUPPLY

4. The existing WES pulse-generator was powered by a hydraulic system using an air reservoir and air/hydraulic multiplier. This system is shown in Figure 1 and a schematic in Figure 2. The new system, consisting of two separate pulse generators and having a larger force capacity, would require a new power supply. Based on requirements of two pulsers each having a nominal 10,000-lbf capacity and a 13-in. stroke, a power system utilizing the air/hydraulic concept would have required: (a) a 14-in. to 3-in. air/hydraulic multiplier with a 20-in. stroke, (b) a 94-gal air reservoir, and (c) an input supply of 100 psi. Such a system would have been considerably larger than the existing system thereby greatly reducing the degree of portability. Due to size and operational characteristics, an alternative to the air/hydraulic multiplier concept was developed.

5. A power supply concept, utilizing a high-pressure pump and accumulator system, is shown schematically in Figure 3. Preliminary calculations, used for initial sizing of components, were made as follows:

Hydraulic cylinders:

10,000-lbf nominal design force
2500-psi operating pressure

$$\begin{aligned}\text{Net area required} &= \frac{10,000 \text{ lb}}{2500 \text{ lb/in.}^2} \\ &= 4.0 \text{ in.}^2\end{aligned}$$

A 2-1/2-in. piston with 1-in. rod has a net effective area of 4.124 in.²

Cylinder volume:

$$(4.124 \text{ in.}^2)(13\text{-in. stroke}) = 53.6 \text{ in.}^3$$

Piston velocity: 120 in./sec (nominal)

Flow rate:

Single cylinder = 128.5 gal/min
Two cylinders = 257 gal/min



Figure 1. Initial WES pulser utilizing air/hydraulic multiplier in power supply.

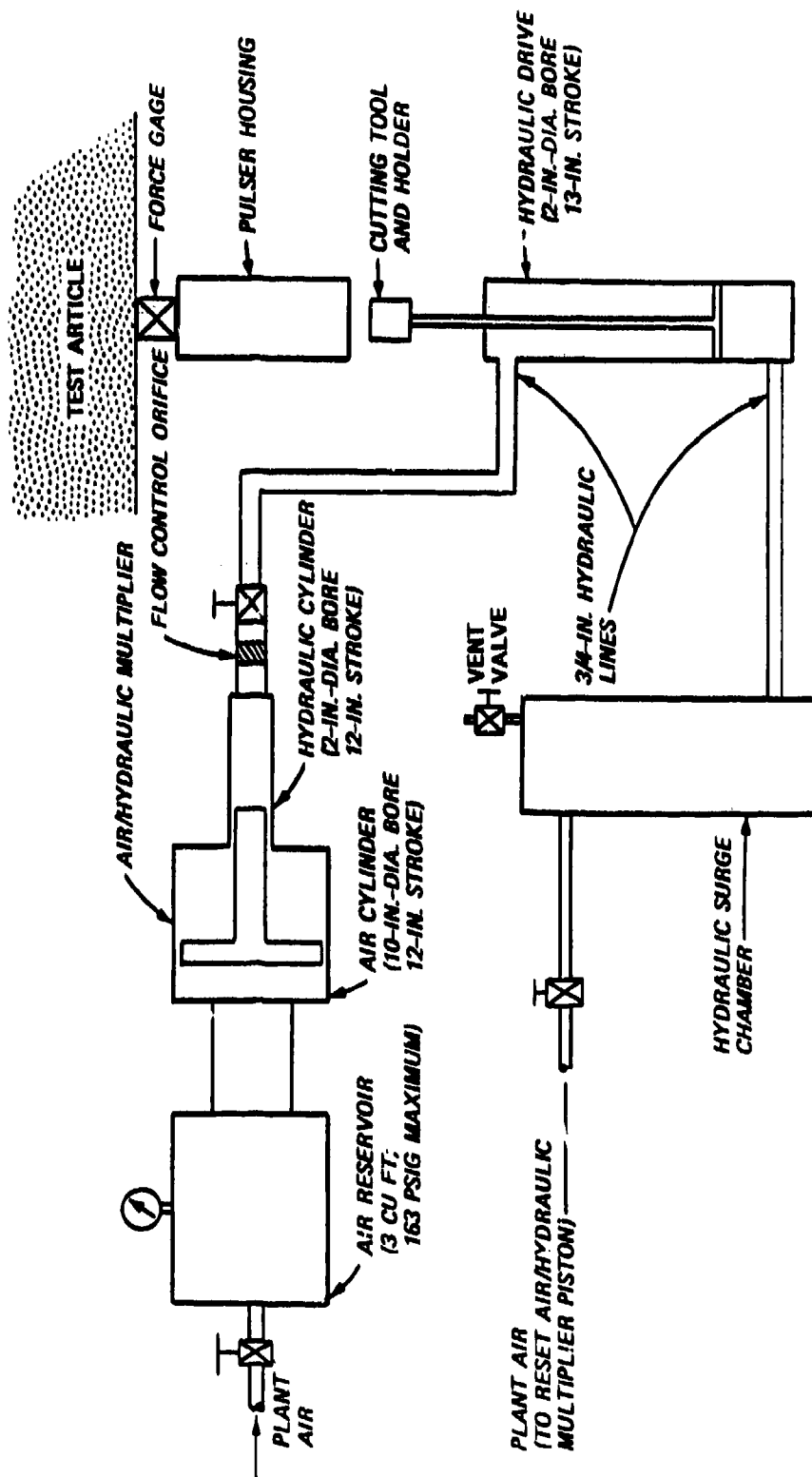


Figure 2. Schematic of initial WES pulser.

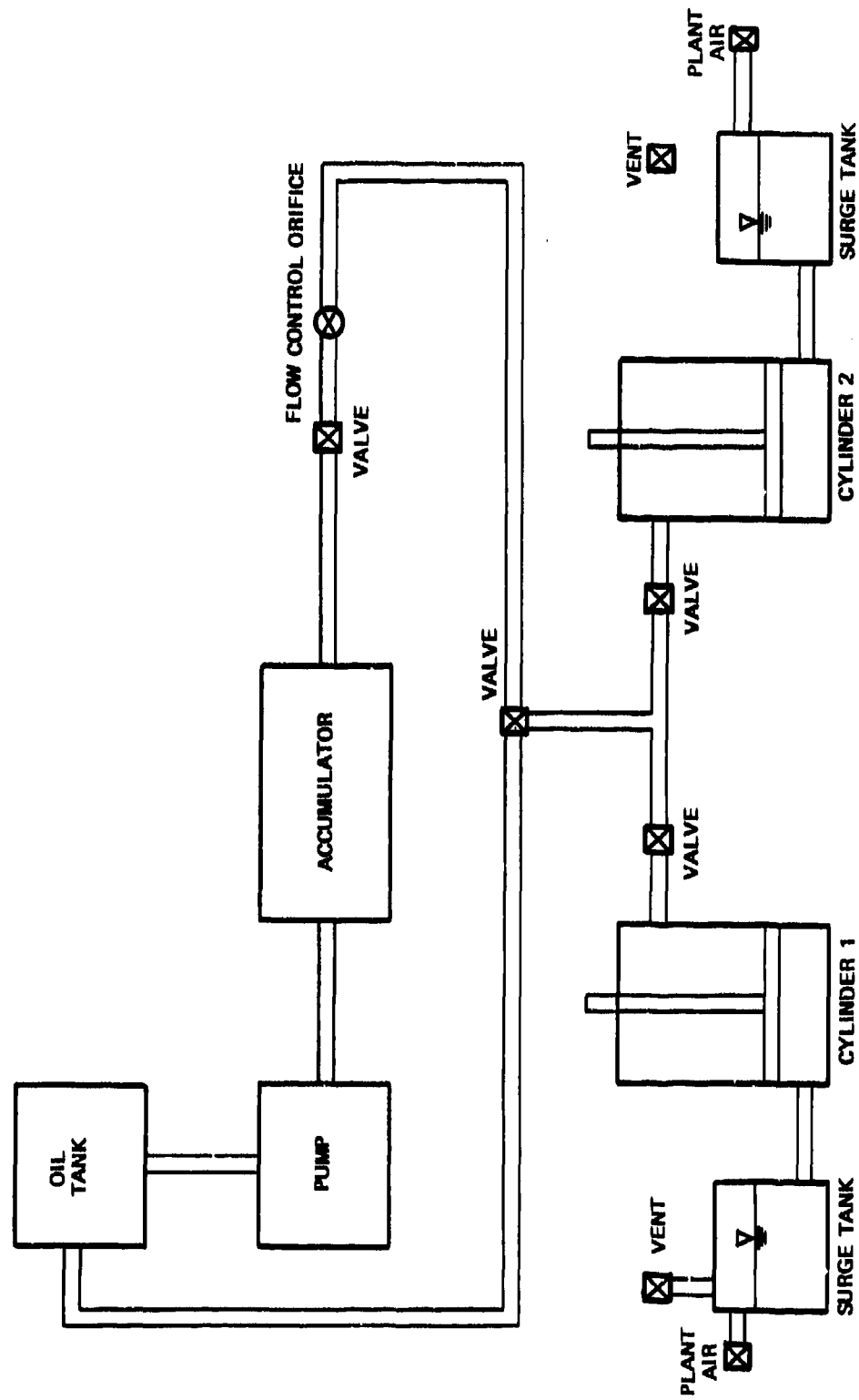


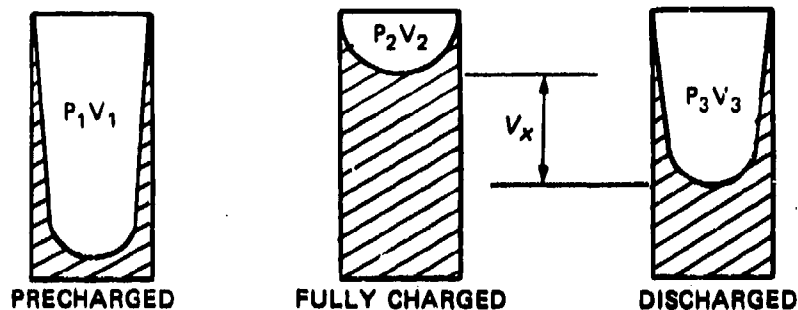
Figure 3. Hydraulic power supply schematic.

6. Gas-oil type accumulators operate on the principle of Boyle's Gas Law, $P_1 V_1^n = P_2 V_2^n$, where P_1 and P_2 are the initial and final gas pressures; V_1 and V_2 are the corresponding gas volumes; and n is the ratio between the specific heat of a gas at constant volume and its specific heat at constant pressure. For an isothermal condition (constant temperature) $n = 1.0$, and for an adiabatic condition (no heat transfer), $n = 1.4$. Generally, an adiabatic condition exists for rapid (less than 1 minute) expansion or compression of gas or when insulating materials are used in the accumulator. For sizing an accumulator as an auxiliary power source, the amount of fluid required from the accumulator to meet the system needs must be known. The following formula presents a simplified method of determining the capacity of the accumulator to be used (Reference 3, p. a-82):

$$V_1 = \frac{V_x \left(\frac{P_3}{P_1} \right)^{1/n}}{1 - \left(\frac{P_3}{P_2} \right)^{1/n}} \quad (1)$$

where:

- V_1 = size of accumulator necessary, in.³ Maximum volume occupied by gas at precharge pressure
- V_x = volume of fluid discharged from accumulator, in.³ Additional volume of fluid demanded by the system
- P_1 = gas precharge of accumulator, psi. Must be less than or equal to minimum system pressure, P_3
- P_2 = maximum system design operating pressure, psi
- V_2 = compressed volume of gas at maximum system pressure, in.³
- P_3 = minimum system pressure at which additional volume of fluid is needed, psi
- V_3 = expended volume of gas at minimum system pressure, in.³
- $n = 1.4$



The maximum precharge pressure, P_1 , was limited to that of a standard nitrogen bottle (2200 psi); considering the volume of two cylinders, V_x was taken to be 130 in.³; the required pressure for 10,000 lbf, P_2 , was taken to be

$$\frac{10,000 \text{ lbf}}{4.124 \text{ in.}^2} = 2424 \text{ psi}$$

and the minimum system pressure, P_3 , was assumed to be 2100 psi. Using these parameters, Equation 1 resulted in a required accumulator volume of approximately 1400 in.³. A 10-gallon accumulator having a volume of 2080 in.³ was selected as optimum.

7. The final system design is shown schematically in Figure 4, and a list of components is given in Table 1. Final sizing and selection of components and fabrication of the complete power supply was performed by Activation Inc. under contract to WES. A photograph of the completed power supply is shown in Figure 5.

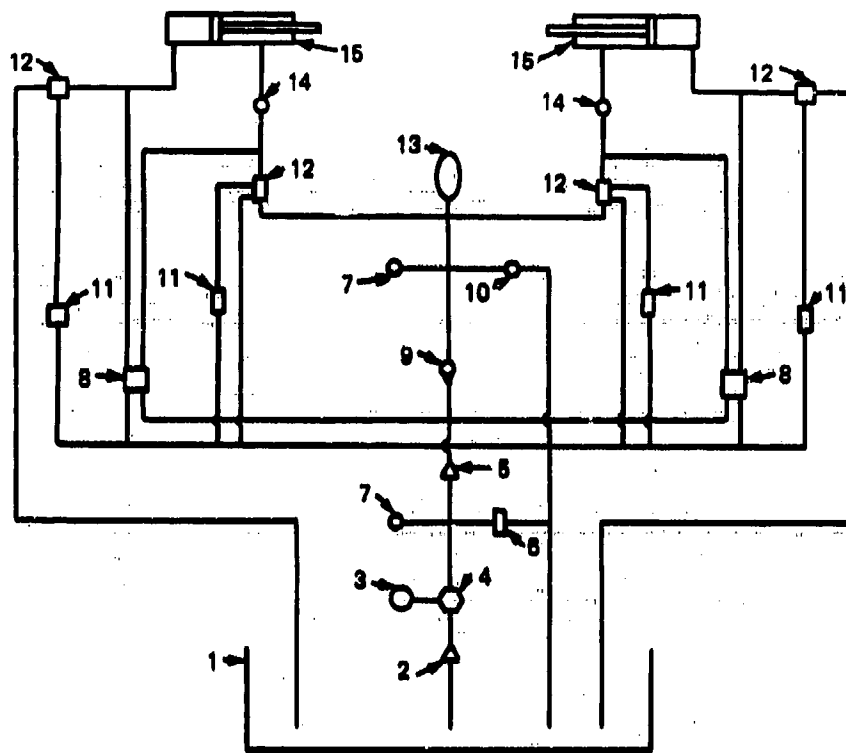


Figure 4. Hydraulic power supply circuit.

Table 1
Hydraulic Power Supply Component List

ITEM	QTY	DESCRIPTION	ITEM	QTY	DESCRIPTION
1	1	Thirty-gallon reservoir with cover, sight gage, flush drain, and baffles, Activation No. T30L	9	1	Check valve, Gould No. DC 500
2	1	Suction strainer, MFF No. SR45	10	1	Bull valve, Clayton Mark No. 1/2 CSB-790
3	1	Electric motor, 3HP, Lincoln No. 182T	11	4	Directional control valve, 4-way, 2-position, solenoid-operated, Double A No. QJ-005-C-10B1
4	1	Pressure compensated pump, Hydura No. PVQ-06-LSAY-CNBN	12	4	Relief valve, Double A No. BT-12-12A2
5	1	High-pressure filter, 5 micron, MFF No. MF1-1-008	13	1	Ten-gallon accumulator, Graser No. 30A-10A
6	1	Relief valve, Sun No. RPOC-JAN-CEN	14	2	Flow control valve, Double A No. YB12-10A1
7	2	Pressure gage, 0-3000 psi, UCC No. UC-3907	15	2	Hydraulic cylinder, 2-1/2-in. bore, 1-in. rod diameter, 13-in. stroke, Shaeffer Heavy Duty MH Series Model No. 2-1/2 HHRF13CRA
8	2	Directional control valve, 4-way, 3-position, solenoid-operated, Double A No. QJ-01-C-10F1			

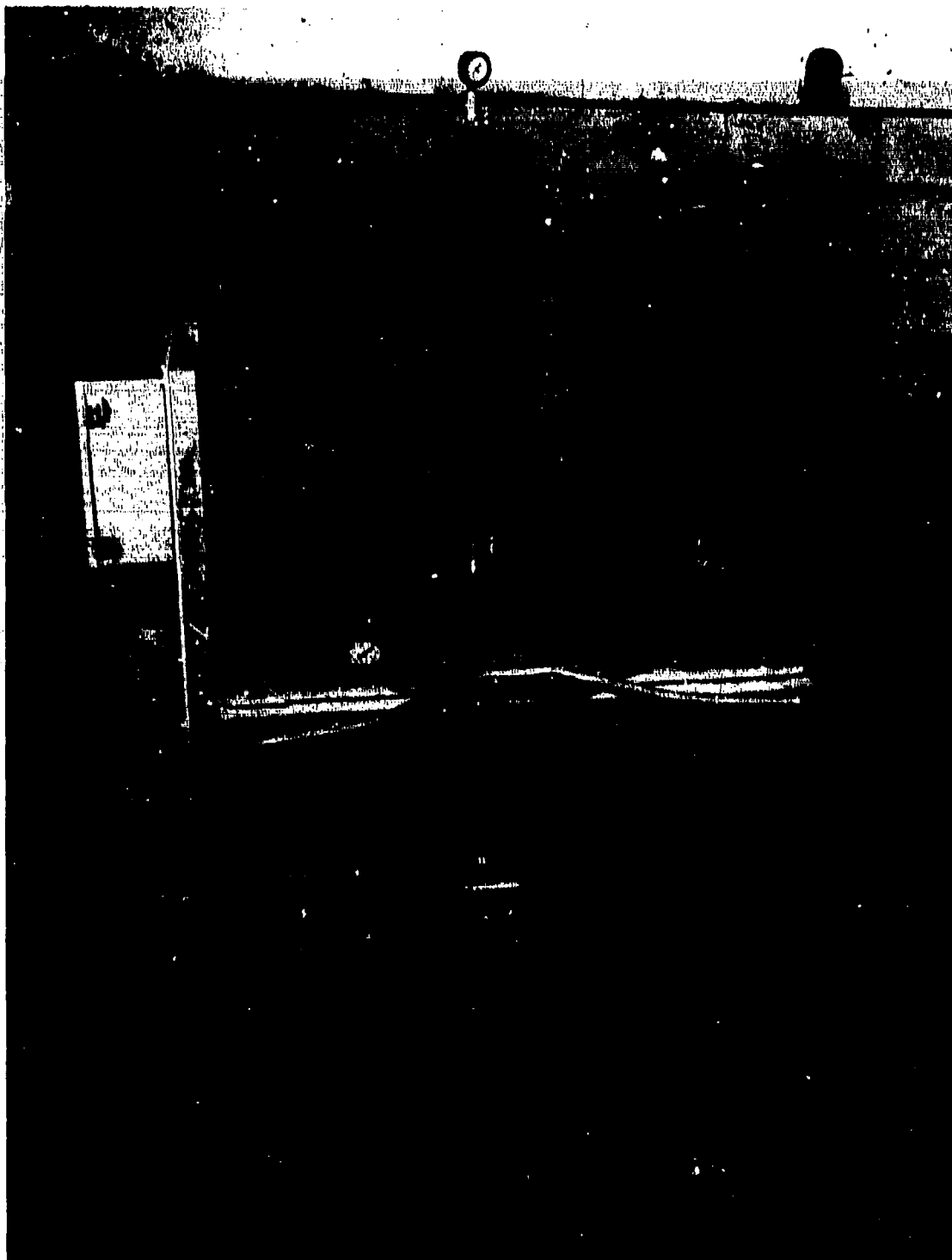


Figure 5. Hydraulic power supply.

PART III: TESTS CONDUCTED

CALIBRATION TESTS

8. An extensive series of calibration tests was conducted, and results are reported in Reference 2.

EQUIPMENT TEST SETUP

9. The equipment rack used in the mobile system and furnished to WES was modified for testing. The rack, constructed of 1-in. aluminum box tubing and 3/16-in. aluminum plate, was reduced in height to approximately 3 ft so that the total height of the system with vertical pulser attached would be less than 8 ft. To accommodate the largest pieces of radio equipment, maximum shelf spacing was not altered in the modified rack. Steel reaction structures to which the pulsers were attached were designed and fabricated. For attaching the pulsers to the equipment rack, a loading yoke ("quadrapod") arrangement was utilized. The loading yoke was fabricated from 3/4-in. steel box tubing and attached to the rack with three 3/8-in. bolts at four locations. The test setup is shown schematically in Figure 6 and as a photograph in Figure 7.

INSTRUMENTATION

10. Accelerations were measured with piezoresistive shock accelerometers (Endevco Model 2264A). These are small gages (0.05 oz weight) having a high resonance frequency (30,000 Hz) and essentially zero damping thereby allowing accurate response to fast-rise-time, short-duration shock motion. Complete specifications are given in Table 2. The accelerometers were attached directly to the equipment with cyanoacrylate adhesive.

11. Force measurements were made with piezoelectric force links (Kistler Model 936A) having a crystalline quartz sensing element. These transducers have a high natural frequency (25,000 Hz), high resolution (0.0004 percent), and very high sensitivity. Complete specifications are given in Table 2.

12. All data were recorded on an FM magnetic tape recorder and played back through a tuneable analog filter on oscillograph traces. Some data were also digitized for additional analysis. The tape

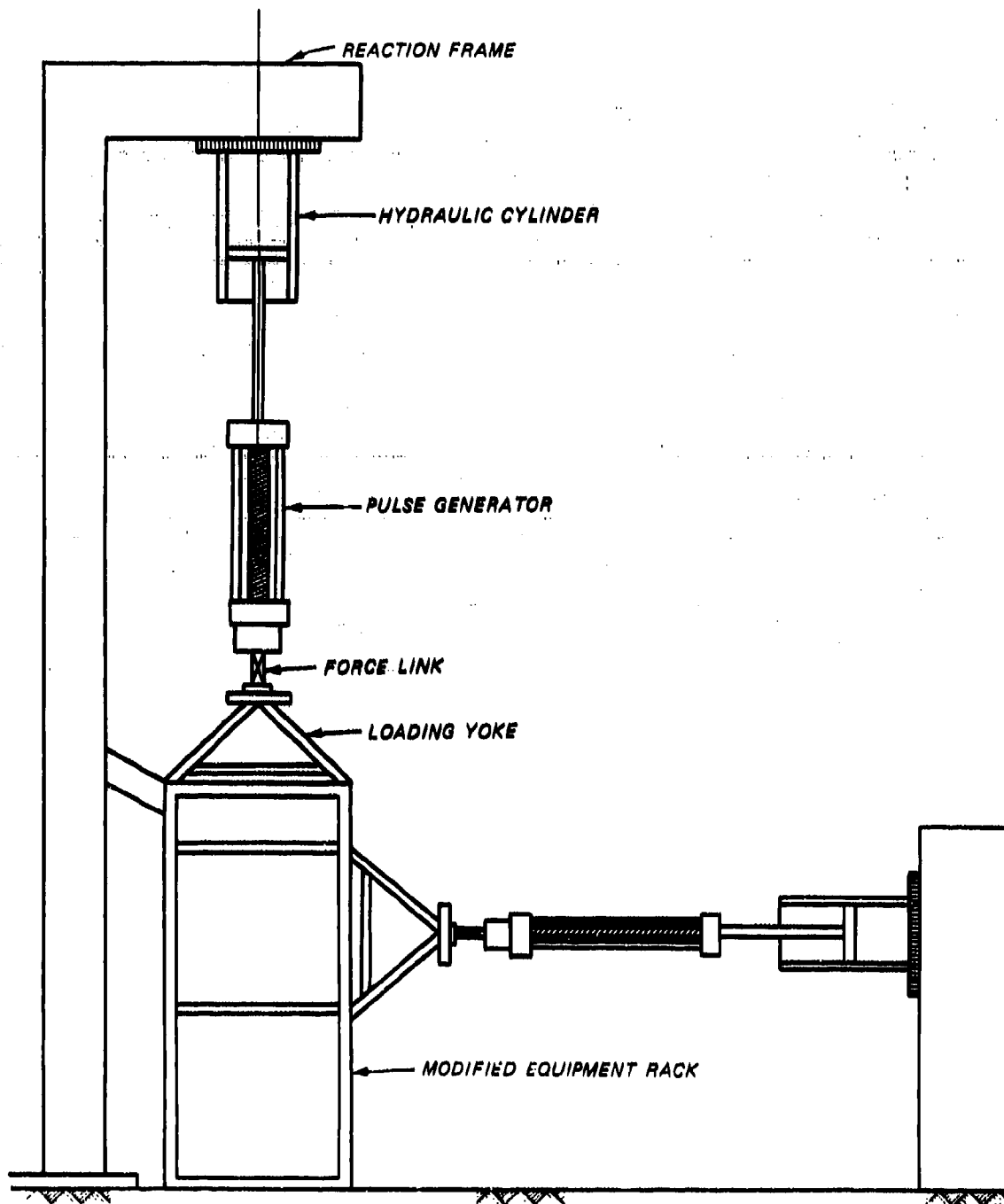


Figure 6. Schematic of biaxial test facility.



Figure 7. Setup for biaxial tests.

Table 2
Transducer Specifications

Endevco 2264A Accelerometer

Range, g's pk	±2000
Sensitivity, mV/g at 10 Vdc, nom.	0.250
Mounted resonance frequency, Hz	30,000
Useful frequency response, Hz, dc to	5000
Environmental acceleration limit, g's pk	±5000
Damping factor, nom	0.002
Transverse sensitivity	5%, max
Weight, oz	0.05

Kistler 936A Quartz Force Link

Range, lb, tension	15,000
compression	25,000
Resolution, lb	0.1
Resonant frequency, Hz, unmounted	25,000
Weight, oz	50
Sensitivity	10 pC/lb
Overload capacity	10%
Linearity	1%
Useful frequency response, Hz, near dc to	5000
Environmental acceleration limit, g's pk	±5000
Rise time	20 µsec

machines were operated at 30 ips, wide band, thereby having a frequency response from DC to 20 kHz (half-power point response).

BIAXIAL TESTS

13. After completion of the calibration test phase, a series of tests was conducted utilizing the biaxial capability of the pulser. As shown in Figure 7, both horizontal and vertical axes were excited. However, in lieu of an actual piece of communications equipment, lead weights were placed in the rack for the initial biaxial tests. No specific pulse train was used for these tests; arbitrary excitation was sufficient to check out the system. For these biaxial tests, both vertical and horizontal accelerations of the equipment rack were measured.

14. The two circuits in the hydraulic power supply have different response times. Delays of up to 30 msec are within specifications of the solenoid-controlled valves in the power supply. Thus, if both pulsers are simultaneously fired with a common circuit, one will start moving 10 to 30 msec before the other. For simultaneous initiation of both pulses (i.e., each cutter striking its first nubbin at the same point in time), it is necessary to position one cutter closer to the first nubbin than the other. After several test firings of both pulsers, simultaneous initiation of the first pulse was achieved with the following parameters:

Precharge accumulator pressure	= 1250 psi
System operating pressure	= 2000 psi
Flow control valve (vertical unit)	= 4-1/2 turns
Flow control valve (horizontal unit)	= 6-1/2 turns
Horizontal cutter initial run-up	= 7.5 mm
Vertical cutter initial run-up	= 5.1 mm

However, after repeated firing with the same parameters, initiation of pulses between the two units could be controlled to within only 7 msec. Typical data records from biaxial tests, produced directly from the tape recorder with no additional filtering, are shown in Figures 8 and 9. As can be seen in Figure 9, significant accelerations were recorded on the rack (800 g's both vertical and horizontal directions) with relatively moderate input forces (approximately 2000 lb). No significant problems

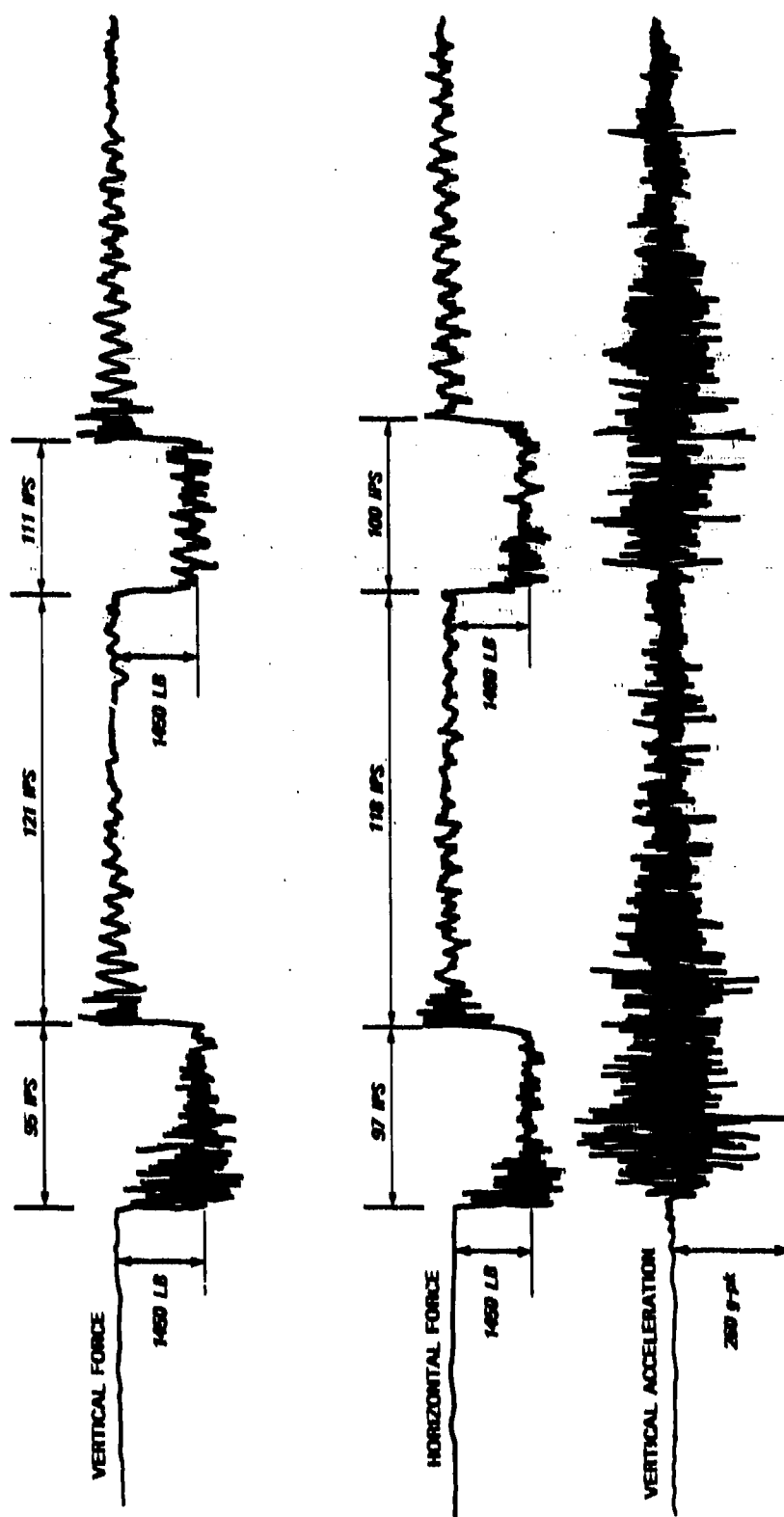


Figure 8. Biaxial pulse test data, simultaneous pulse initiation.

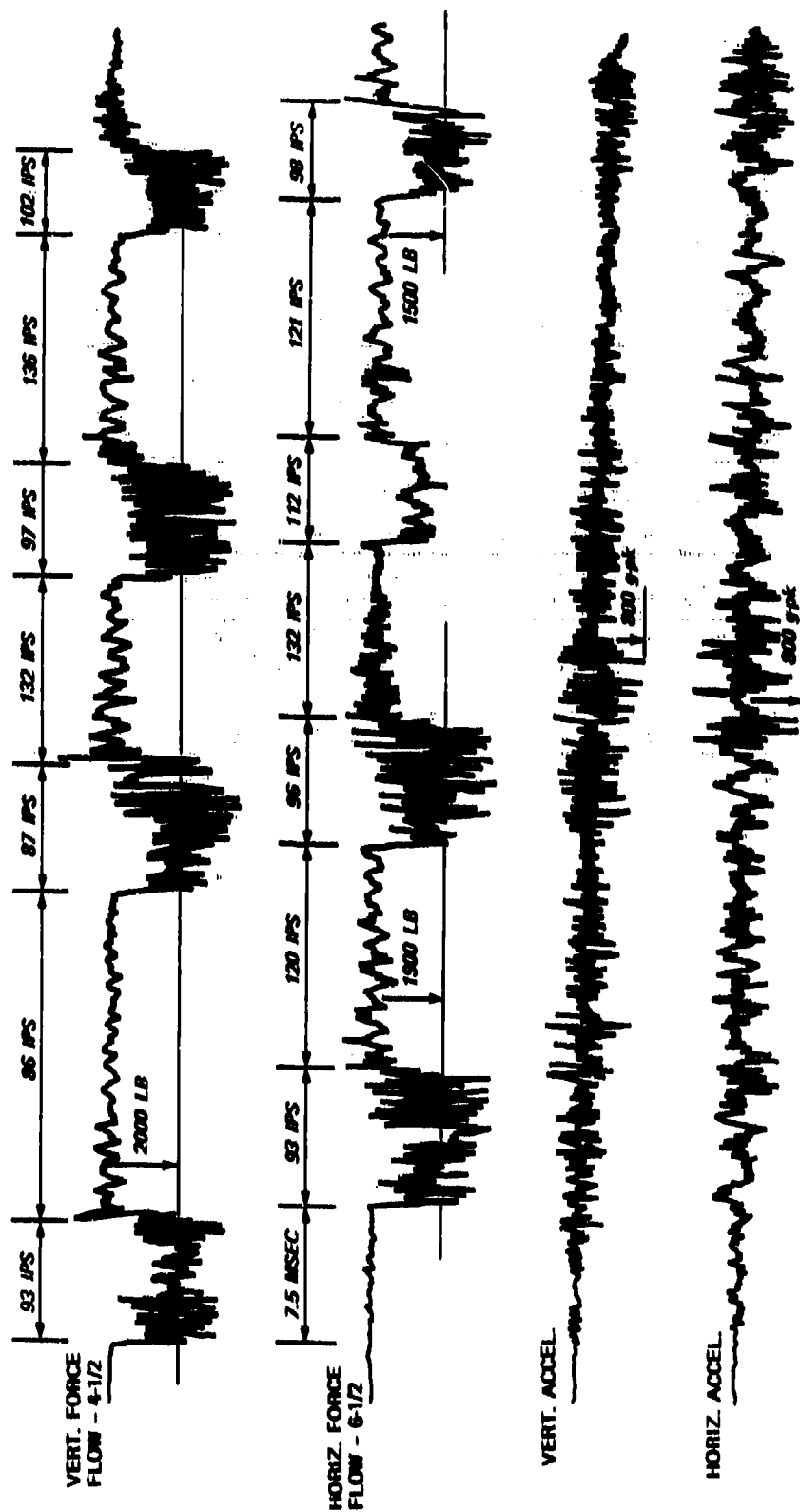


Figure 9. Biaxial pulse test data, delayed pulse initiation.

were encountered while operating the system in the biaxial mode, other than maintaining alignment, which is a critical inherent characteristic of the system.

IMPEDANCE TESTS

15. Two sets of impedance tests were run. The first set, as specified in the original test plan (Reference 1), was conducted using a hammer to produce a force impulse. Data from these tests were to be used in deriving a pulse train to simulate field test response records. The other set of impedance tests was conducted using vibration sine sweeps. Frequency response data of the radio equipment and rack were obtained from these vibration tests. All impedance tests were conducted with the rack hard-mounted to the floor and reaction structure.

16. Hammer tests. The system configurations shown in Figures 10 and 11 were utilized for the hammer impedance tests. Force impulses, induced by a calibrated hammer having a force link attached to its head, excited the system, and the resulting accelerations were measured in both horizontal and vertical directions. Figure 10 shows the arrangement for the vertical impedance test. Horizontal testing was also performed with the vertical pulser attached and the input being applied horizontally. Source impedance measurements were made, as shown in Figure 11, by exciting the pulse generators directly (pulse generators disconnected from equipment rack) and measuring the drive point acceleration. A nonoperational AN/GRC-103 radio system was mounted in the rack for all the impedance tests. The data were recorded on FM magnetic tape and later digitized. The digital records were forwarded to Agbabian Associates for analysis and use in the pulse optimization algorithms.

17. Vibration tests. Once the degree of acceleration attenuation from equipment rack to radio had been observed, vibration tests were conducted. Frequency response data of both the equipment rack and AN/GRC-103 radio were obtained from these tests. The pulsers were disconnected from the rack, and an electromagnetic vibrator was attached to the horizontal loading yoke (Figure 12). Frequency sweep tests from 100 to 10,000 Hz were conducted using a 2-lb sinusoidal input. Other

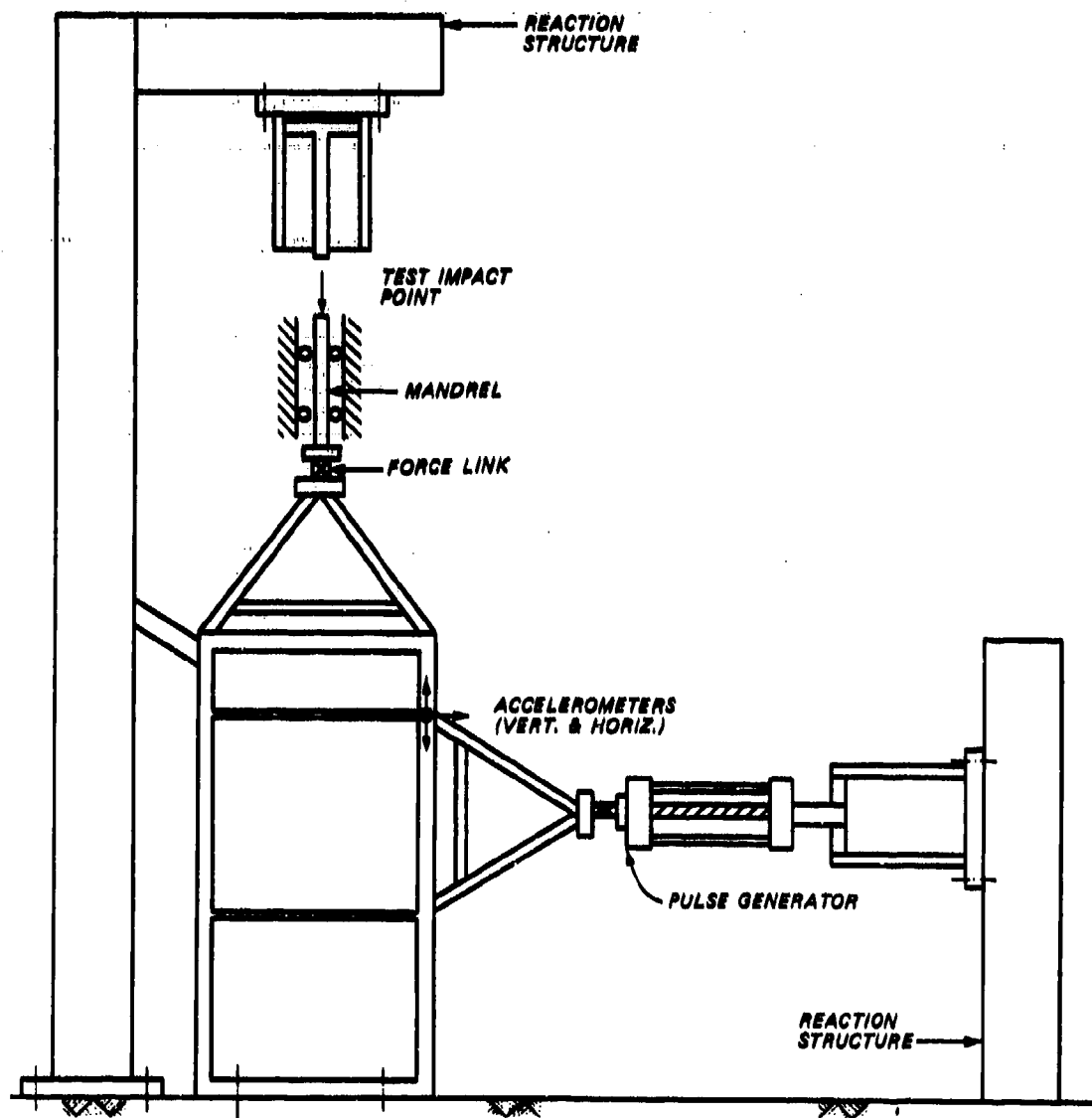


Figure 10. Vertical impedance test of biaxial test facility.

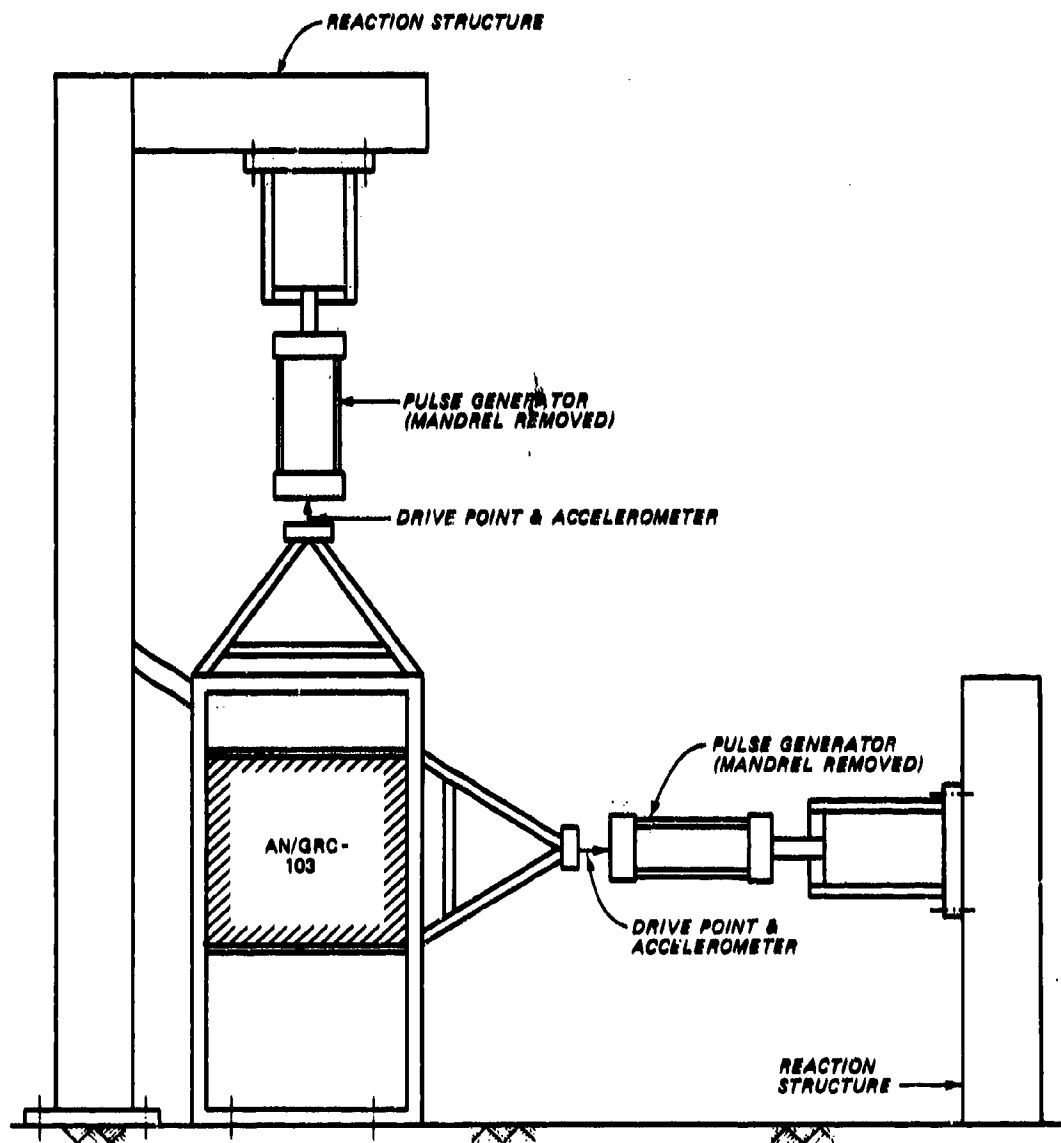


Figure 11. Source impedance measurement locations of biaxial test assembly.

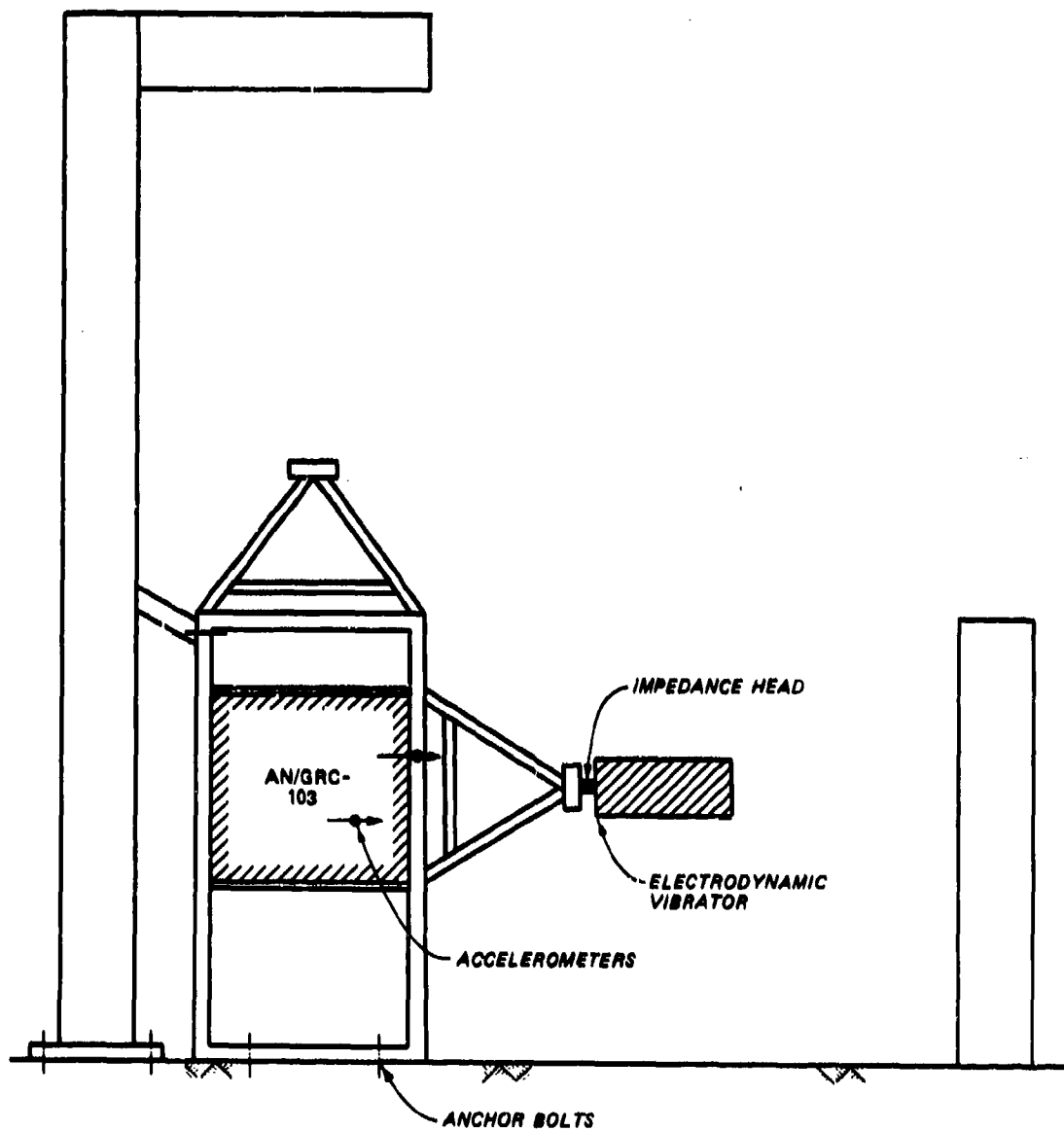


Figure 12. Vibration test setup.

tests were conducted using 1-, 5-, and 20-lb input forces. Accelerations were measured at the point of loading (drive point acceleration) on a vertical leg of the rack and on the face of the AN/GRC-103 transmitter (directly in front of a stiffening plate).

18. Data from the vibration tests are shown in Figures 13-16. Figures 13, 14, and 15 are inertance plots, $(\frac{\text{acceleration response}}{\text{driving force}})$ versus frequency. Figure 13 is the drive point inertance, i.e., $(\frac{\text{drive point acceleration}}{\text{input force}})$; Figure 14 is the inertance plot of the rack;

and Figure 15 is the inertance plot of the radio as mounted in the rack. A comparison of Figures 14 and 15 reveals that general response characteristics of the rack and radio are quite similar. Several resonance peaks are observed in the 100- to 400-Hz range, with distinctive anti-resonances particularly prevalent in the 400- to 700-Hz range. Numerous resonances occur at frequencies above 1000 Hz, the strongest being at approximately 2600 Hz. Above 4000 Hz, the radio response has more anti-resonances than the rack. Figure 16 is a transmissibility plot, the ratio of radio and rack accelerations versus frequency. As can be seen, there are numerous, high Q (lightly damped) resonances and anti-resonances throughout the frequency range. There are distinctive peaks in the curve at frequencies below 400 Hz, particularly in the 150- to 200-Hz range, representing amplifications of up to 10 of radio versus rack accelerations. However, the curve generally falls in the 0.1 to 1.0 amplitude range signifying reduced accelerations being transmitted from the rack to the radio. This energy is apparently lost in the radio/rack bolted connection.

TESTS OF OPERATIONAL EQUIPMENT

19. Two units of operational equipment were delivered to WES for testing: (a) AN/GRC-103 Transmitter and Receiver, and (b) TD660 Multiplexer. These units were brought to WES, installed in the rack, and operated on-line during testing by personnel from the U. S. Army Depot, Tobyhenna, Pa. Horizontal, uniaxial pulse tests were conducted on these units utilizing the same instrumentation as in the impedance tests; i.e.

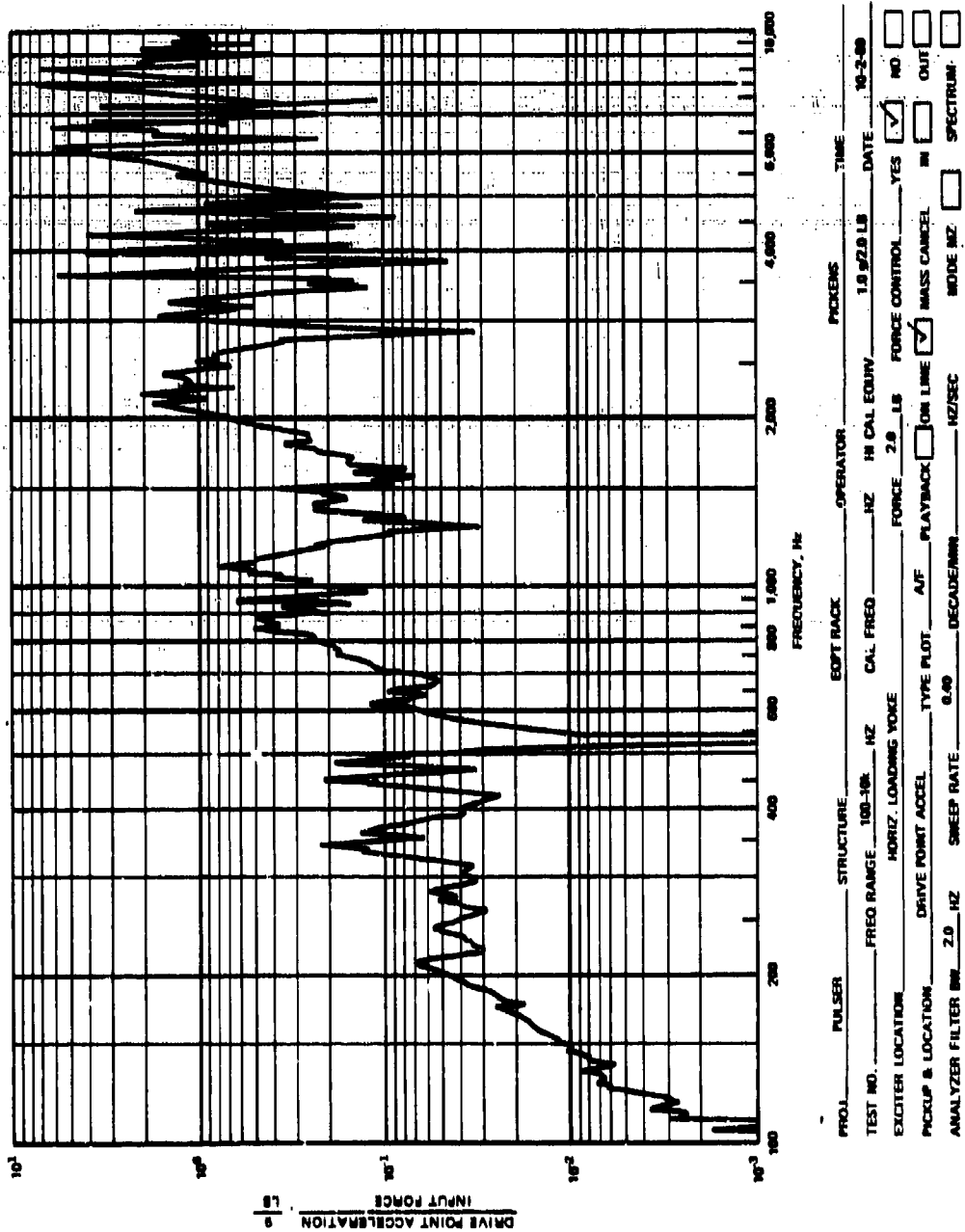
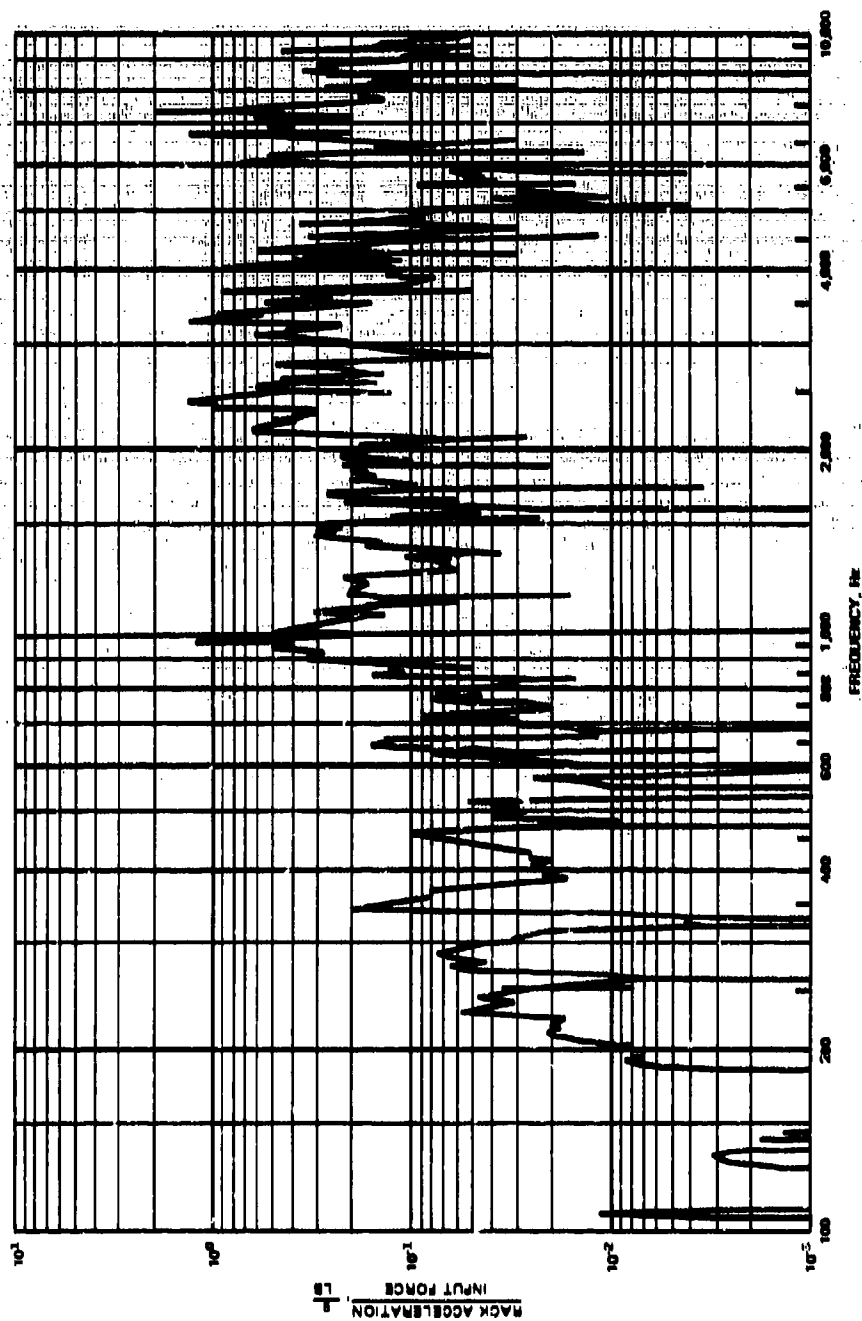


Figure 13. Vibration test data, drive point inertance.



PROJ. _____ PULSER _____ STRUCTURE _____ EQUIP. RACK _____ OPERATOR _____ PICKERS _____ TIME _____
 TEST NO. _____ FREQ. RANGE 100-10,000 Hz CAL. FREQ. _____ Hz IN CAL. EQUIV. 2.0 g/2.0 LB DATE 10-2-80
 EXCITER LOCATION _____ HORIZ. LOADING Yoke _____ FORCE 2.0 LB FORCE CONTROL YES ☒ NO ☐
 PICKUP & LOCATION _____ EQUIP. RACK VERTICAL LEG TYPE PLOT A/F PLAYBACK ☐ ON LINE ☒ MASS CANCEL IN ☐ OUT ☒
 ANALYZER FILTER BW 2.0 Hz SWEEP RATE 0.25 Hz/SEC DECADE/MIN. _____ Hz/SEC MODE NZ ☐ SPECTRUM ☒

Figure 14. Vibration test data, equipment rack inertia.

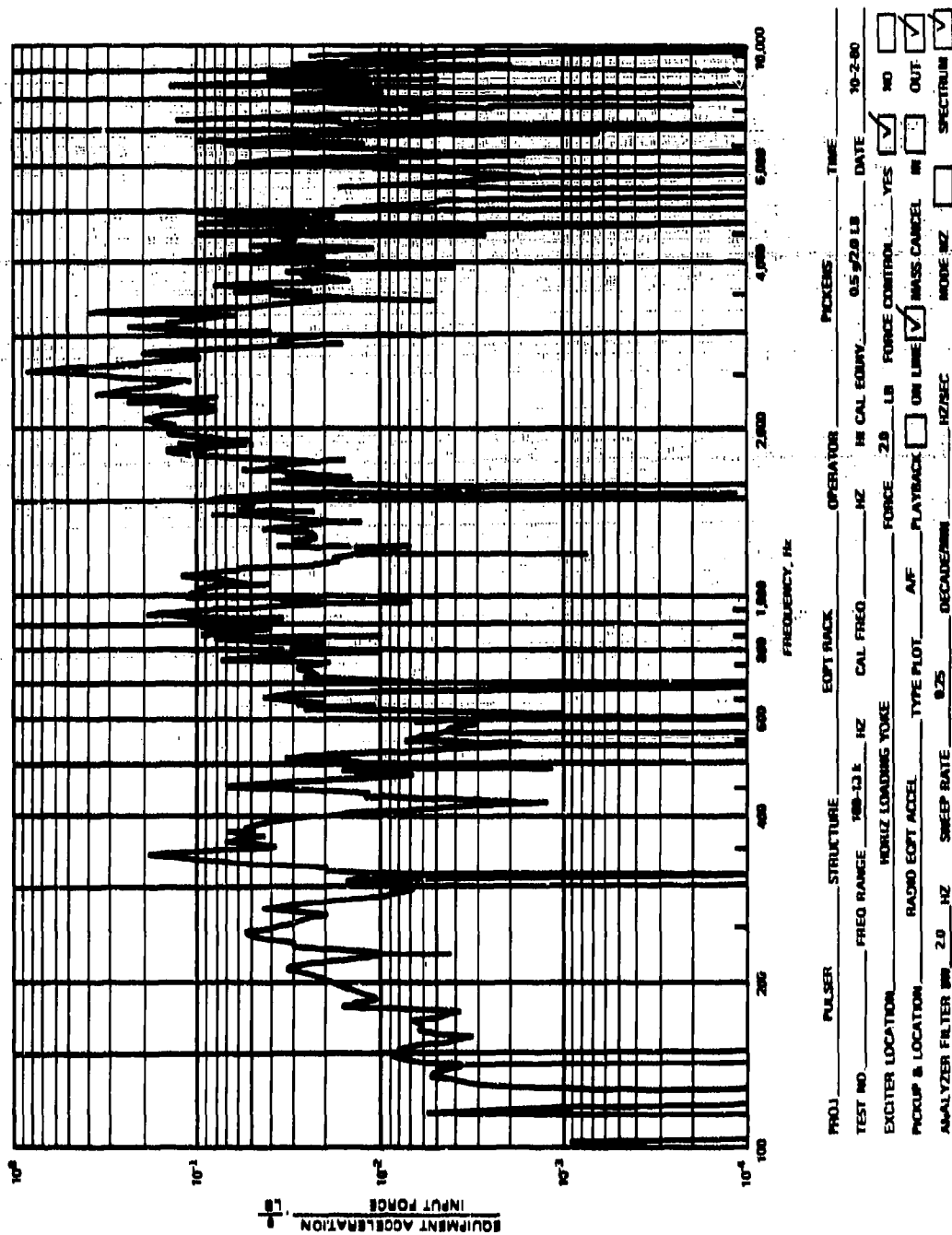


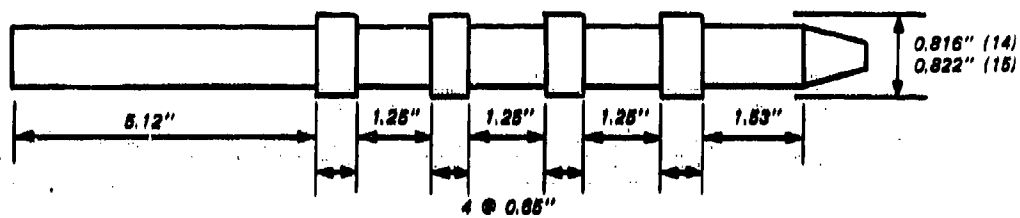
Figure 15. Vibration test data, equipment inertance.

accelerometers on the rack vertical leg and on the face of the equipment along with the force link. Initial tests were run with the AN/GRC-103 installed, but not on-line, followed by on-line tests of both the AN/GRC-103 and TD660.

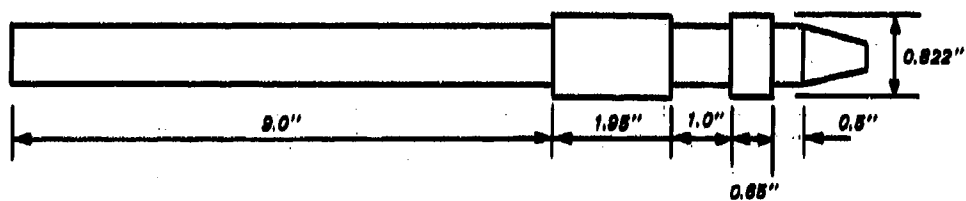
20. Both transmitter and receiver were mounted in the rack using standard mounting angles and screws. Six tests were conducted utilizing different pulse trains (Figure 17) in the horizontal axis. The tests are summarized in Table 3, and data for each test are presented in Appendices A-F. The data were digitized at rates of 20,000 and 10,000 samples per second, thereby limiting the useful frequency ranges to 10 kHz and 5 kHz, respectively (based on conventional digitizing procedures). Data for each test are in the form of time histories, fast Fourier transforms (FFT's), auto correlations, cross correlations, and cross spectral density records. For the data in the frequency domain (at the 10K digitizing rate), both fine and coarse plots were made; i.e., the curves were defined with either 1024 points or 512 points. The coarse data plots simply give gross approximations of the curves, often better for visualization of the data.

21. There was no apparent damage to any of the pieces of equipment during the tests. The off-line tests of equipment were conducted using nonoperational units followed by the tests of operational units. For the operational, on-line tests, the units were turned on several minutes before testing and allowed to operate several minutes after testing. Even though relatively high acceleration levels were measured on the rack (up to 200 g's peak), the equipment suffered no apparent damage. This result led to a closer look at what the measured accelerations actually indicate.

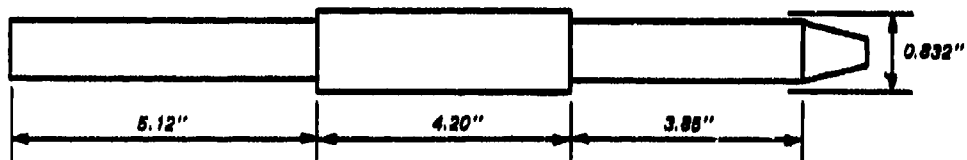
22. The motions measured on the rack and those transmitted to the equipment are highly dependent on the particular pulse train. Maximum utilization of the pulse generator, leading to maximum loading of the equipment, can only be accomplished using specifically designed pulse trains taking into account the dynamic characteristics of the total system being tested. The energy accepted by the equipment is frequency-sensitive, and the frequency content of a particular pulse train cannot



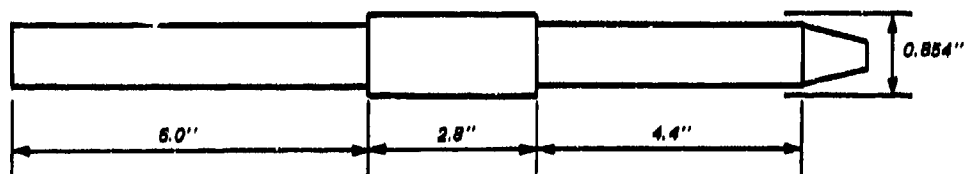
TESTS 14 AND 15



TEST 16



TEST 17



TESTS 18 AND 20

Figure 17. Pulse trains for tests 14-20, rack hard-mounted.

Table 3
Summary of Tests 14-20, Rack Hard-Mounted

Test No.	Average Force (lb)	Rack Acceleration (g)			Equipment Acceleration (g)			$\frac{\text{EQUI}}{\text{RACK}}$ RMS	Low-Pass Filter (kHz)	Notes
		MAX	RMS	MAX	MAX	RMS	MAX			
14	1100	516	111	0.23	88	20	0.23	0.18	10	AN/CRC-103, off-line
	1000	116	38	0.24	69	18	0.26	0.47	5	
15	1400	428	68	0.16	165	26	0.16	0.38	10	
	1400	232	38	0.16	109	20	0.18	0.52	5	
16	1500	477	81	0.17	130	24	0.18	0.30	10	
	1400	175	28	0.16	86	15	0.17	0.54	5	
17	2400	968	176	0.18	208	48	0.23	0.27	10	
	2200	202	47	0.23	152	42	0.28	0.89	5	
18	4000	2029	257	0.13	167	32	0.19	0.12	10	AN/CRC-103, on-line
	4000	772	114	0.15	85	22	0.26	0.19	5	
20	4000	1750	302	0.17	148	3	0.20	0.10	10	TD660, on-line
	4000	800	194	0.24	88	22	0.25	0.12	5	

be predetermined without a detailed analysis. However, the general pulse trains used in these initial tests were quite useful in determining how the equipment responds to motions input to the rack.

23. The accelerations measured on both the rack and the equipment contain sharp, high-frequency peaks. The 10-kHz filtered data contain rack acceleration peaks of up to 4.8 times those of the 5-kHz limited digitized records (Test 17, Table 3). For Test 15, the 10-kHz rack peak accelerations were only 1.8 times those of the 5-kHz records. However, the pulse trains of Tests 15 and 17 are significantly different. Perhaps more important than peak response is the RMS value of measured acceleration. The 5-kHz RMS acceleration response of the equipment in Test 17 is nearly equivalent to that of the rack (42 g's versus 47 g's). For this pulse train, then, the transmissibility of energy from rack to equipment was quite high (89 percent). However, in Test 20, the RMS equipment response was only 22 g's compared to rack RMS response of 194 g's, giving a transmissibility of only 12 percent. The ratios of equipment RMS response to rack RMS response are shown in Table 3 for each test. It is of interest to note that although the pulse trains of Tests 20 and 17 are quite similar (except for depth of cut; i.e., nubbin diameter), these two tests represent the extremes of equipment-to-rack response ratios (0.89 for Test 17 and 0.12 for Test 20). Upon comparison of the FFT's for the force input for each test (plot No. 90, Appendix D, for Test 17 and plot No. 98, Appendix F, for Test 20), it is seen that the primary frequency content is 2880 Hz for Test 17 and 2620 Hz for Test 20. This relatively small difference in frequency content of input force can significantly change the transmissibility ratio of equipment-to-rack response. This is quite apparent when considering the transmissibility plot of Figure 16 from the vibration tests. Extremely large differences in the ratio, on the order of 1000 to 1, exist for only minute changes in frequency. This is simply the nature of the rack-equipment system. It is a high Q, lightly damped, ringing type of structure having numerous resonances. It must also be kept in mind that the vibration tests were conducted using a 2-lbf input and the resonances and anti-resonances for both rack and radio could change significantly for a

force input of several thousand pounds due to nonlinearity in the system.

24. Consider the force input FFT for Tests 14-20. With the exception of Tests 14 and 15, there is a predominant peak occurring in the 2500- to 3000-Hz region, indicating that most of the input force is at this frequency. This harmonic motion can also be seen on the auto correlation functions of the force inputs. This motion is due to chatter in the pulse generator as the cutter plows through a nubbin. The chatter is also apparent in the cut nubbin as the cut surface contains ripples rather than being smooth. The deeper and longer the cut, the greater the amount of chatter. During the calibration tests, a different cutter geometry was tried in an effort to reduce this chatter. However, the new cutter, which utilized a rake angle, did not reduce chatter; it actually increased it somewhat. The pulse train used in Tests 14 and 15 contained several short nubbins, as opposed to a single longer nubbin, and the chatter is not as severe. This fact is reflected in the FFT's of the input force for these tests, which do not exhibit the large spike in the 2500- to 3000-Hz region.

TESTS OF SOFT-MOUNTED EQUIPMENT

25. In an effort to introduce higher accelerations into the equipment at lower frequencies, the equipment rack mounting configuration was changed. For all previous tests, the rack was secured directly to the concrete floor with four anchor bolts and tied to the reaction structure with a steel angle and bolts. This type mounting arrangement was considered to be a "hard mount." The "soft-mount" arrangement, shown schematically in Figure 18 and in the photographs, Figures 19-21, consisted of using Firestone Airmount Isolators (air bags) for all horizontal support. The floor anchor bolts were removed as was the horizontal steel angle positioned at the top of the rack. The rack was attached to four air bags (two at the top and two at the bottom) as shown in Figures 18-21. The air bags used, Firestone Airmount No. 125, have a natural frequency of 160 Hz and will deflect approximately 3 in. before bottoming out. Tests were conducted with the bags pressurized at values ranging from 30 to 70 psi. Having an effective area of 11.5 in.² each, or 46 in.² total, the four bags could resist a load of up to 1380 lb with each bag

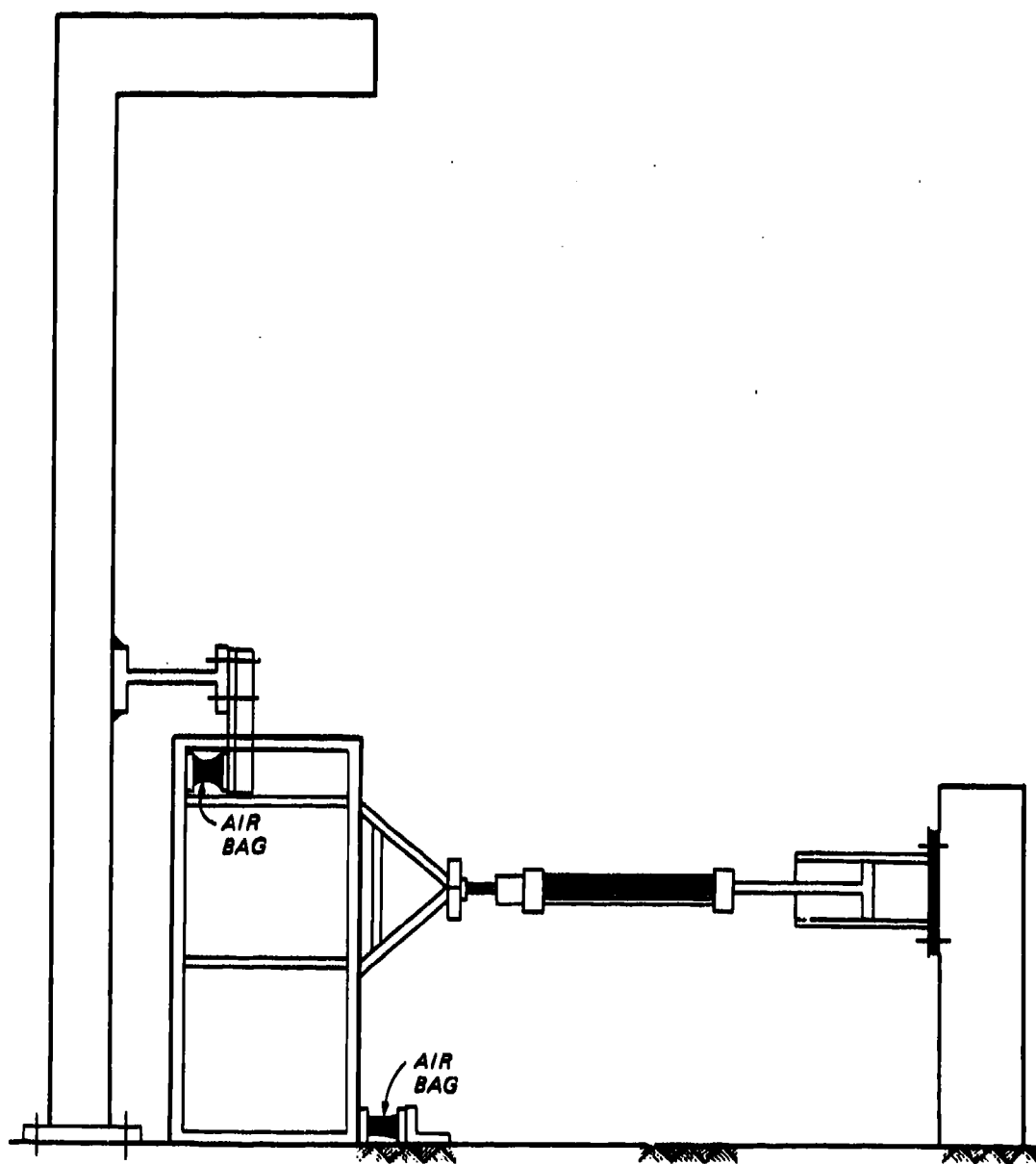


Figure 18. Schematic of soft-mount test setup.



Figure 19. Test setup with rack so.t-mounted (view A).

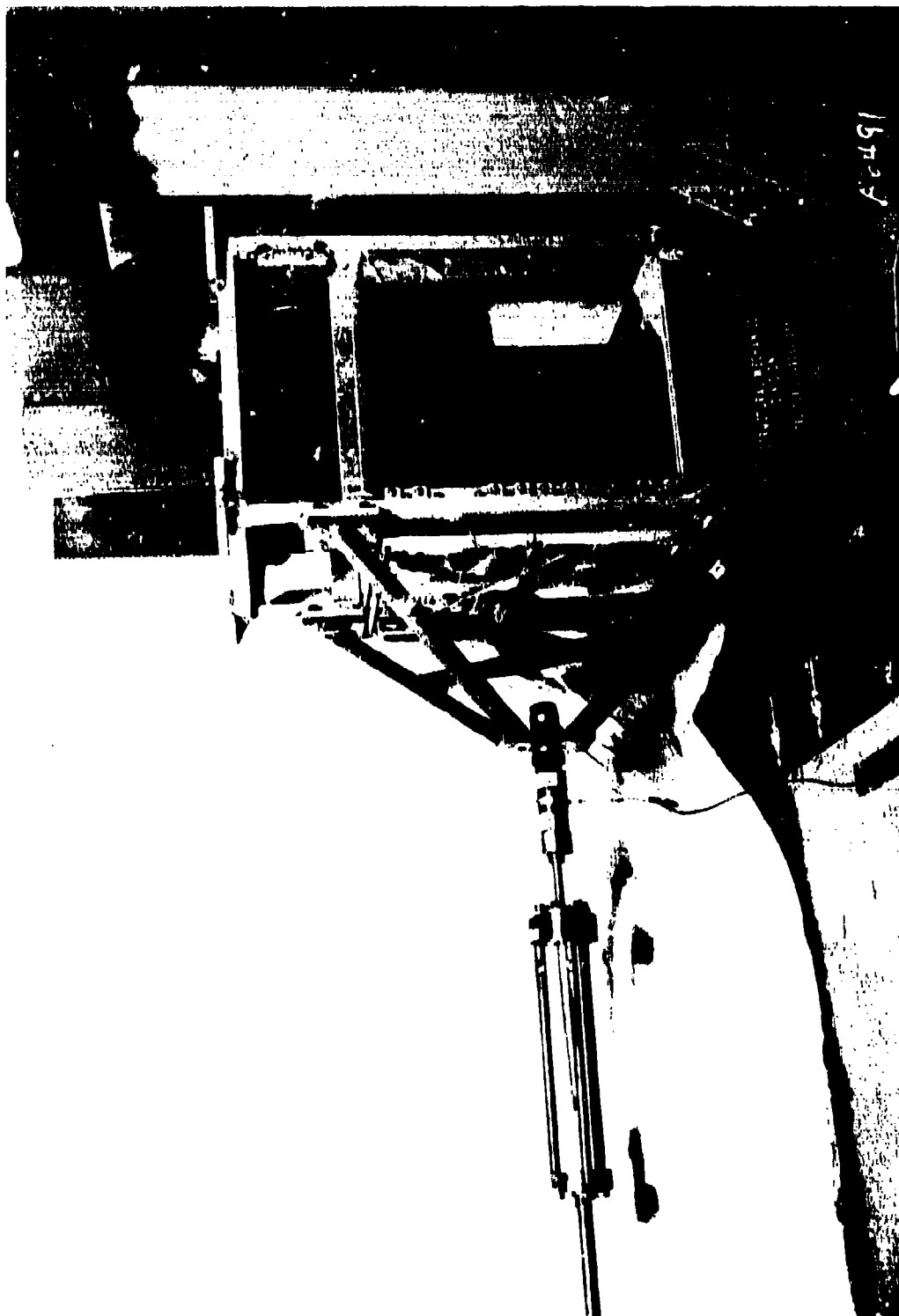


Figure 20. Test setup with rack soft-mounted (view B).

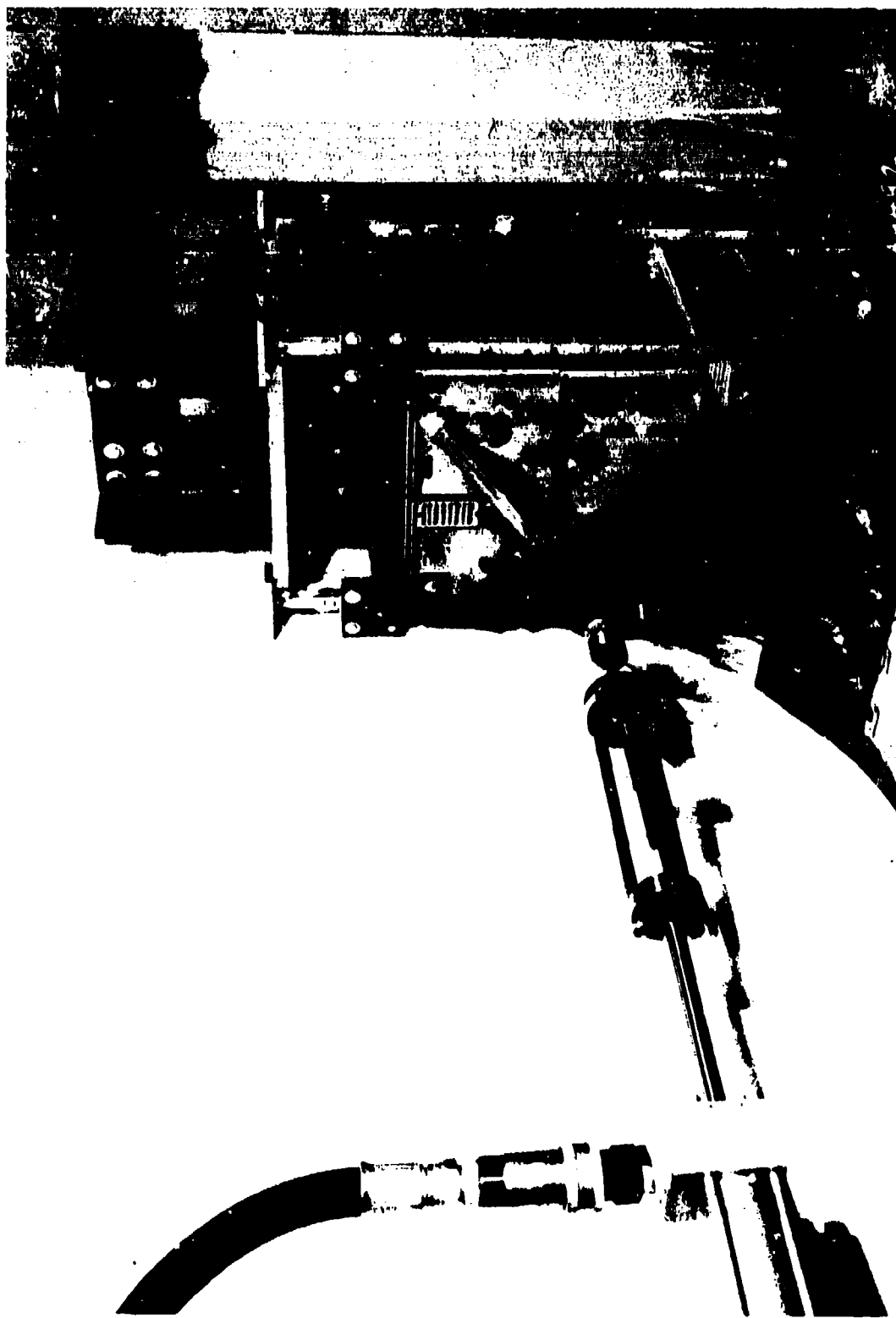
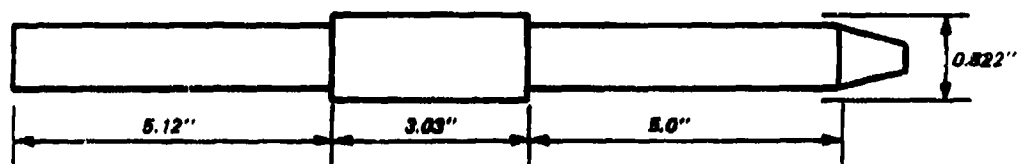


Figure 21. Test setup with rack soft-mounted (view C).

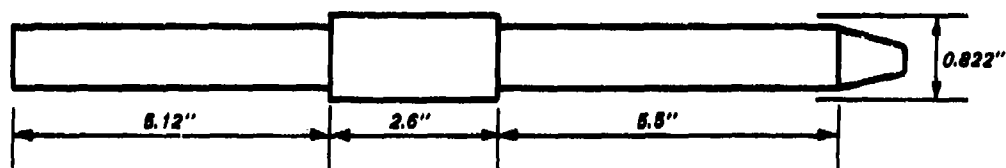
pressurized at 30 psi and up to 3220 lb at 70 psi (net area \times pressure).

26. A nonoperational AN/GRC-103 transmitter and receiver was placed in the rack and the system was instrumented as in the previous tests; i.e. a force link, an accelerometer on the rack vertical leg, and an accelerometer on the equipment face plate. Five tests were run using the pulse trains shown in Figure 22. The data are summarized in Table 4 and presented in graphical form in Appendices G-K.

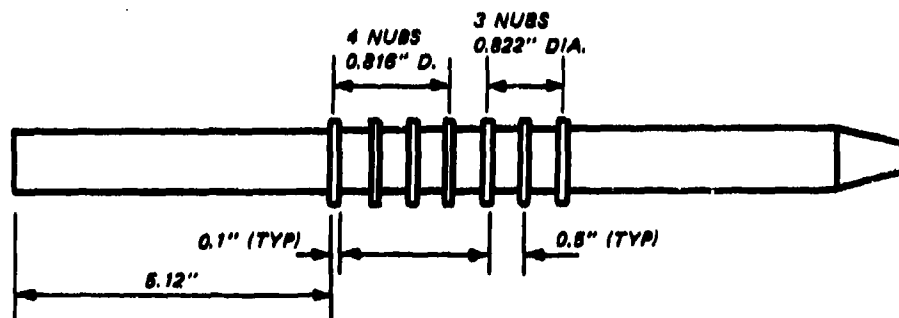
27. In general, the RMS value of the rack accelerations was 9 to 20 percent that of the peak acceleration, whereas, for the equipment, the RMS value ranged from 14 to 40 percent that of the peak. Playbacks of the time histories, FFT's, and cross spectral density records using low-pass filters of 10, 5, 3.5, 2.5, 1.5, and 0.5 kHz are given in the appendices. Such filtered plots offer a better picture of the frequency-dependent equipment motion. For the five tests conducted, the RMS value of the 500-Hz filtered equipment acceleration ranged from 25 percent to 50 percent that of the 10-kHz filtered RMS values. The ratio of equipment-to-rack RMS accelerations varied from 0.08 to 0.16 (considering only 5- and 10-kHz filtered data). For the hard-mounted tests, this same ratio ranged from 0.10 to 0.89. Thus, in general, more energy was transmitted from the rack to the equipment in the hard-mounted tests than in the soft-mounted tests. Displacements for the soft-mounted tests were substantially larger, however, as the rack was observed to move approximately 2 in. For the hard-mounted tests, displacements were on the order of 0.1 in.



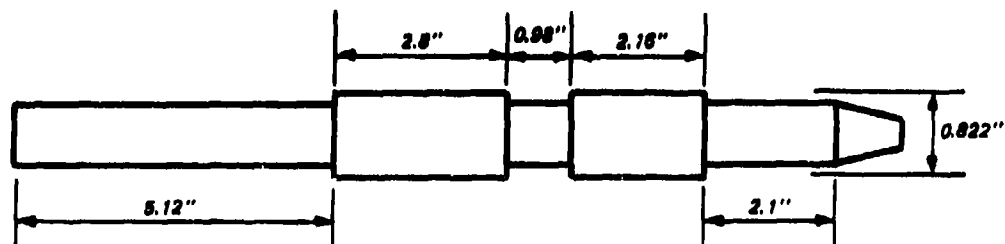
TESTS 21 AND 22



TEST 23



TEST 24



TEST 25

Figure 22. Pulse trains for Tests 21-25, rack soft-mounted.

Table 4
Summary of Tests 21-25, Rack Soft-Mounted on Air Bags

Test No.	Average Force (lb)	Rack Acceleration (g)			Equipment Acceleration, (g)			EQPT [RACK]	RMS	Low-Pass Filter (kHz)
		MAX	RMS	RMS MAX	MAX	RMS	RMS MAX			
21	900	1244	233	0.19	84	19	0.23	0.08		10
		1145	252	0.22	70	19	0.27	0.08		5
		1400	227	0.16	70	18	0.26	0.08		3.5
		1150	203	0.18	55	15	0.27	0.07		2.5
		900	177	0.20	30	9	0.30	0.05		1.5
		680	138	0.20	25	8	0.32	0.06		0.5
22	1000	1302	203	0.16	63	16	0.25	0.08		10
		1160	210	0.18	50	16	0.32	0.08		5
		1300	192	0.15	70	15	0.21	0.08		3.5
		1100	169	0.15	30	11	0.37	0.06		2.5
		930	142	0.15	22	8	0.36	0.06		1.5
		600	102	0.18	20	8	0.40	0.08		0.5
23	1000	1252	134	0.11	98	19	0.19	0.14		10
		1100	142	0.13	90	19	0.21	0.13		5
		700	120	0.17	70	17	0.24	0.14		3.5
		650	93	0.14	38	12	0.32	0.13		2.5
		350	65	0.19	22	8	0.36	0.12		1.5
		130	31	0.24	21	8	0.38	0.26		0.5
24	1500	1221	155	0.13	99	14	0.14	0.12		10
		1200	163	0.14	80	14	0.18	0.09		5
		1500	132	0.09	70	12	0.17	0.09		3.5
		1226	107	0.09	40	8	0.20	0.07		2.5
		850	84	0.10	25	7	0.28	0.08		1.5
		320	54	0.17	15	5	0.33	0.09		0.5
25	1100	1238	184	0.15	152	29	0.19	0.16		10
		1174	191	0.16	130	28	0.22	0.15		5
		1150	160	0.14	130	27	0.21	0.17		3.5
		900	120	0.13	80	16	0.20	0.13		2.5
		700	93	0.13	22	8	0.36	0.08		1.5
		350	57	0.16	20	7	0.35	0.12		0.5

PART IV: CONCLUSIONS AND RECOMMENDATIONS

CONCLUSIONS

28. The effort to date has been successful. A unique test device has been developed and has been shown to be an effective means for subjecting communication equipment to acceleration levels that might be encountered in a battlefield condition. Based on results of tests thus far conducted, the following conclusions are drawn:

a. A biaxial force-pulse generating device (pulser) has been developed which has a force output capacity of approximately 10,000 lb.

b. The pulser can be controlled to initiate simultaneous force pulses in both horizontal and vertical axes.

c. Up to 2000-g-peak and 300-g-RMS acceleration levels have been induced in the equipment rack with up to 200 g's peak and 48 g's RMS being transmitted to the equipment in the rack.

d. The AN/GRC-103 and TD660 communication equipment sustained no damage while being operated on-line during force-pulse tests which produced 300 g's peak (32 g's RMS) in the equipment.

e. For the pulse trains thus far used in the test program, acceleration levels measured on the equipment were 10 to 89 percent (average of 34 percent) of those measured on the rack with the rack hard-mounted and 8 to 16 percent with the rack soft-mounted on air bags (considering 5-kHz low-pass filtered data).

f. The present cutter being used in the pulser produces a certain amount of tool chatter as the aluminum nubbins are cut. This chatter results in a high concentration of force in the 2500- to 3000-Hz region. For cuts without the chatter, the force input is more broad-banded without large concentrations of energy at particular frequencies.

RECOMMENDATIONS

29. For a successful program of testing communication equipment with the force-pulse generator, the following recommendations are offered:

a. Specific pulse trains should be designed utilizing the dynamic characteristics of the equipment and equipment-rack system.

Furthermore, the dynamic characteristics should be obtained from high-level excitation such as an actual force-pulse test.

b. Additional development work should be done in an effort to reduce tool chatter. Areas to consider include cutter shape, depth of cut, and nubbin material. Perhaps a softer material, such as nylon, Teflon, Micarta, etc., using greater depths of cuts with the existing cutter would produce acceptable force levels with reduced chatter.

c. A realistic acceleration standard, to which the communication equipment could be subjected in a laboratory test environment, should be developed. Once this standard is known, a pulse train should be designed which will result in equipment response matching the standard.

REFERENCES

1. Agbabian Associates. 1979 (Dec). "Biaxial Transient Vibration Simulation for C³ Equipment to Match Field Test Records-Tests Plan," Report R-8014-4994, El Segundo, Calif.
2. US Army Engineer Waterways Experiment Station and Agbabian Associates. 1980 (Oct). "Biaxial Transient Vibration Simulation for C³ Equipment-Pulse Train Calibration," Report R-8014-5136, El Segundo, Calif.
3. Industrial Publishing Co. 1972/73. Fluid Power Handbook and Directory, Cleveland, Ohio.

APPENDIX A: TEST 14 DATA

TEST 14
Equipment Rack Hard-Mounted
AN/GRC-103 in Rack, Off-Line

Plot Heading Nomenclature (Tests 14-20)

CHAN 1 - Input force (data at 20,000 digitizing rate)

CHAN 2 - Rack acceleration (data at 20,000 rate)
- Input force (data at 10,000 rate)

CHAN 3 - Equipment acceleration (data at 20,000 rate)
- Rack acceleration (data at 10,000 rate)

CHAN 4 - Equipment acceleration (data at 10,000 rate)

RMS, AVG, MAX, XMAX, XMIN, MEAN - RMS, average, maximum, minimum
and mean values of data plots

FREQ - Frequency at which maximum value occurs

FFT 0.0 - Fast Fourier transform of time history

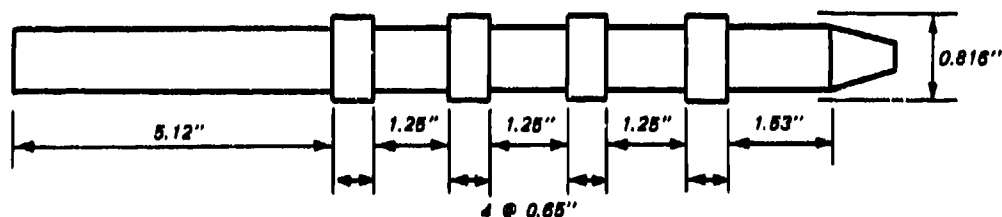
TIME 0.0 - Time history record

CSDF 0.0 - Cross spectral density function

CH/2 1.0 Channel number of the second channel for plots involving
CH/2 2.0 two-channel functions (CSDF)
CH/2 3.0

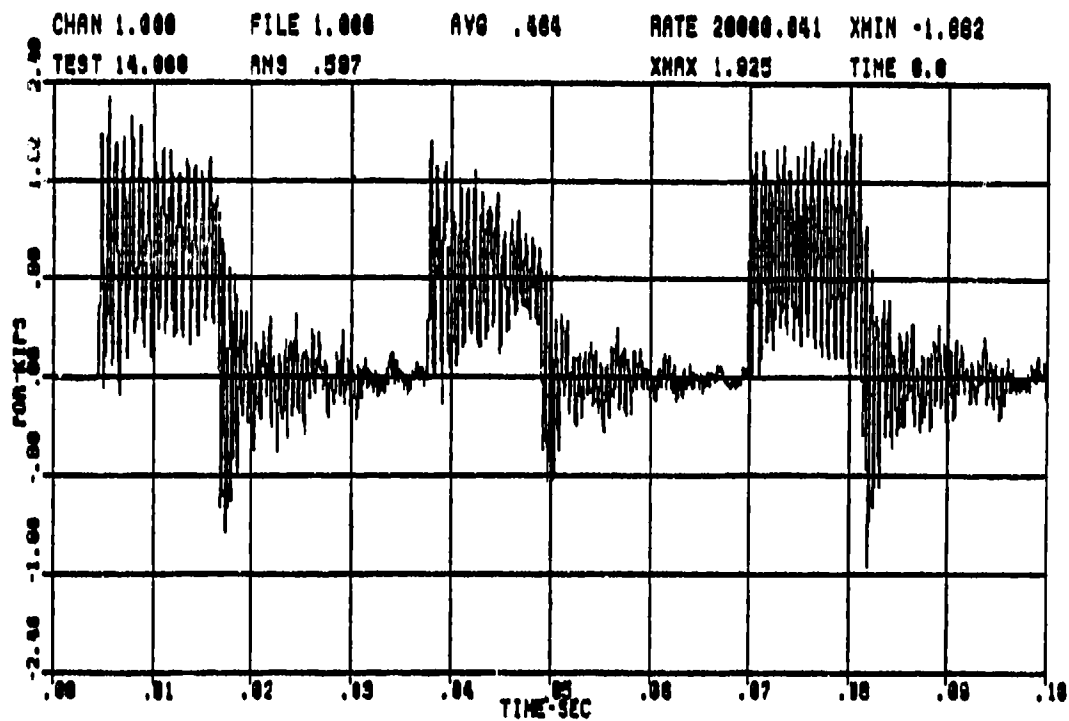
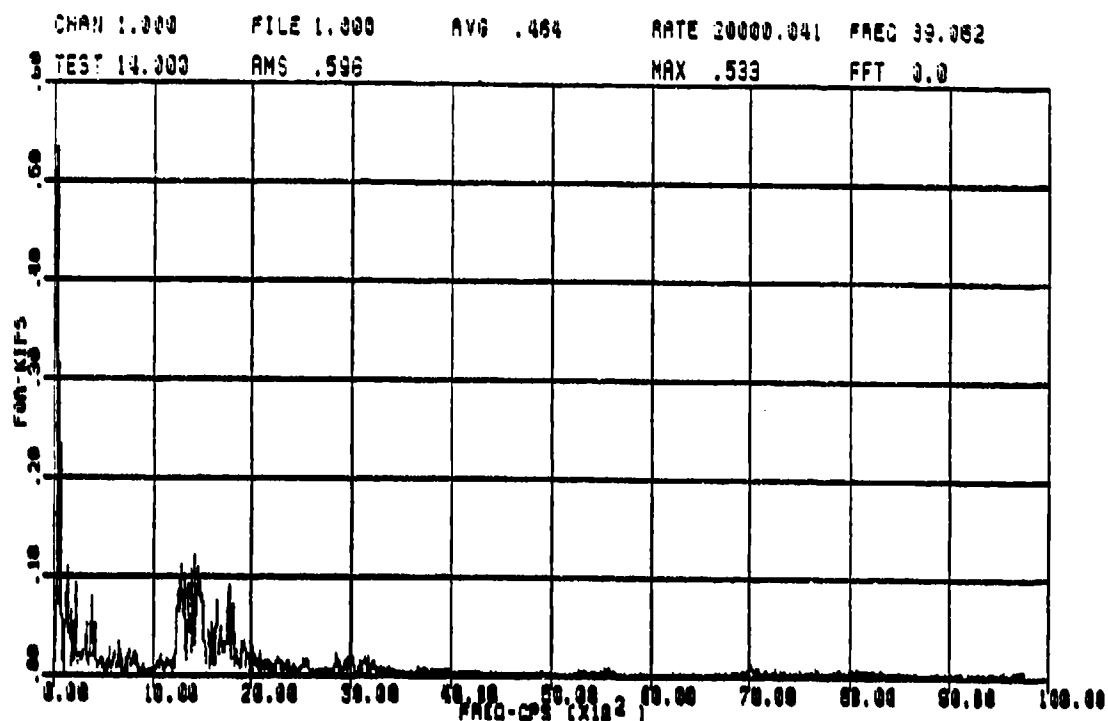
POINTS - Number of points used for plotting the record

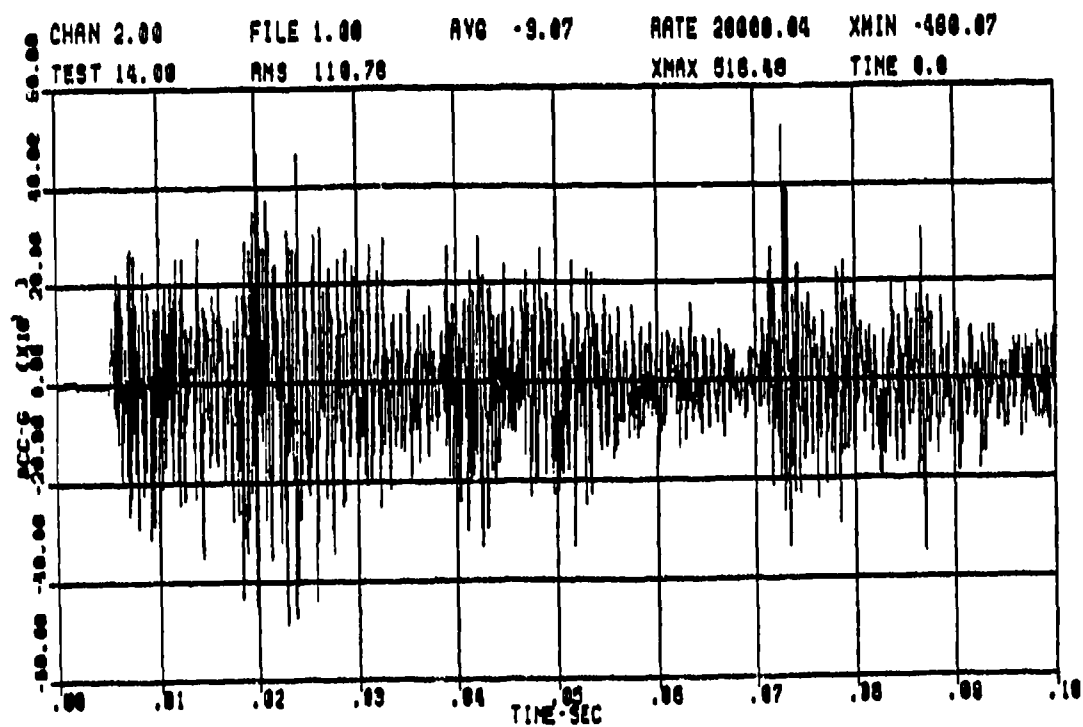
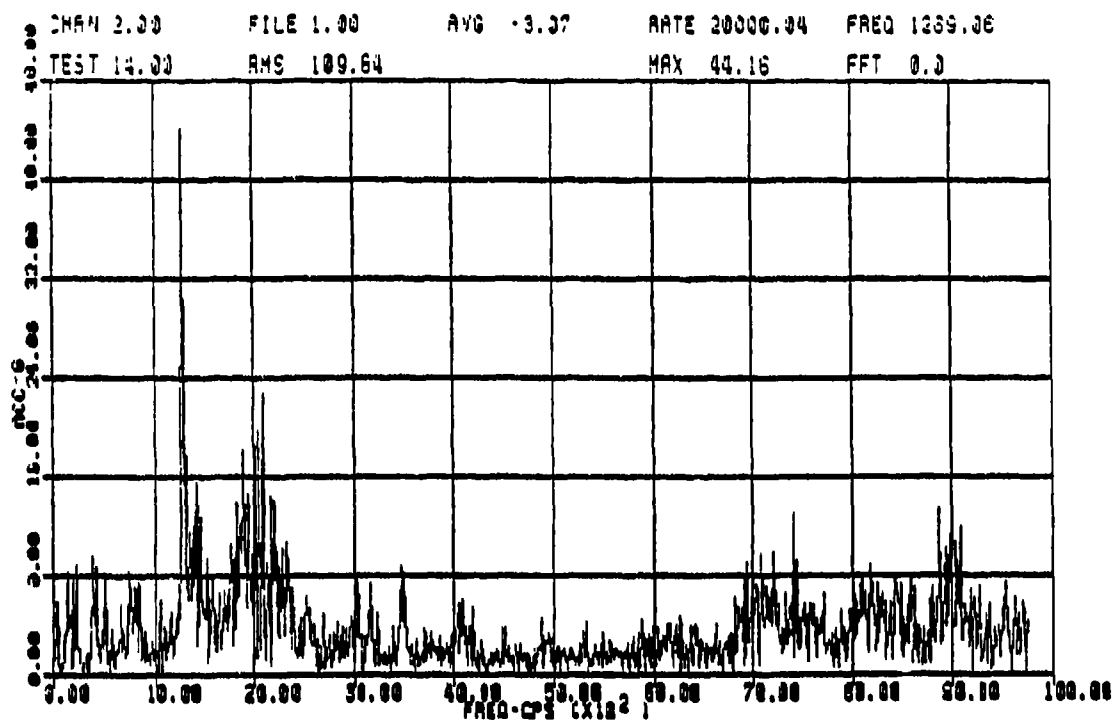
RATE - Digitizing rate, samples per second

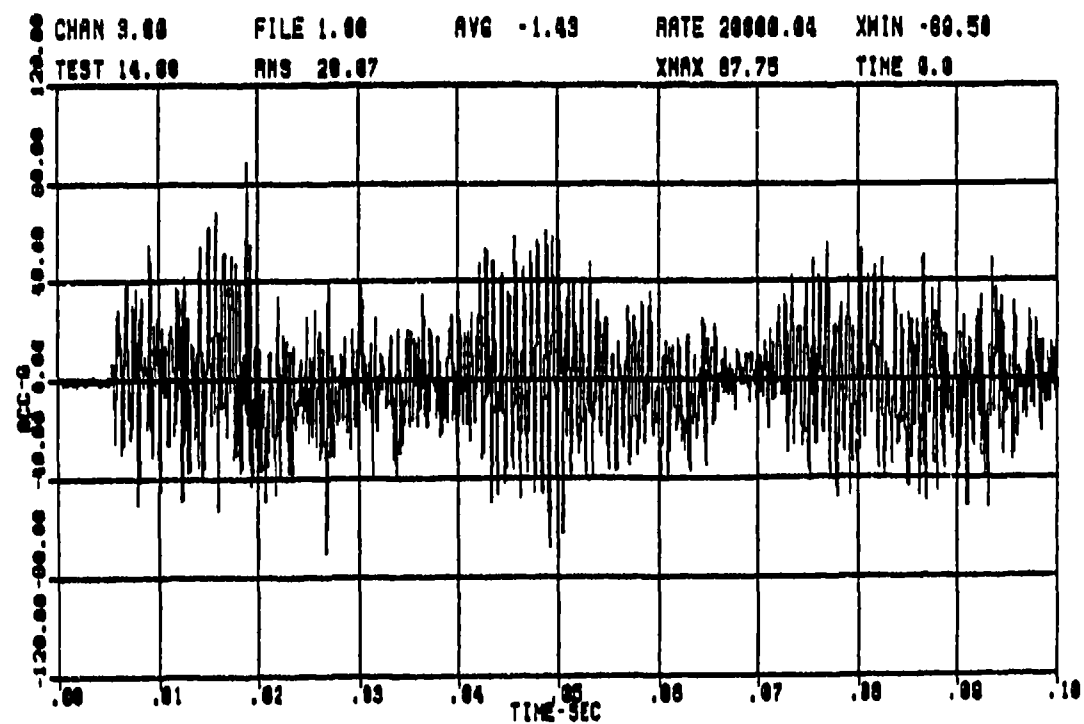
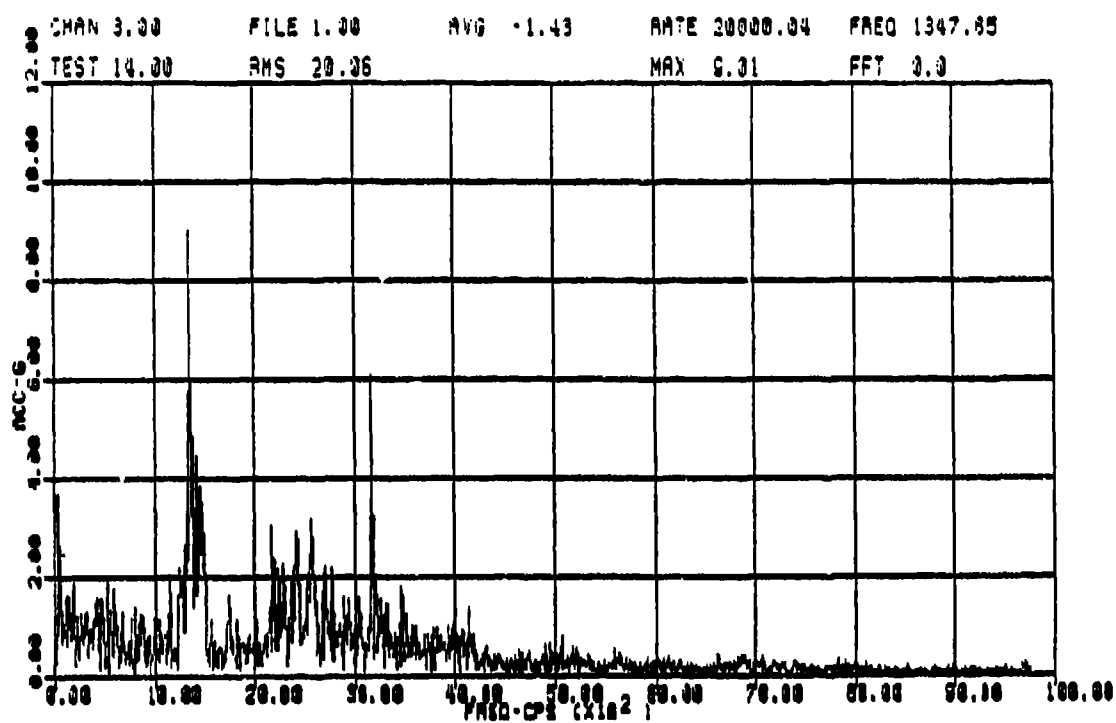


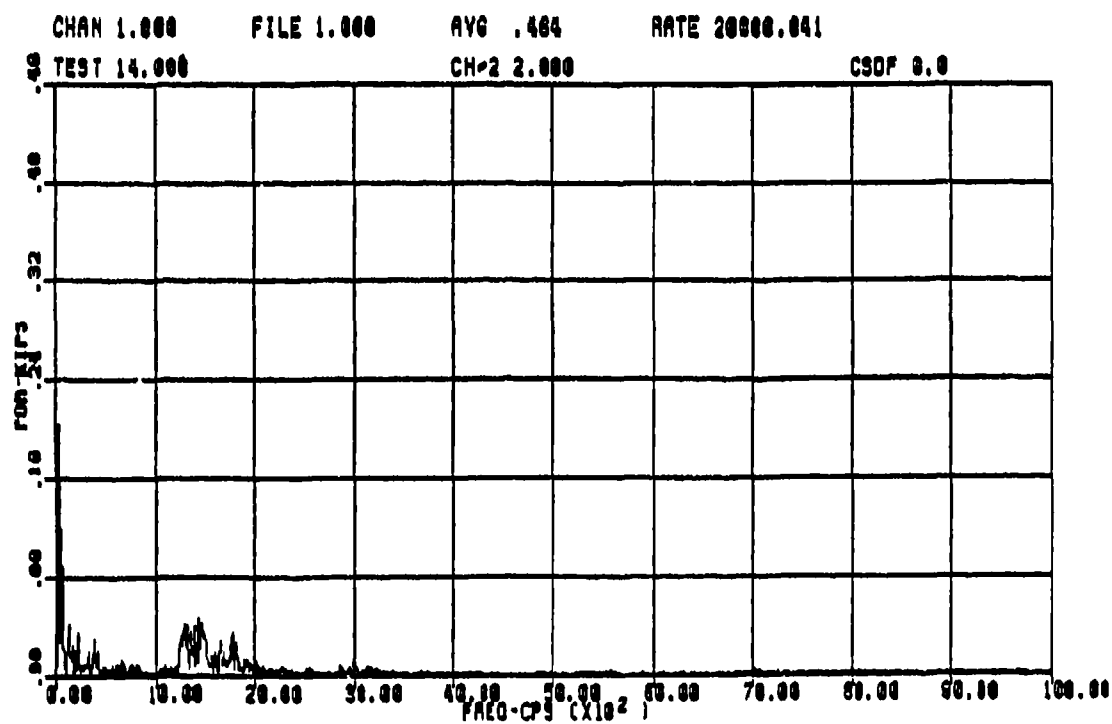
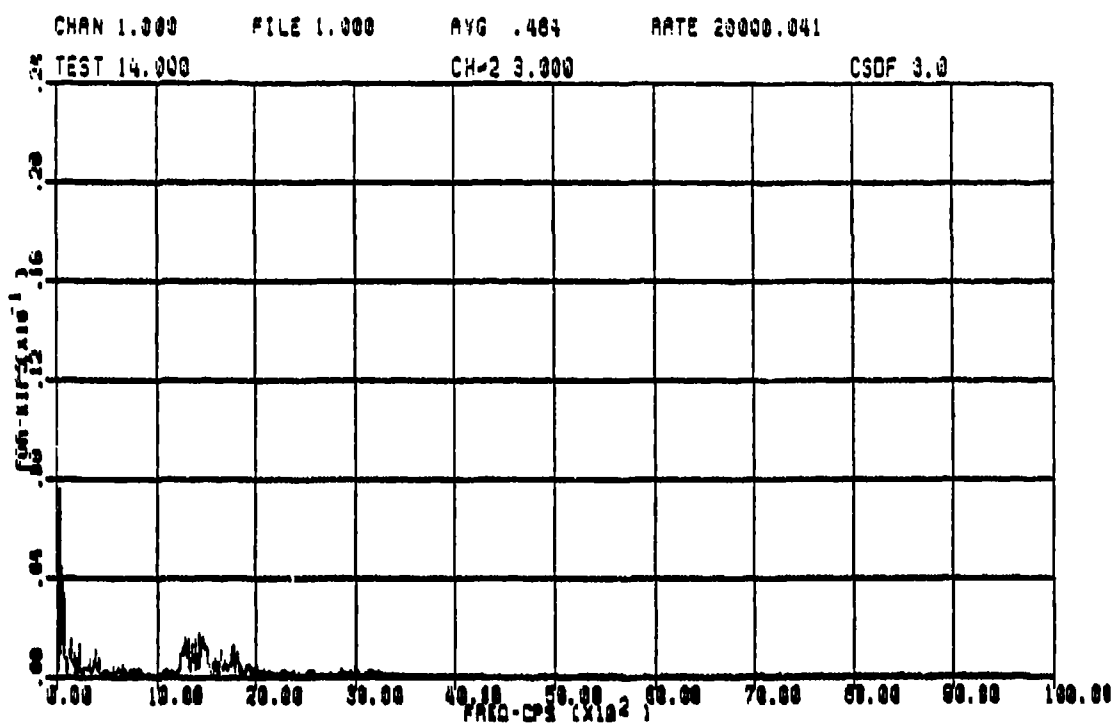
PULSE TRAIN - TEST 14

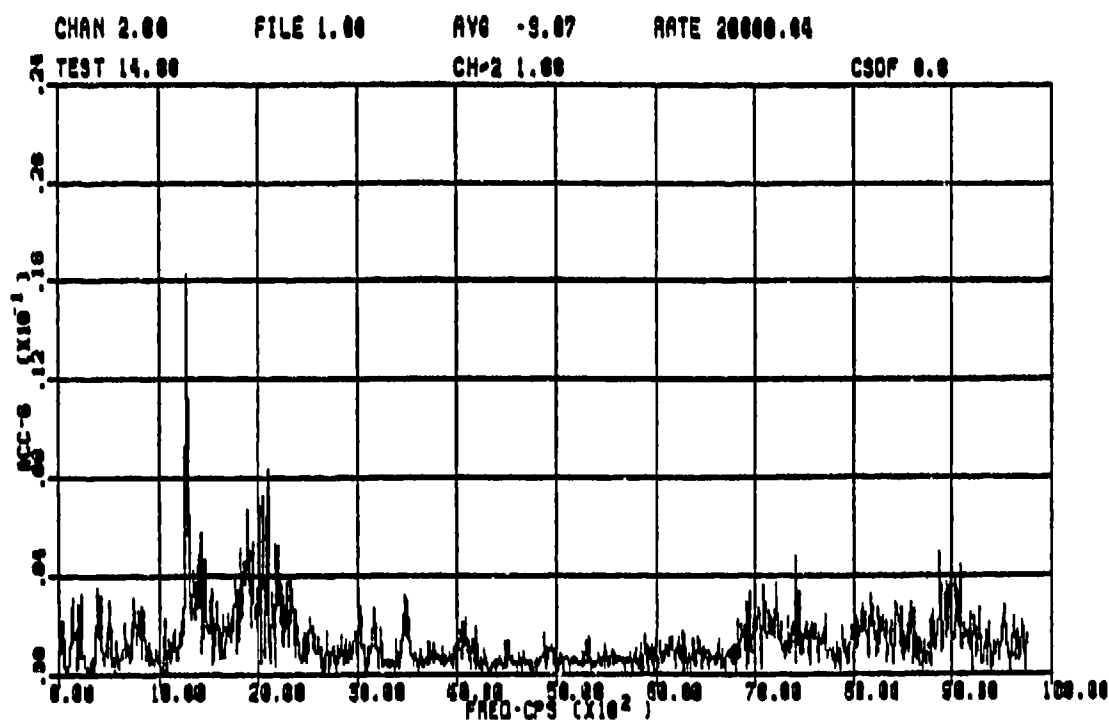
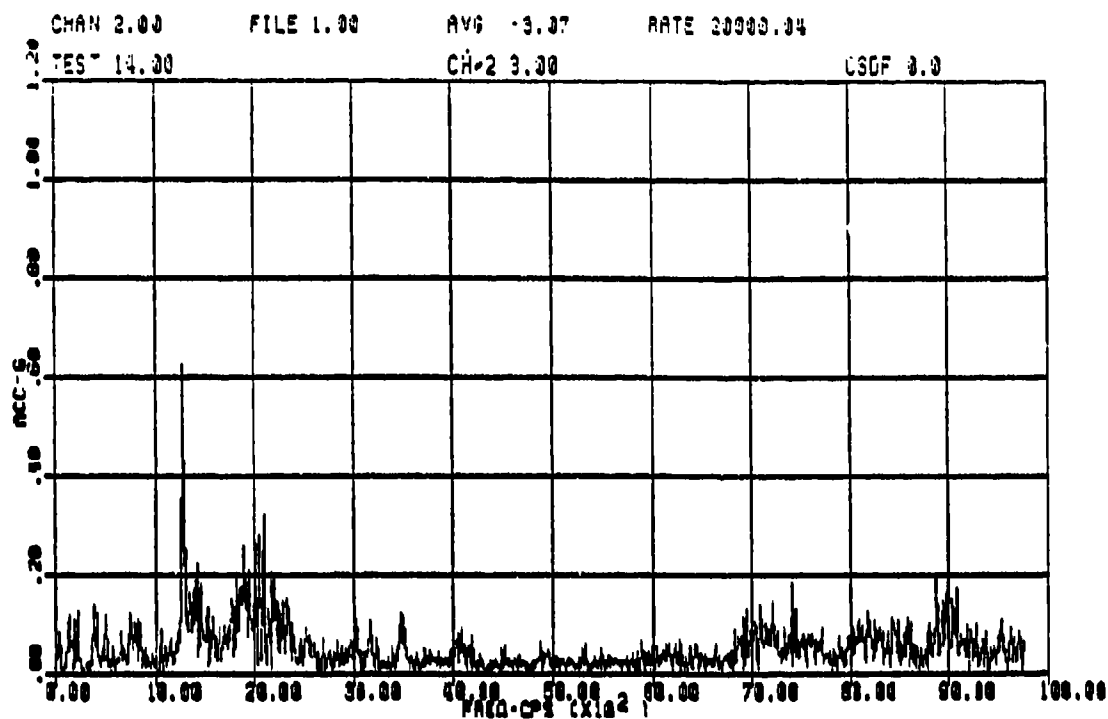
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SYSTEM PRESSURE - 2000 PSI
FLOW CONTROL #8%

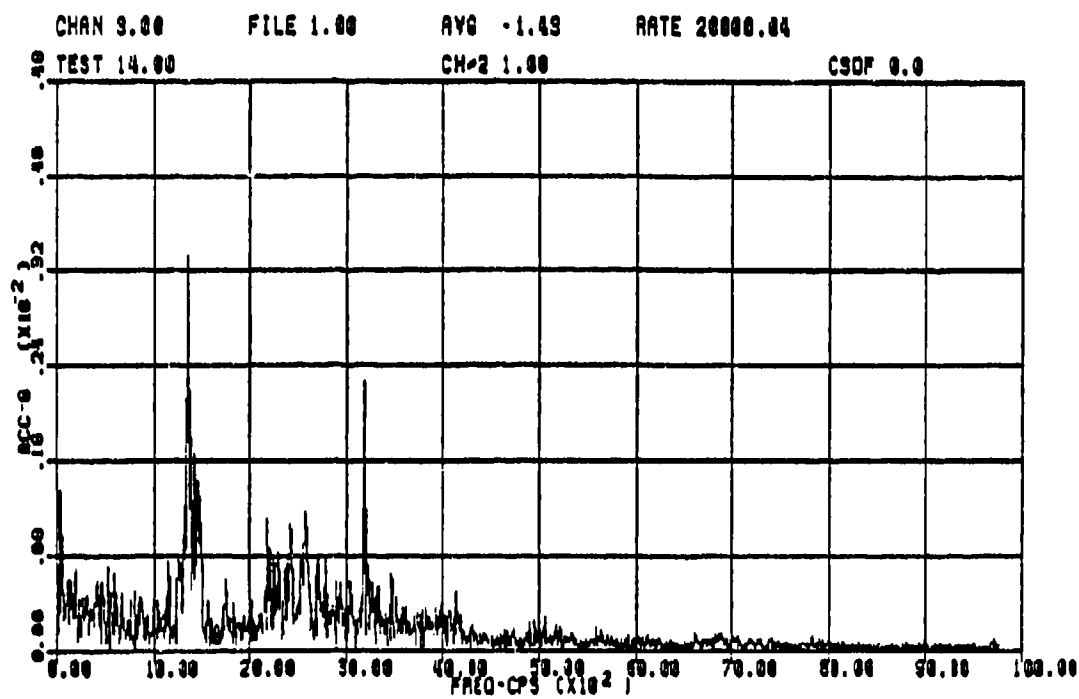
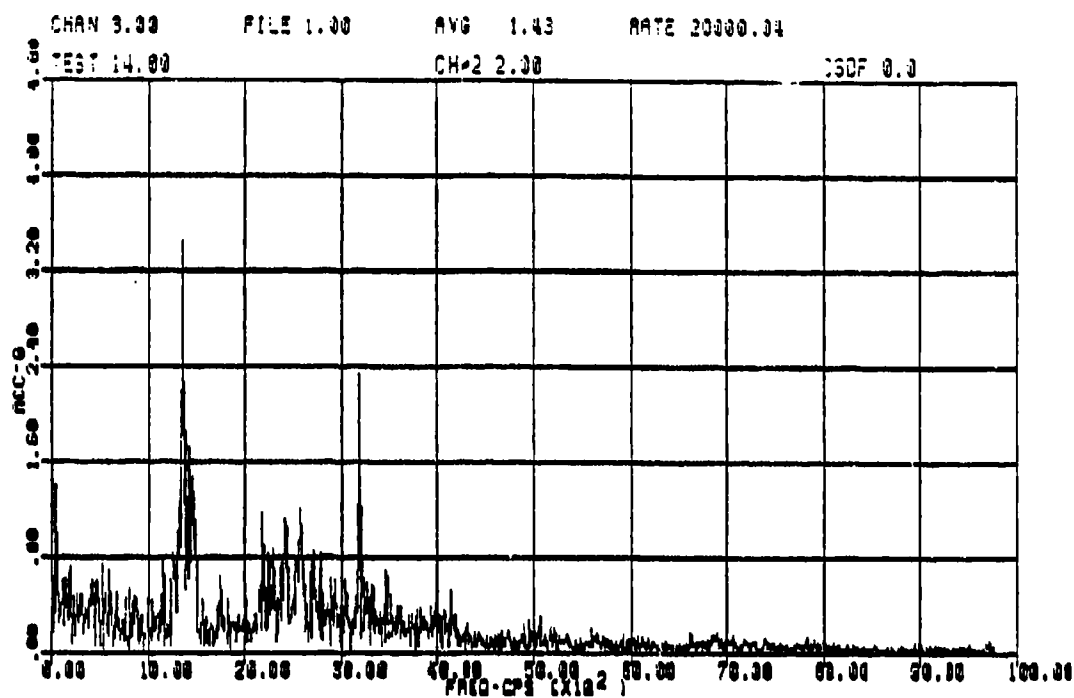




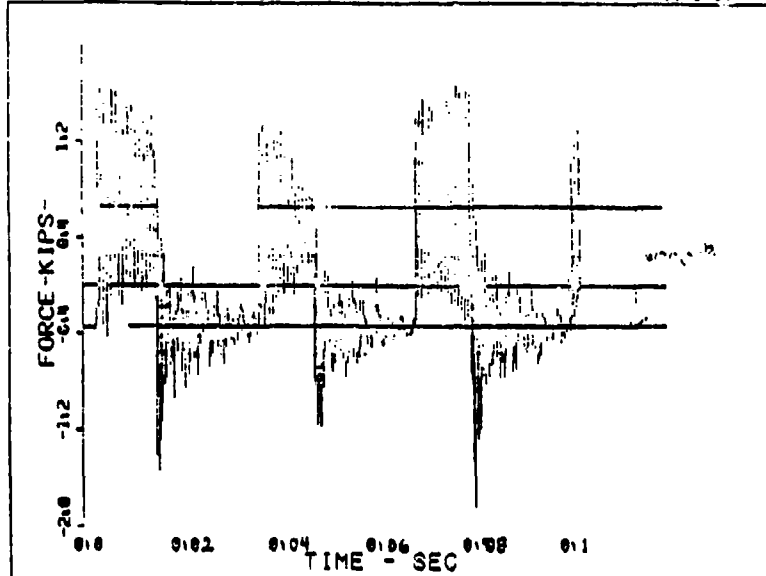








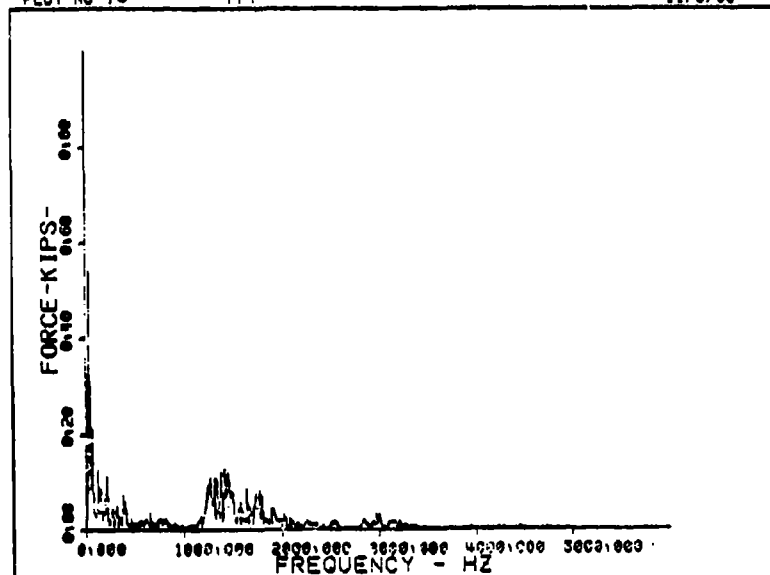
PLOT NO 73 TIME HISTORY 11/3/88



RAW

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PLOT NO 74 FFT 11/3/88



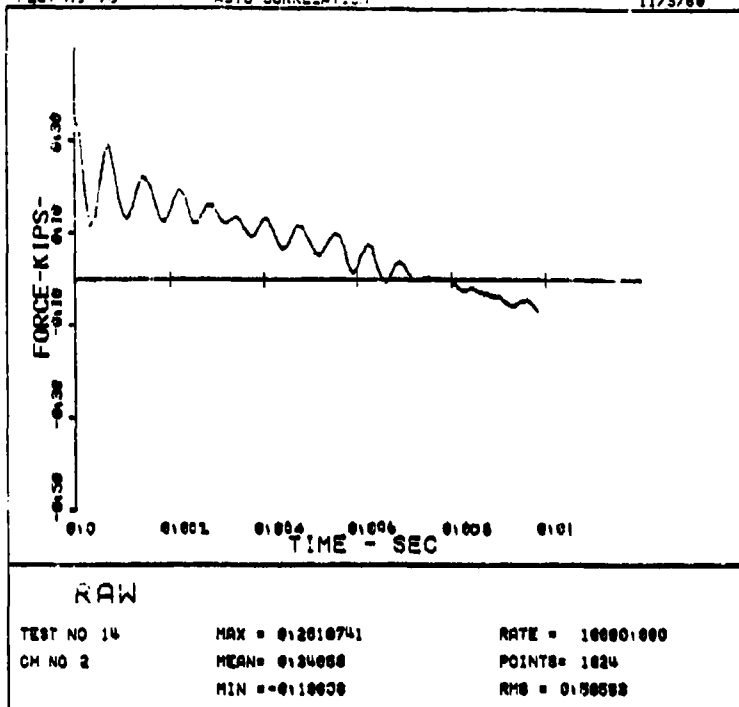
RAW

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PLOT NO 75

AUTO CORRELATION

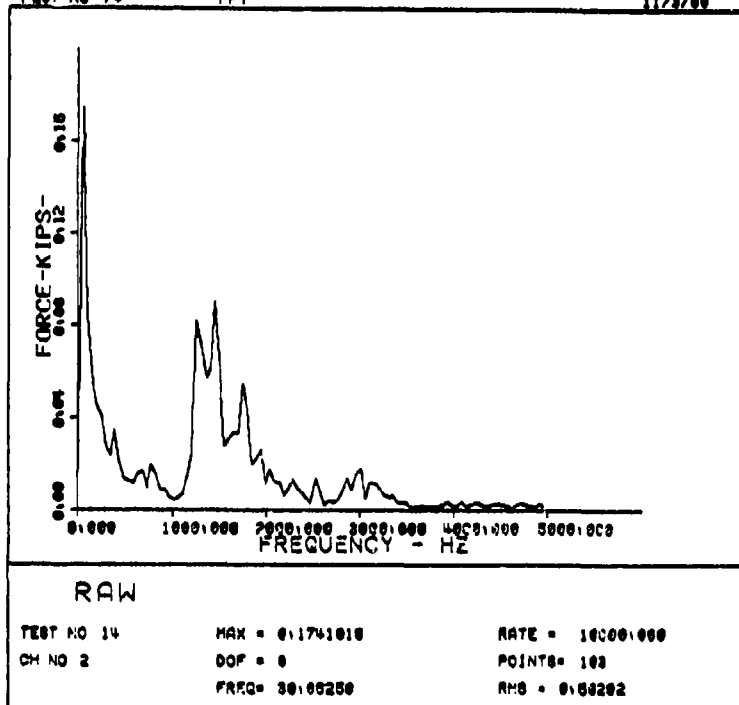
11/3/88

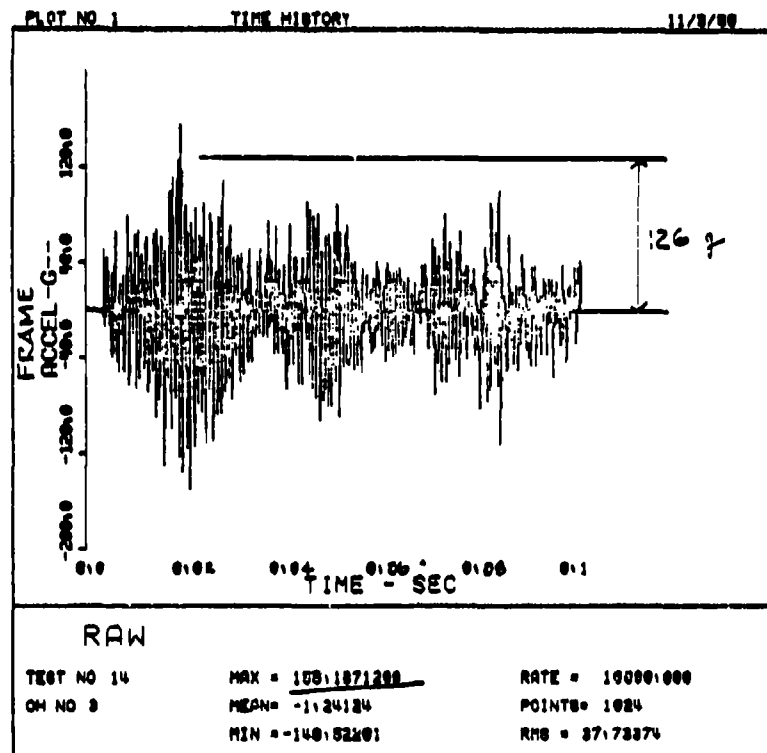
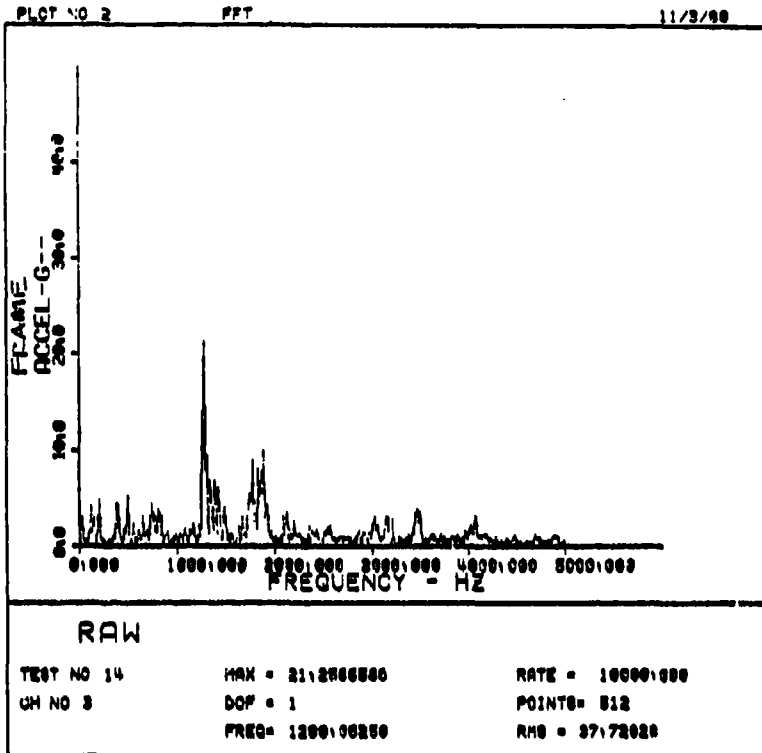


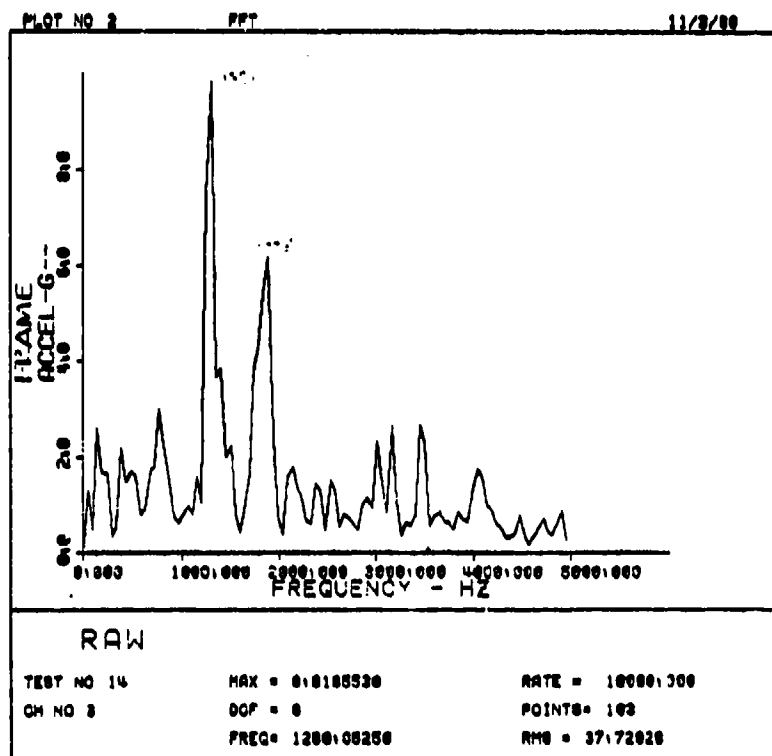
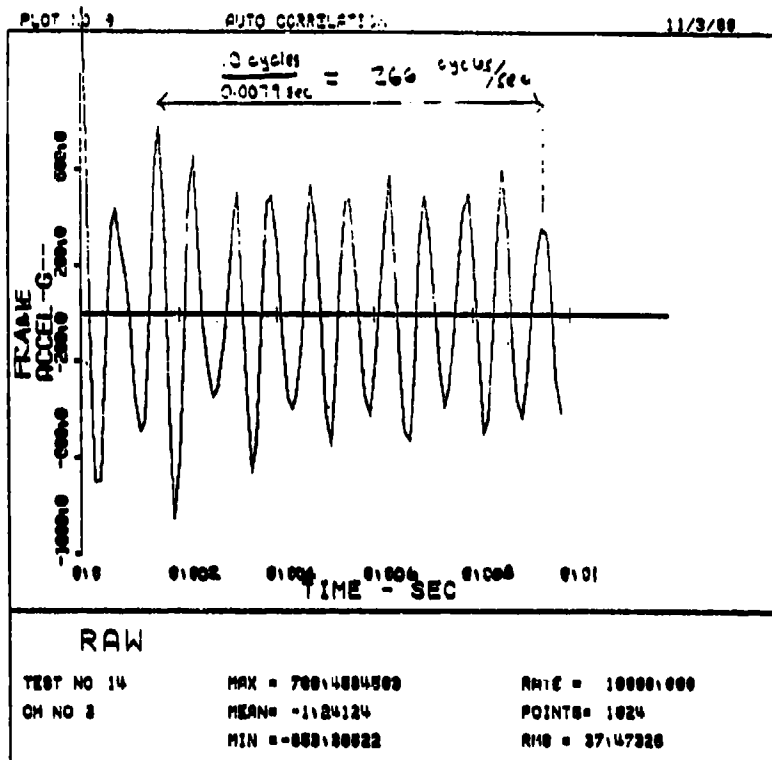
PLOT NO 76

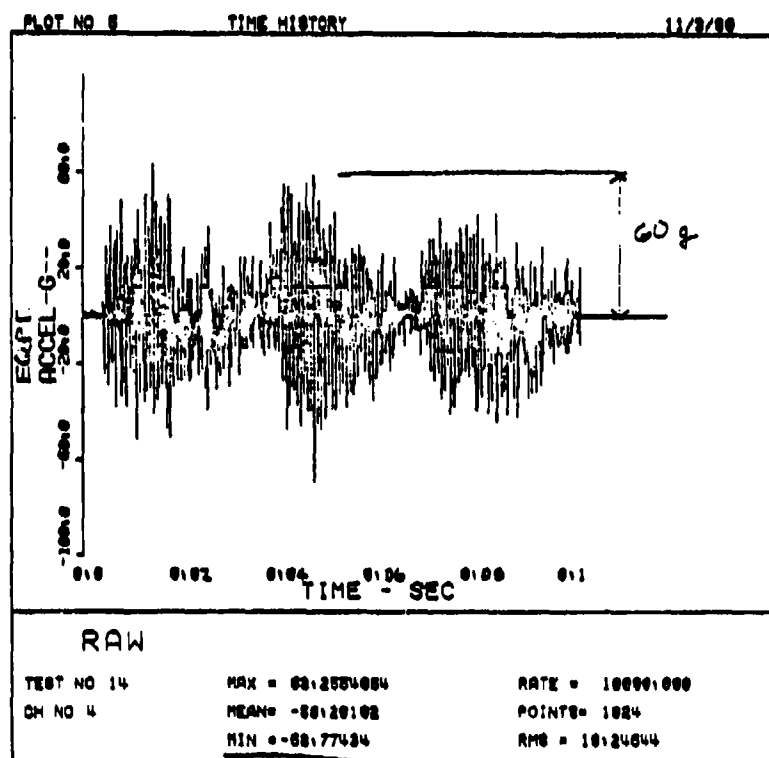
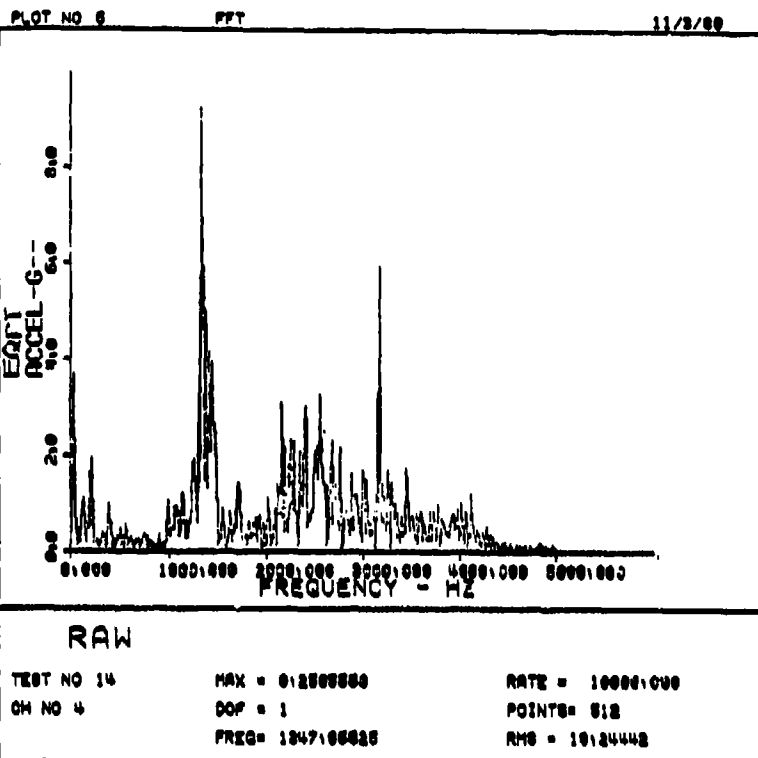
FFT

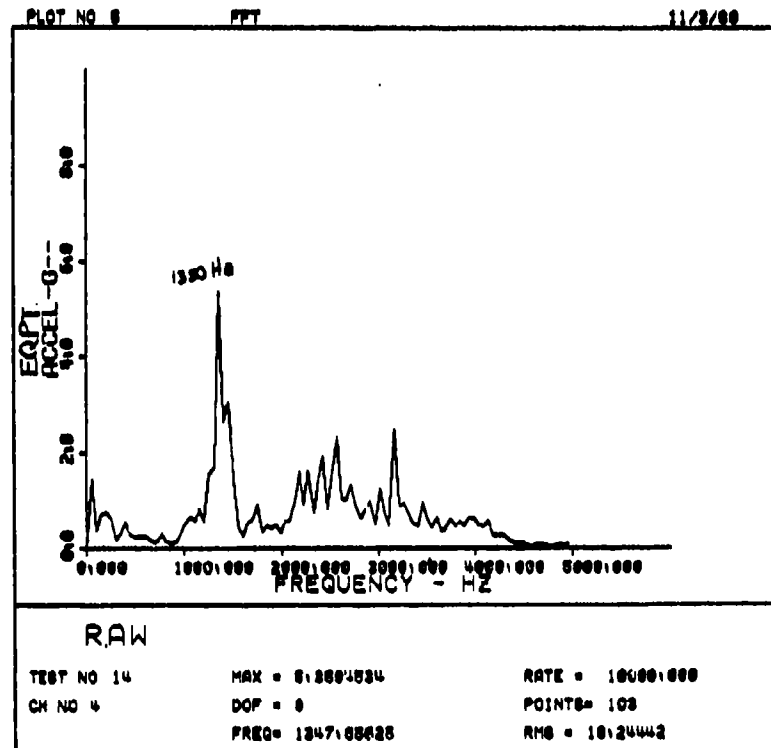
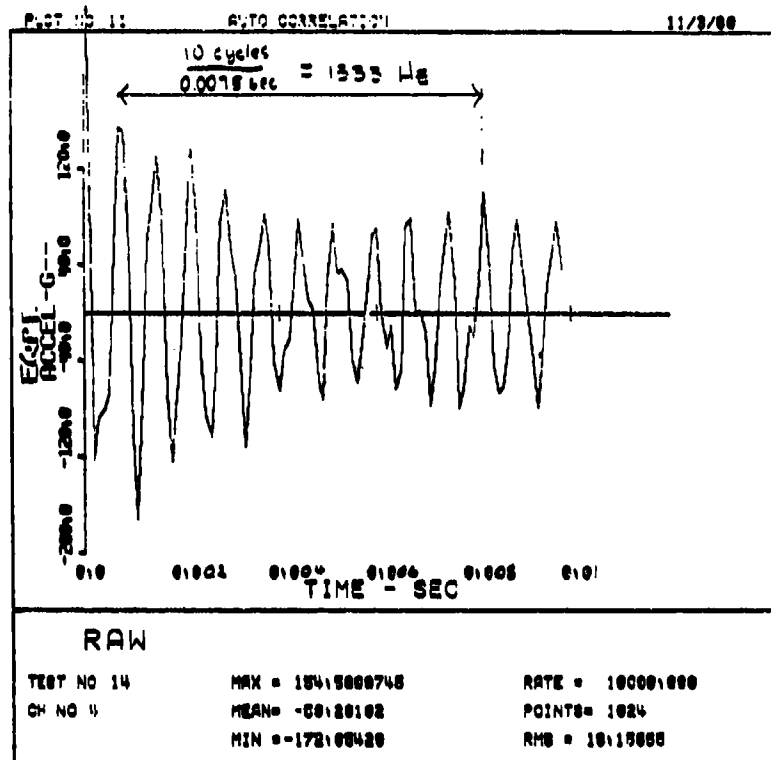
11/3/88







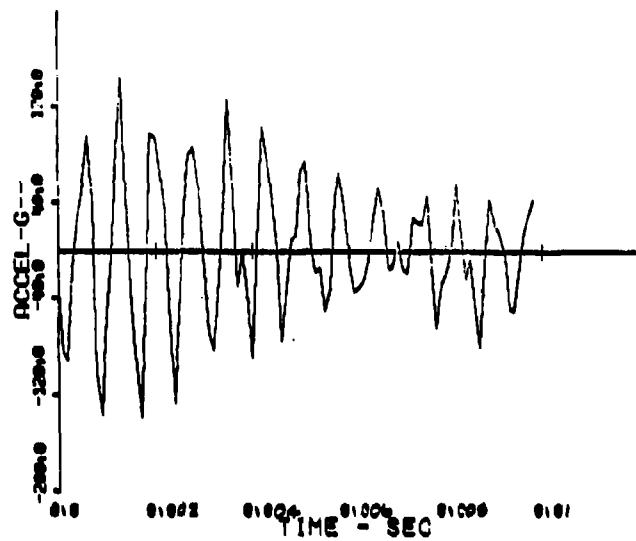




PLOT NO 18

GROSS CORRELATION

11/2/89



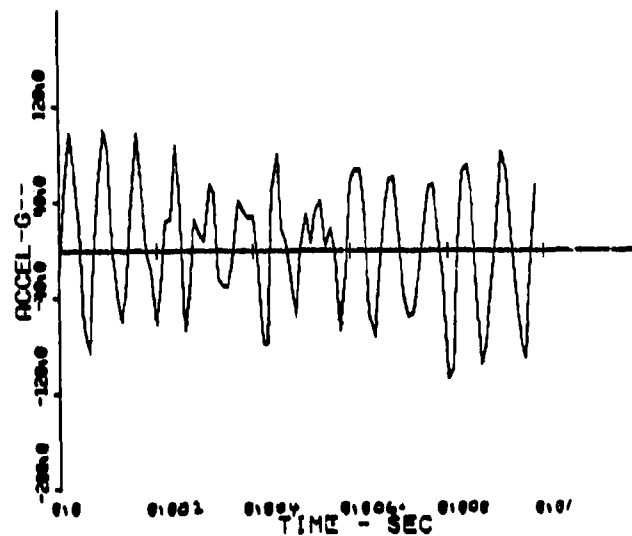
RAW

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PLOT NO 19

GROSS CORRELATION

11/2/89



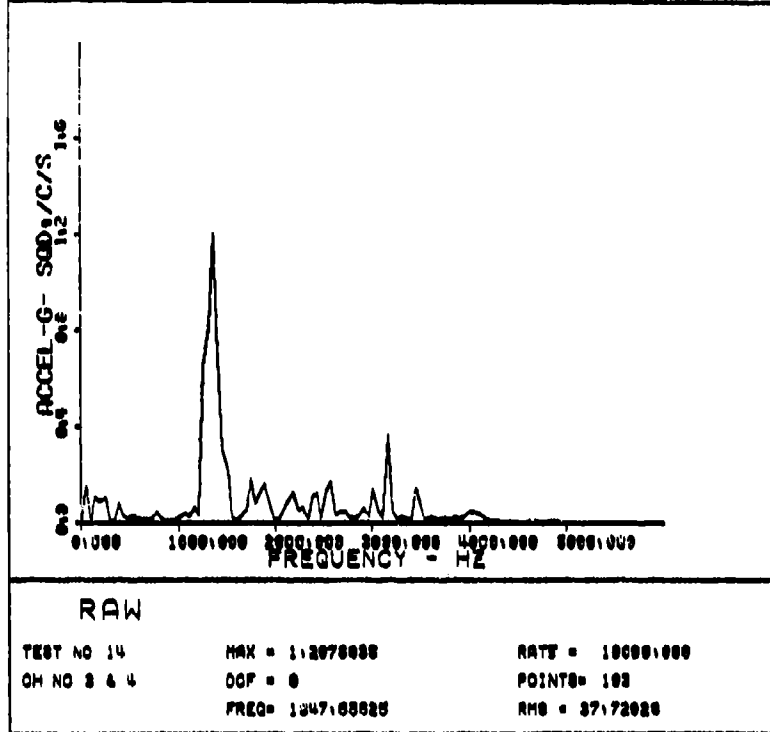
RAW

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PLOT NO 4

GSD

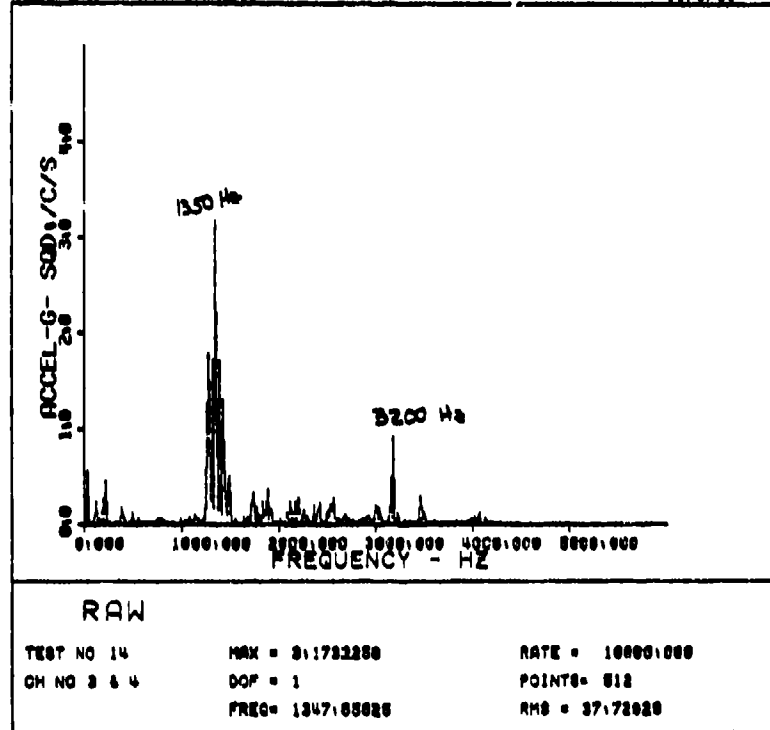
11/3/88



PLOT NO 4

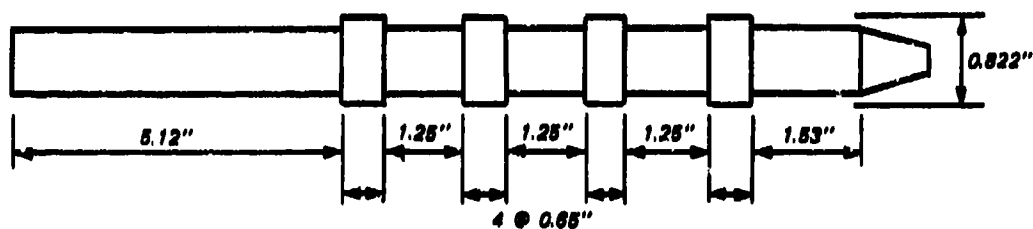
GSD

11/3/88



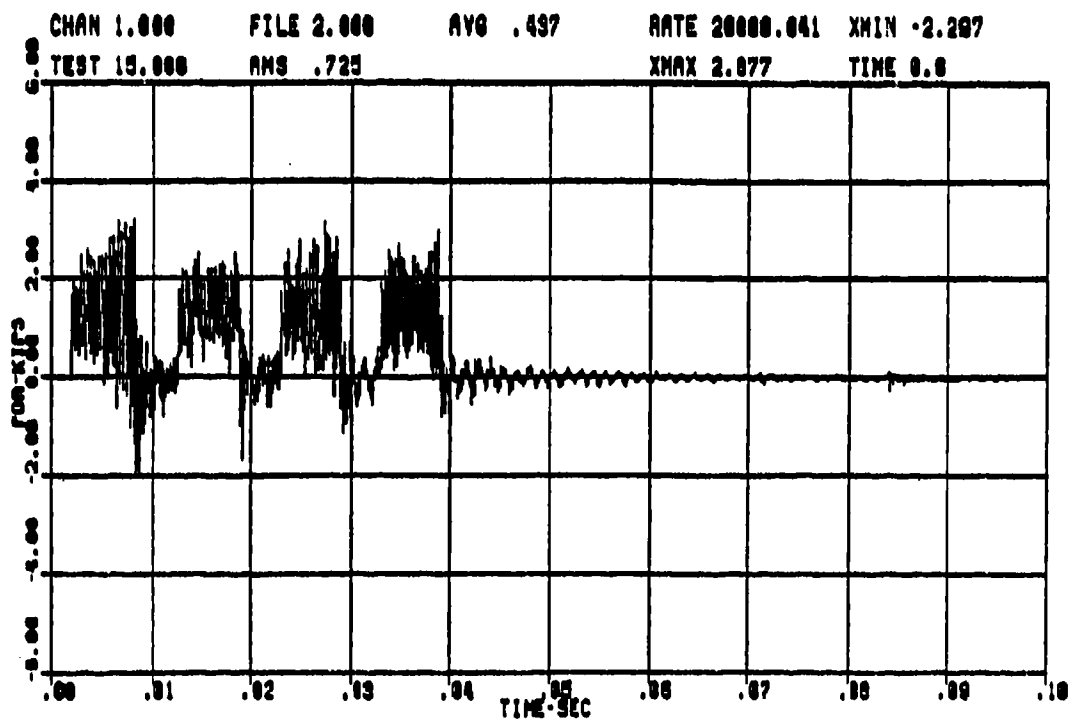
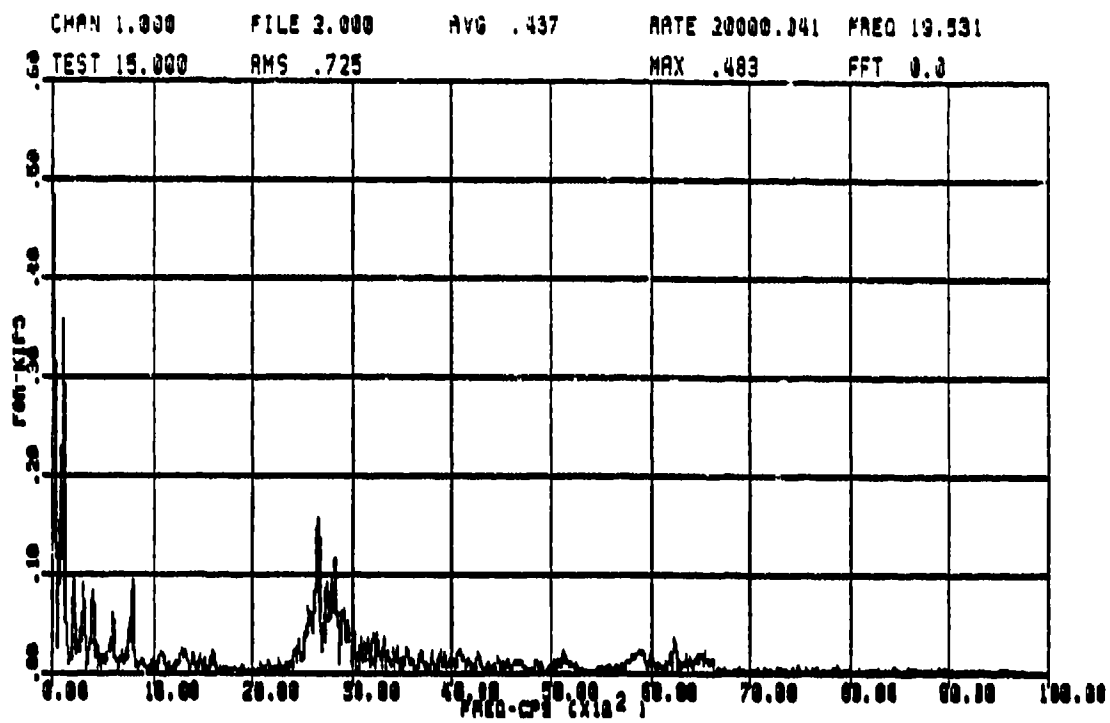
APPENDIX B: TEST 15 DATA

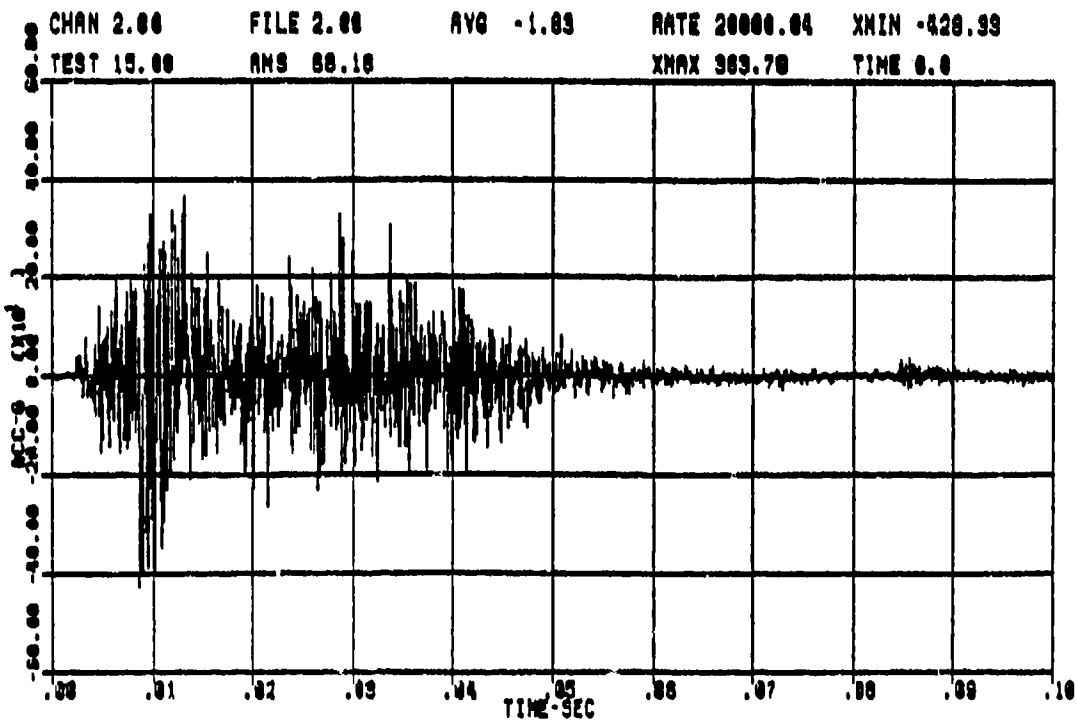
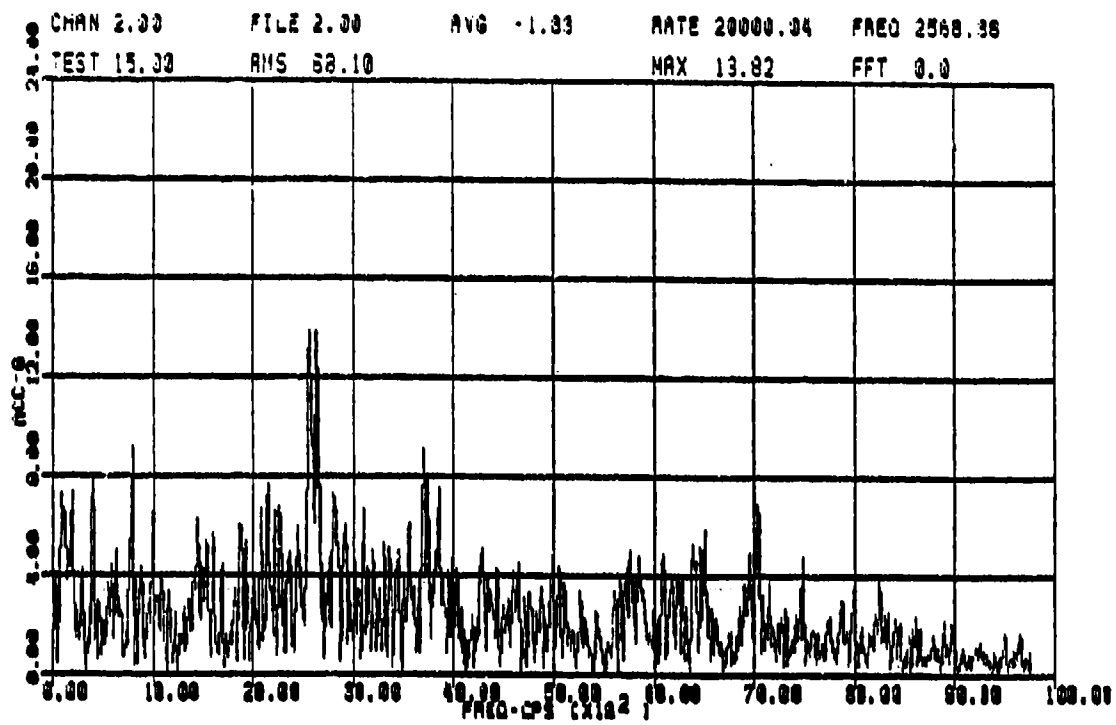
Test 15
Equipment Rack Hard-Mounted
AN/GRC-103 in Rack, Off-Line

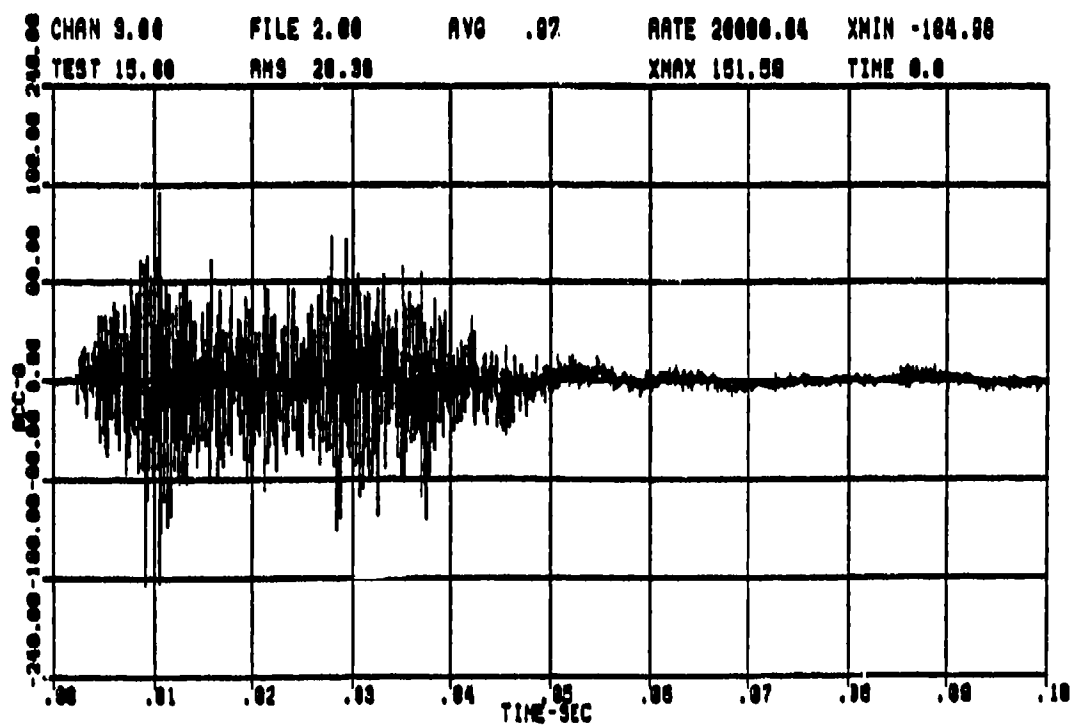
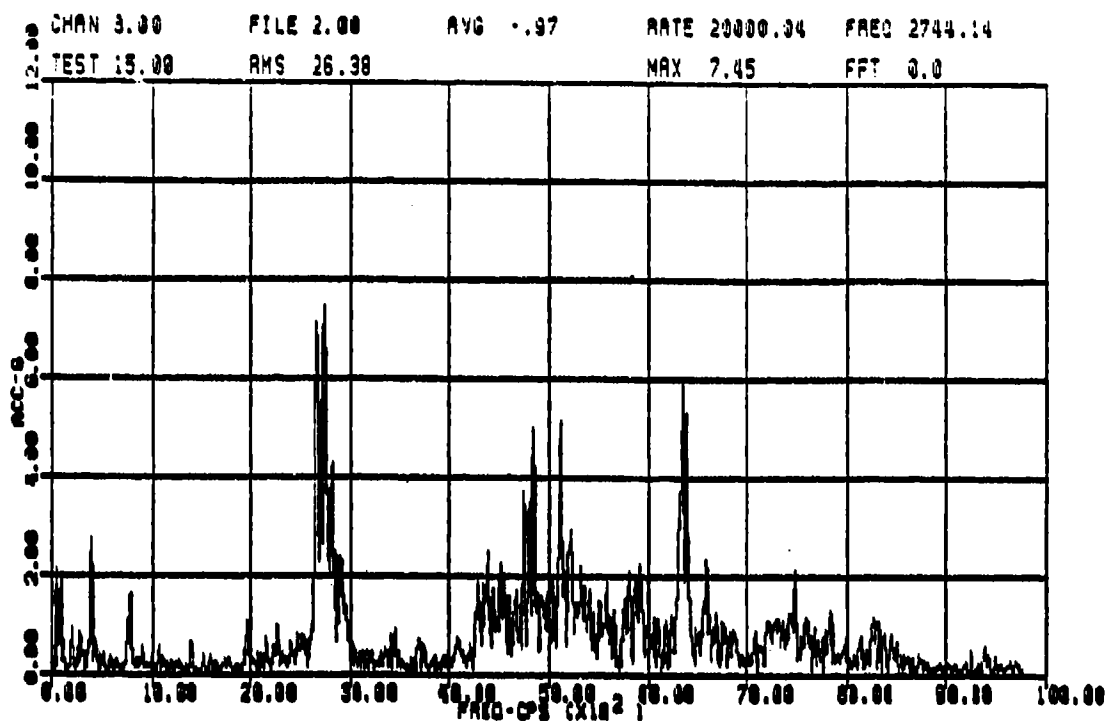


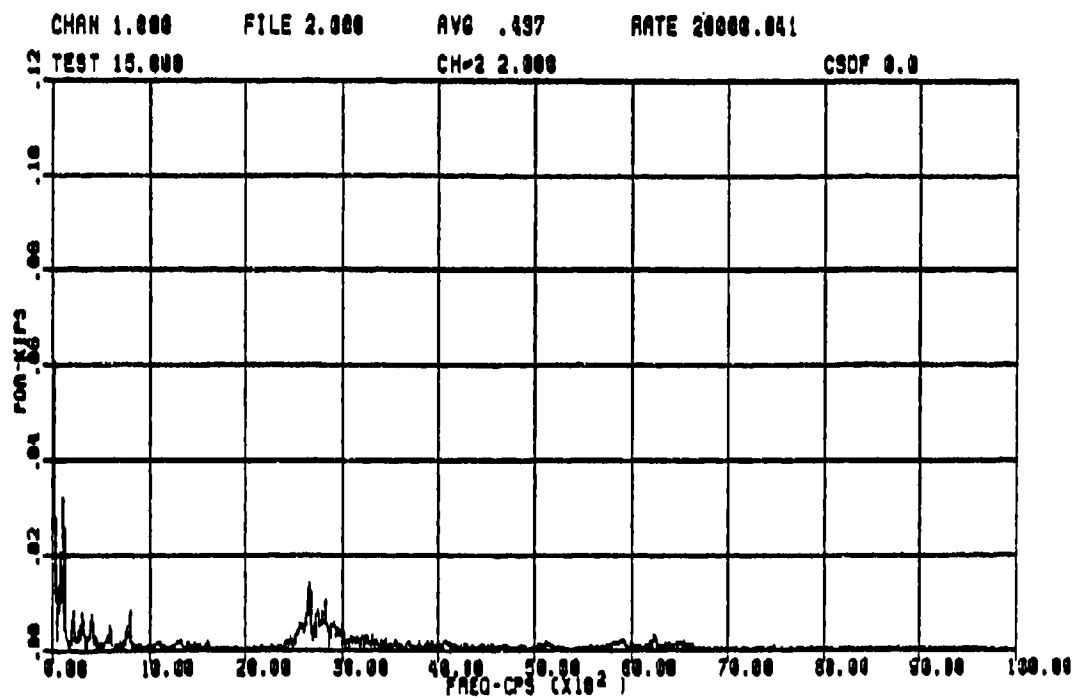
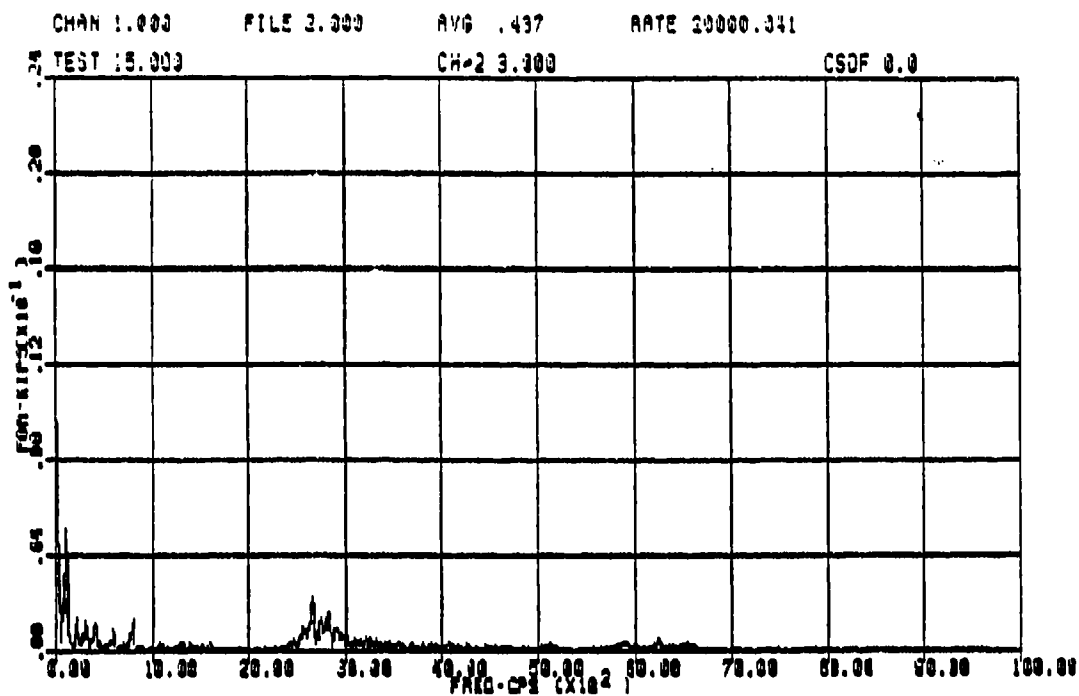
PULSE TRAIN - TEST 16

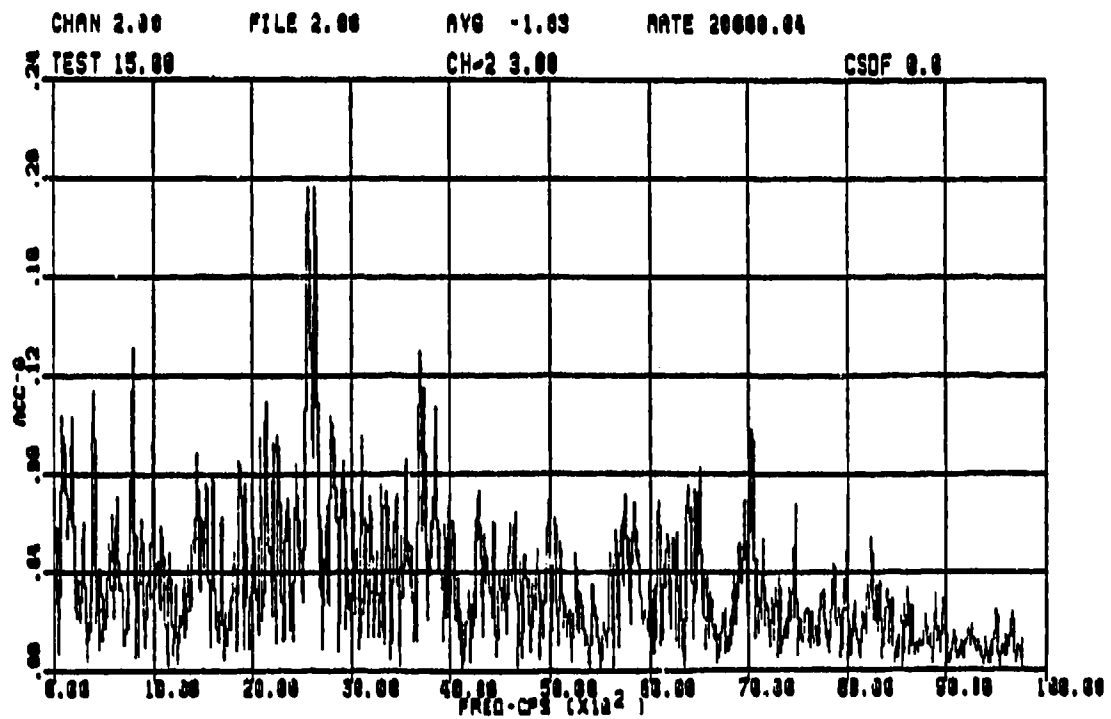
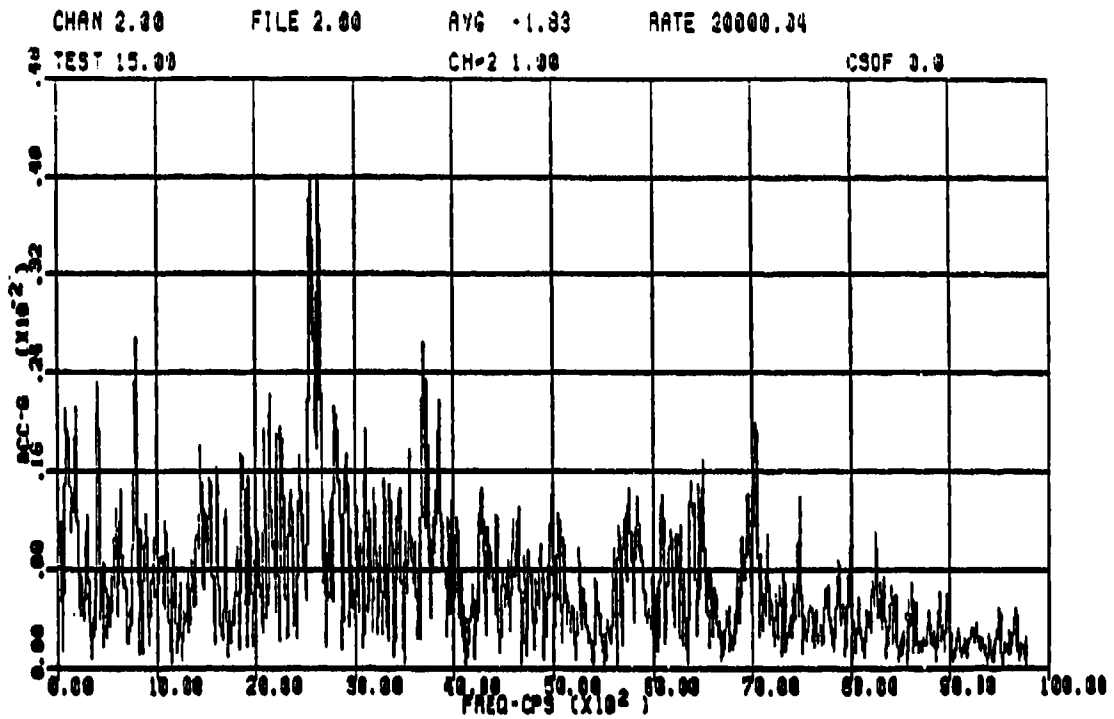
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #6%

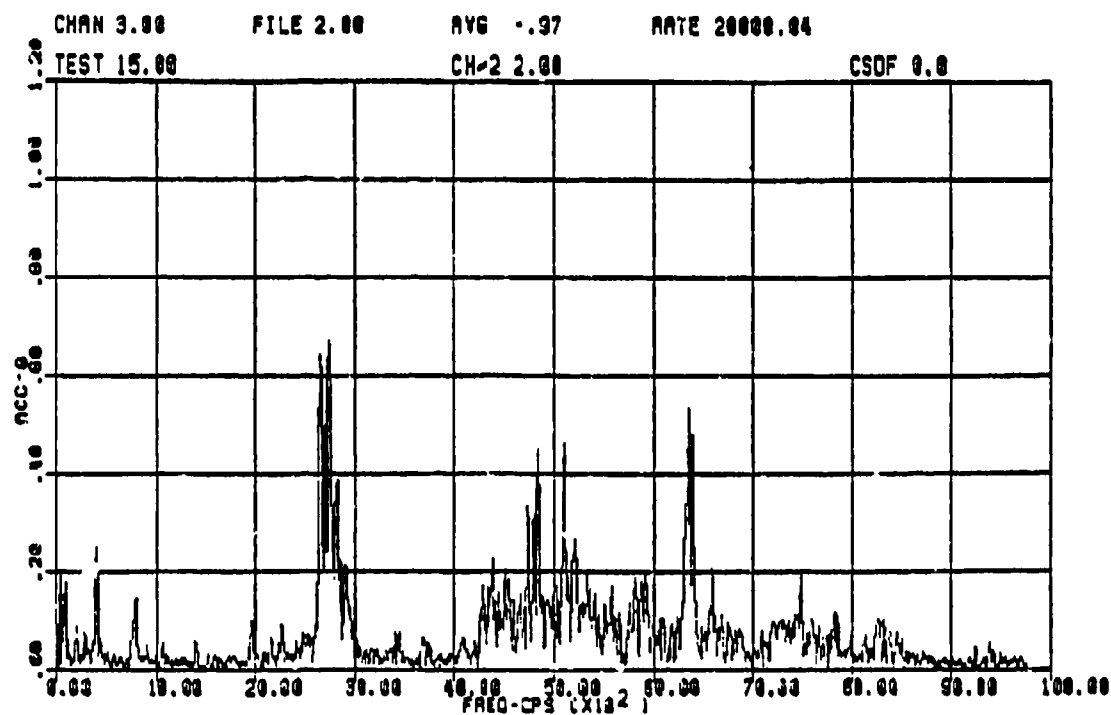
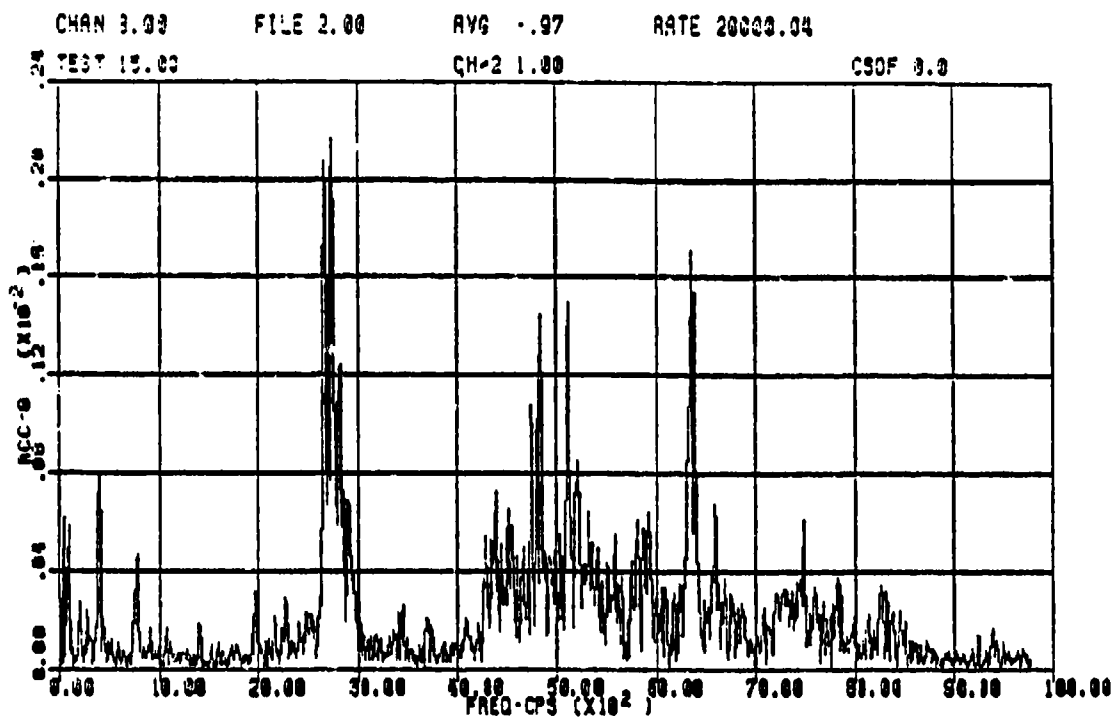








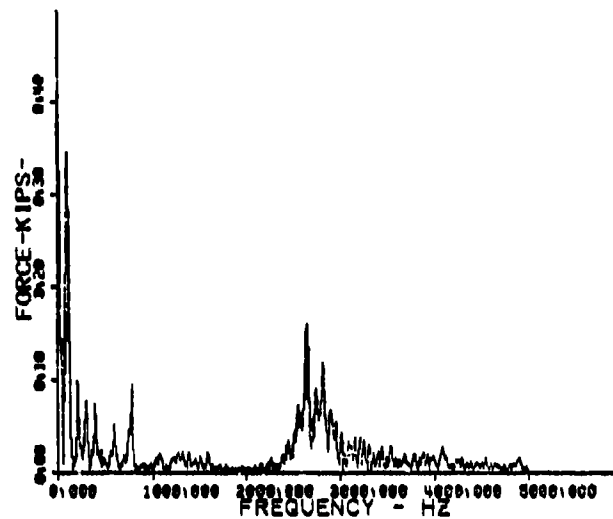




PLOT NO 92

FFT

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RAW

TEST NO 18

MAX = 0.4073482

RATE = 10000.000

CH NO 2

DOF = 1

POINTS= 512

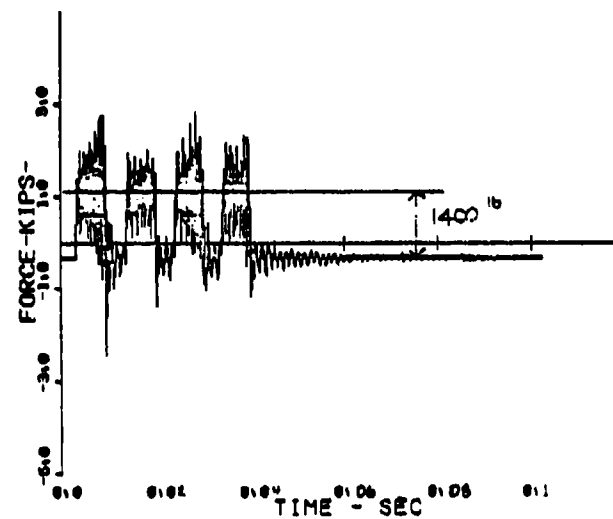
FREQ= 10.53125

RMS = 0.71012

PLOT NO 81

TIME HISTORY

11/3/89



RAW

TEST NO 18

MAX = 2.0300021

RATE = 10000.000

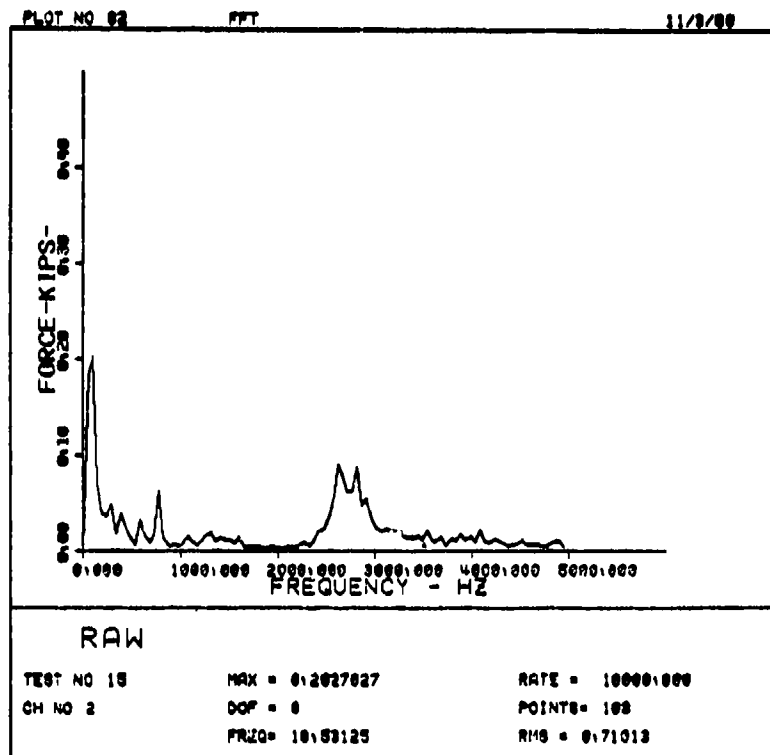
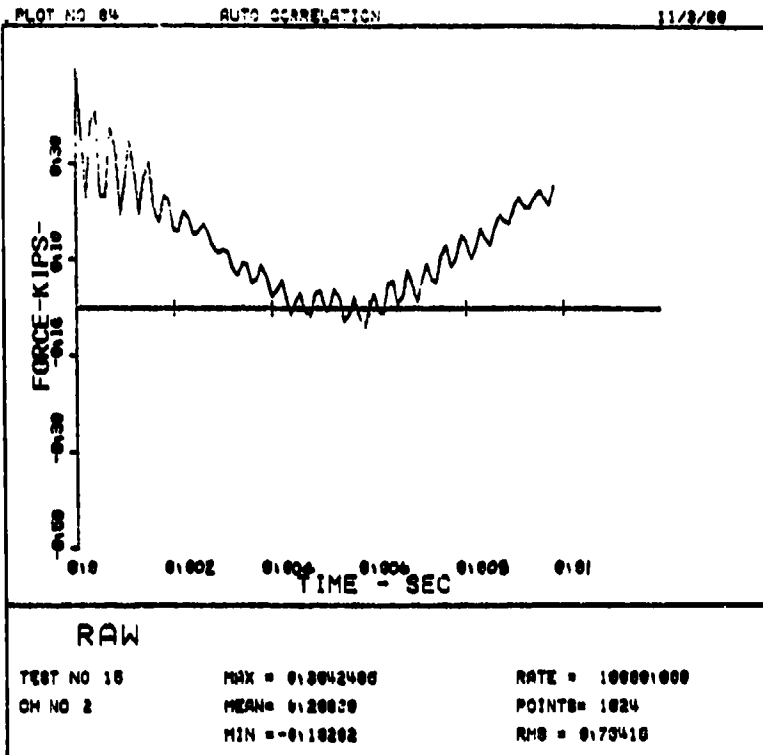
CH NO 2

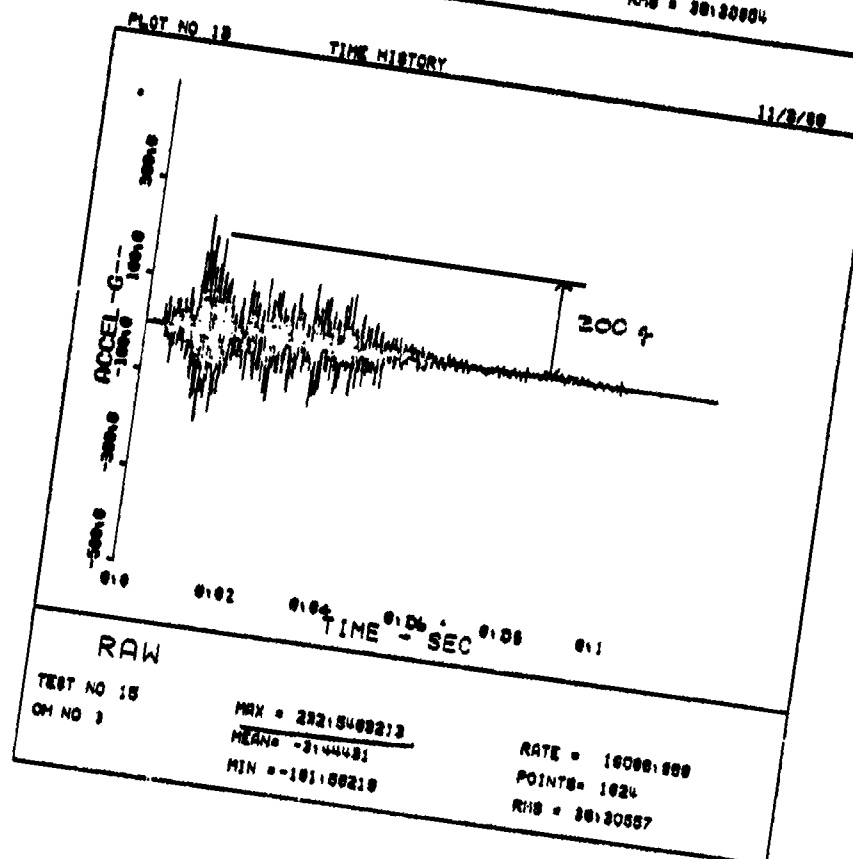
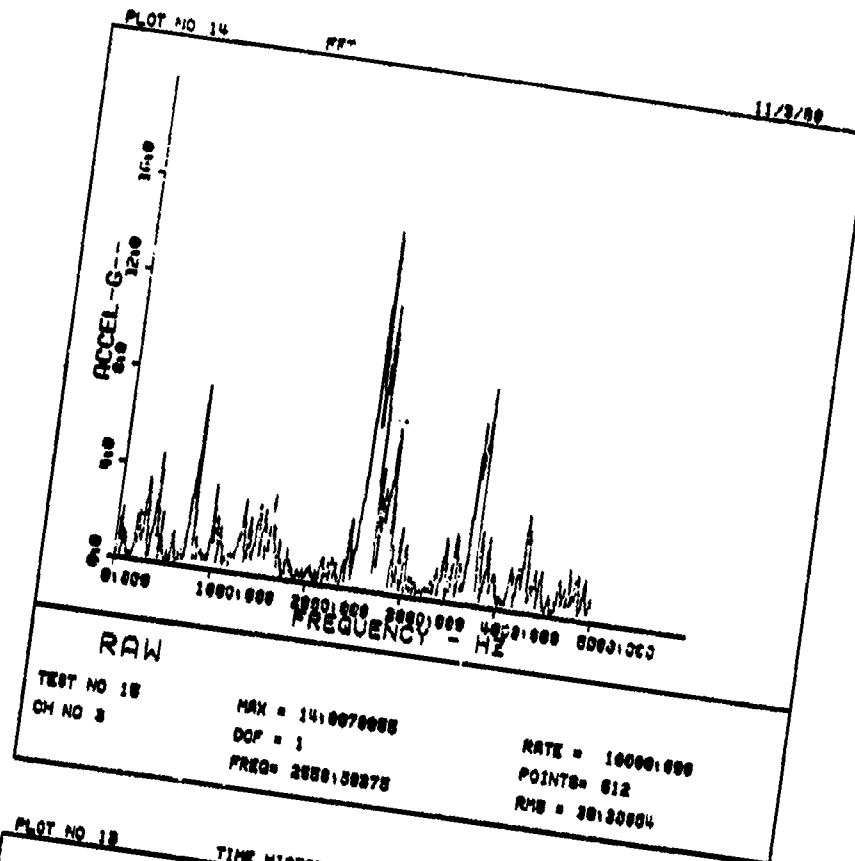
MEAN= 0.20000

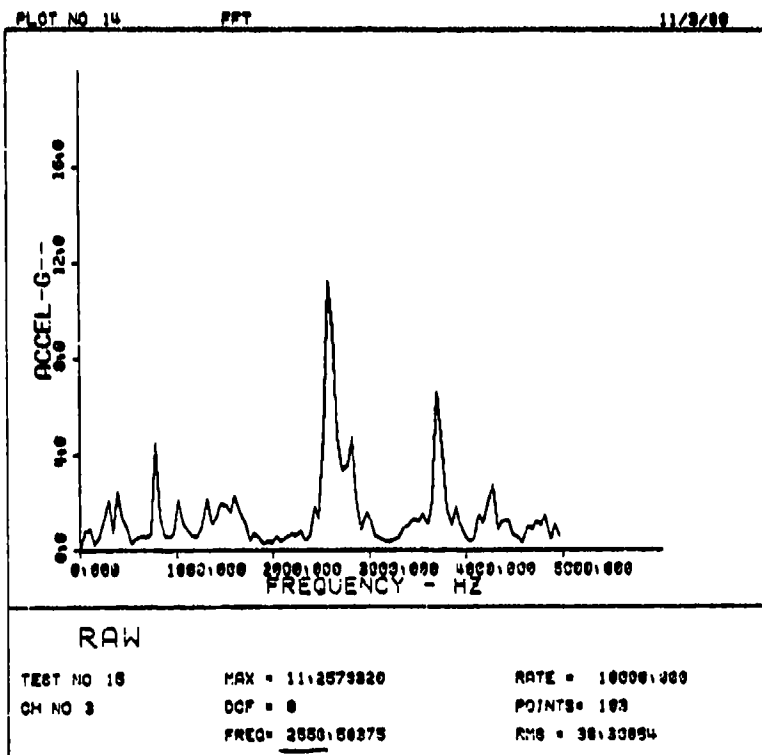
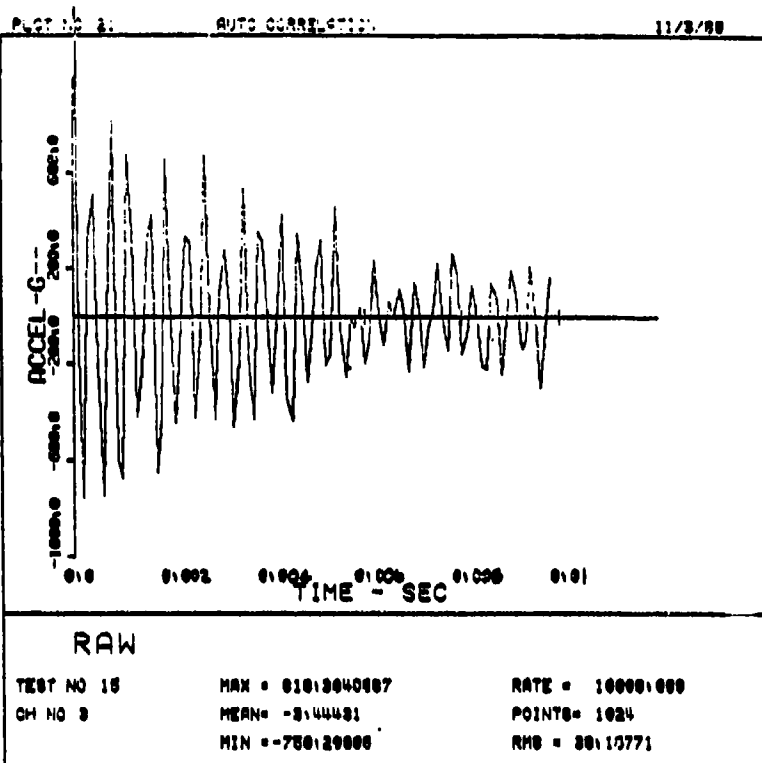
POINTS= 1024

MIN = -2.144001

RMS = 0.71021



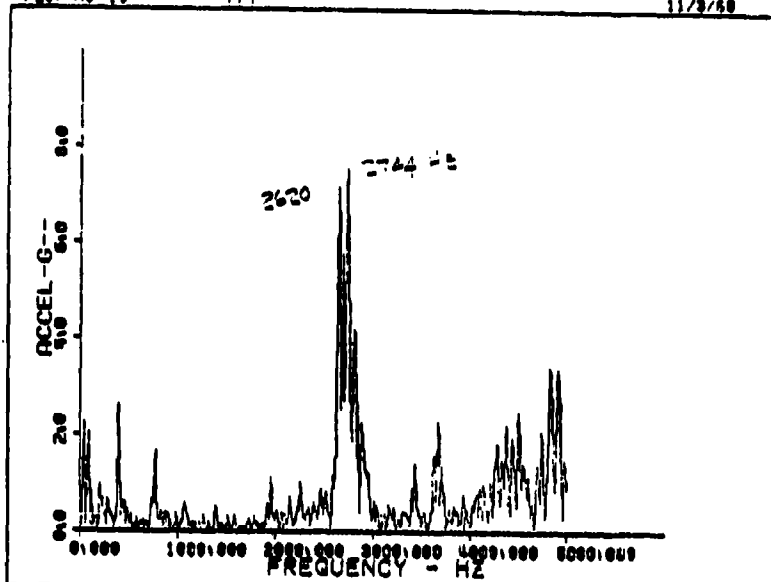




PLOT NO 16

FFT

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RAW

TEST NO 16

MAX = 7.5322966

RATE = 10000.000

CH NO 4

DOP = 1

POINTS = 512

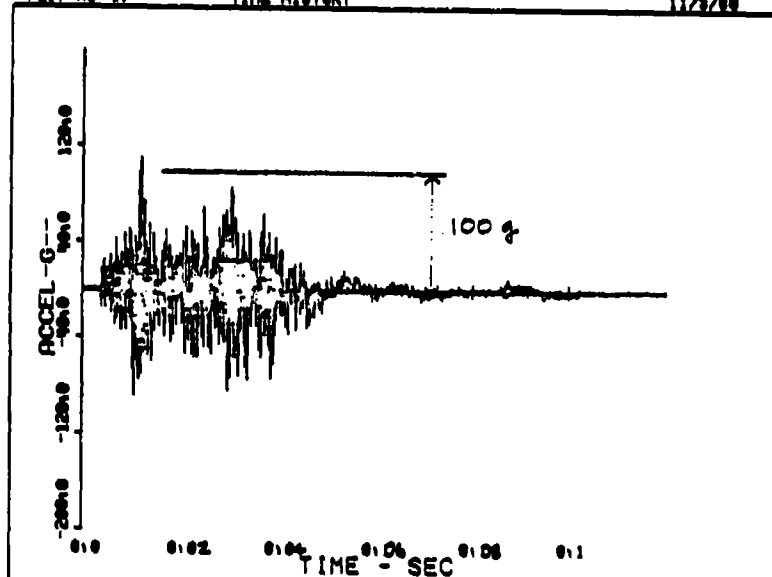
FREQ = 2744.14062

RMS = 16.77581

PLOT NO 17

TIME HISTORY

11/3/68



RAW

TEST NO 16

MAX = 100.6579402

RATE = 10000.000

CH NO 4

MEAN = -51.13047

POINTS = 1024

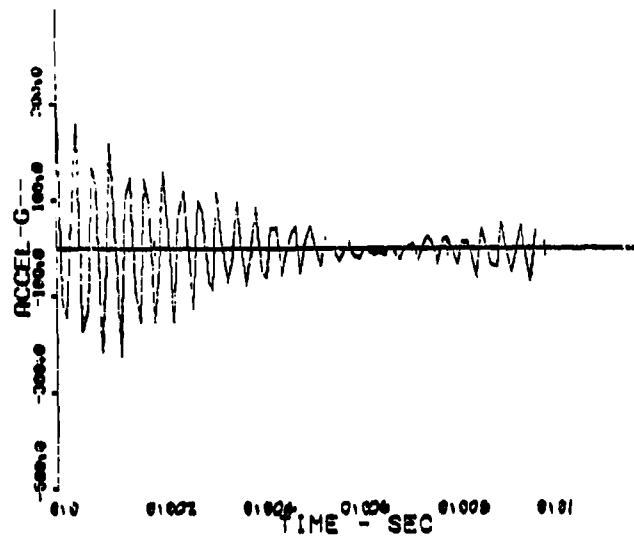
MIN = -66.66520

RMS = 19.77966

PLOT NO 23

RAW CORRELATION

11/3/69



RAW

TEST NO 18
CH NO 4

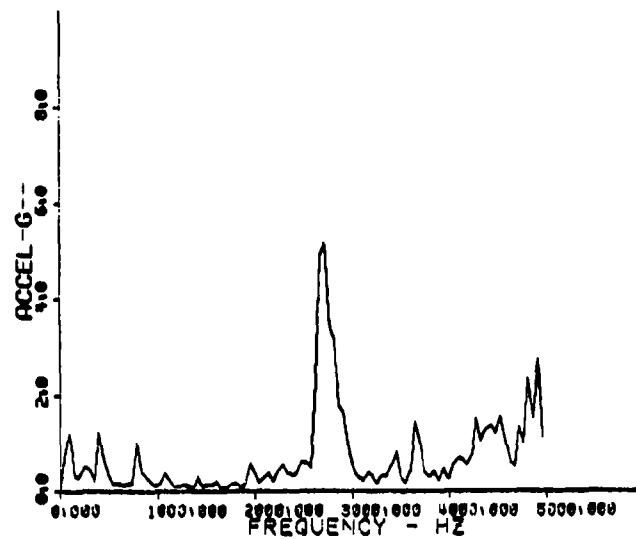
MAX = 2581.8807718
MEAN = -51.12947
MIN = -222.28788

RATE = 10000.000
POINTS = 1024
RMS = 18.76824

PLOT NO 19

FFT

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RAW

TEST NO 18
CH NO 4

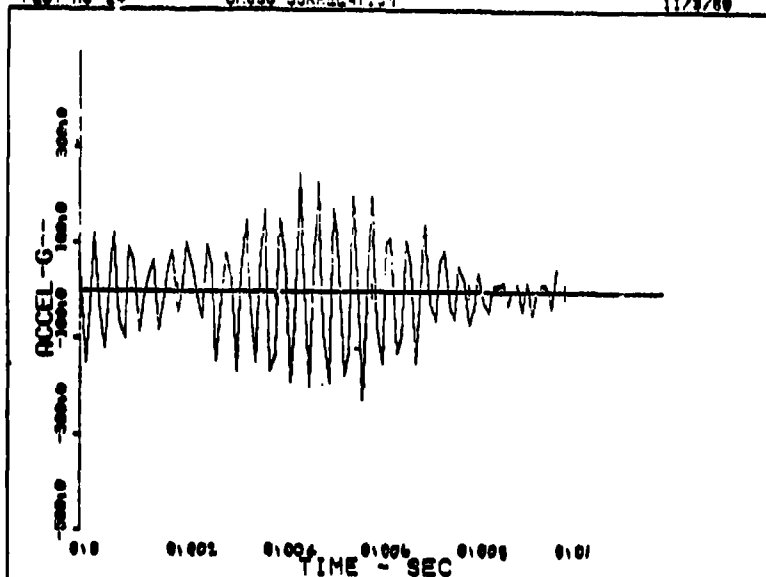
MAX = 5.1788220
DOP = 0
FREQ = 2744.14682

RATE = 10000.000
POINTS = 1024
RMS = 18.77521

PLOT NO 24

GROSS CORRELATION

11/3/89



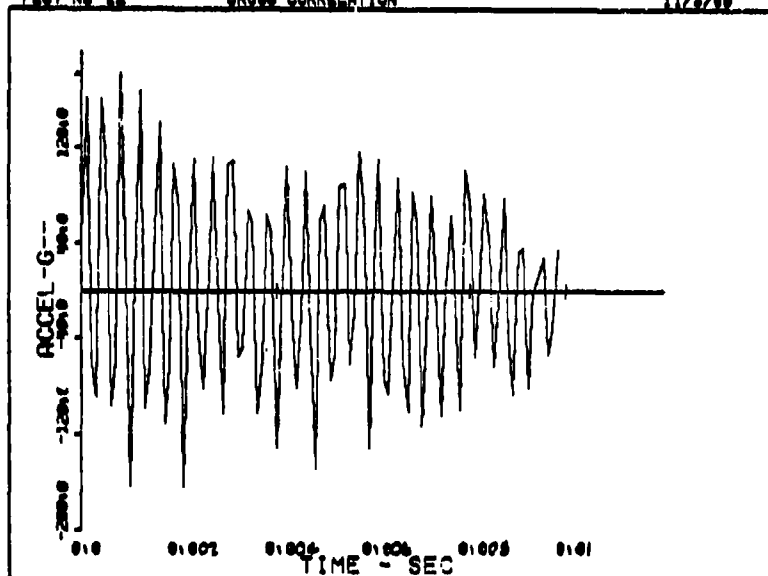
RAW

TEST NO 18
CH NO 4 & 8MAX = 246.888874
MEAN = -81.12847
MIN = -224.41885RATE = 10000.000
POINTS = 1024
RMS = 18.77889

PLOT NO 22

GROSS CORRELATION

11/3/89



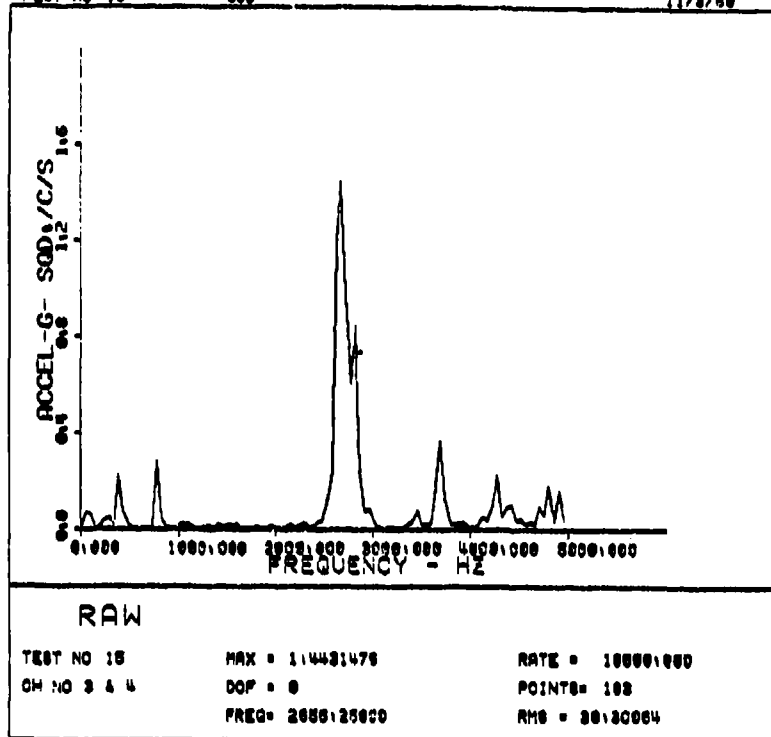
RAW

TEST NO 18
CH NO 3 & 4MAX = 181.888848
MEAN = -31.44431
MIN = -188.82885RATE = 10000.000
POINTS = 1024
RMS = 38.30557

PLOT NO 15

CSD

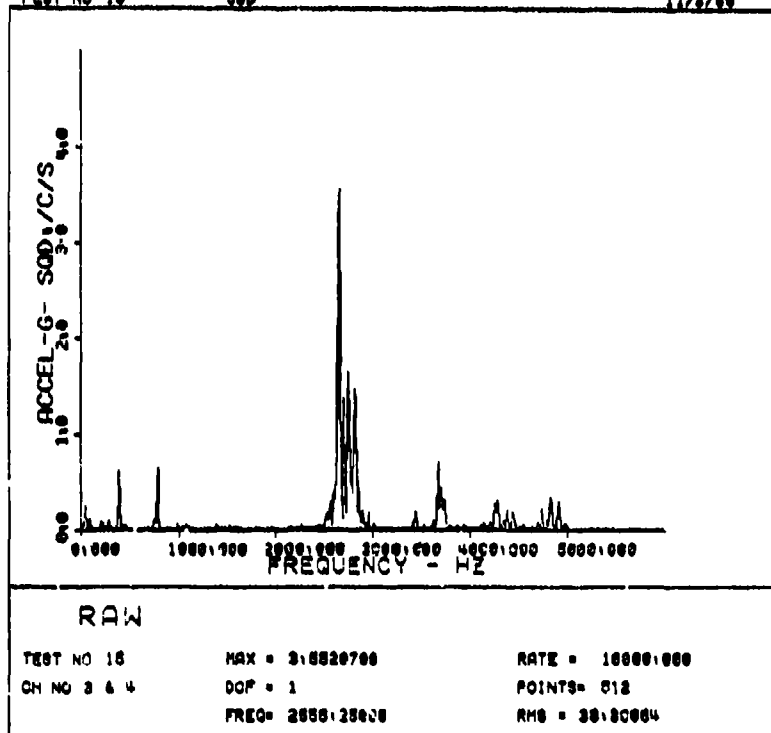
11/8/88



PLOT NO 16

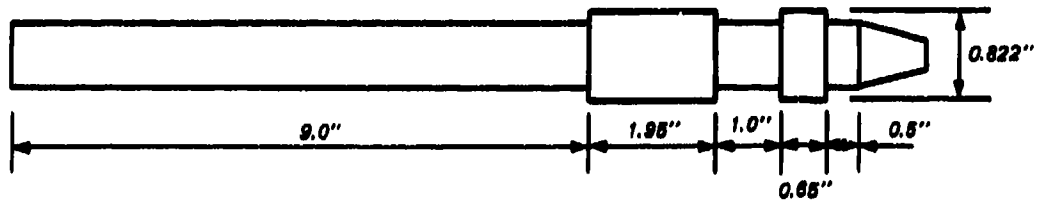
CSD

11/8/88



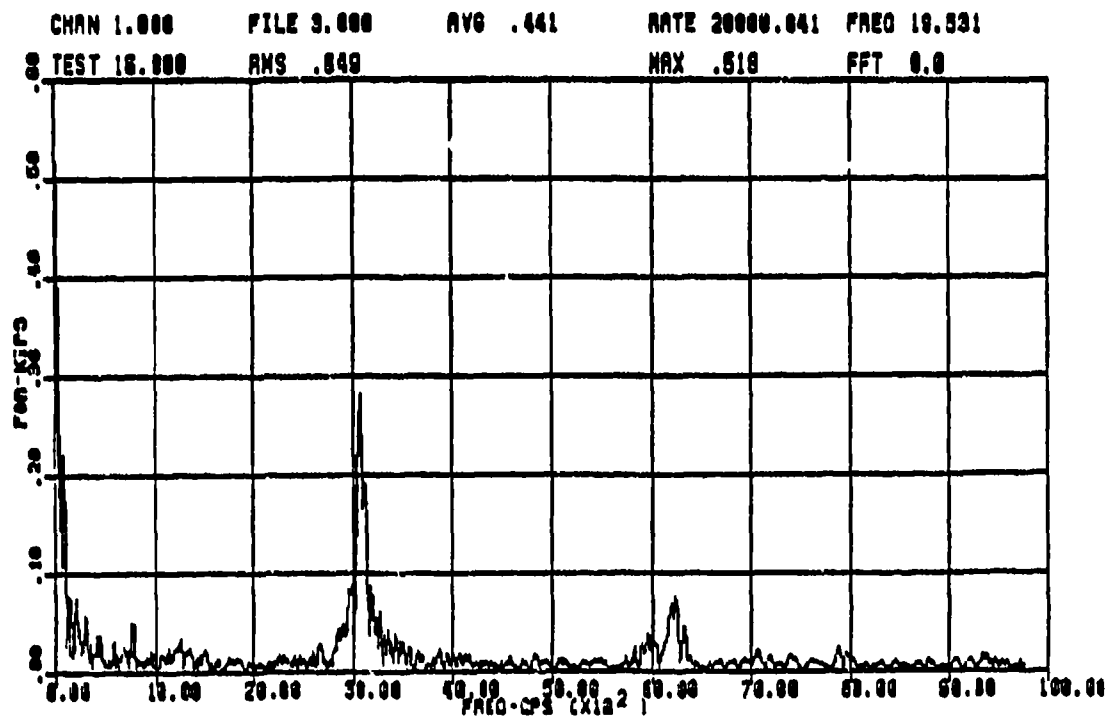
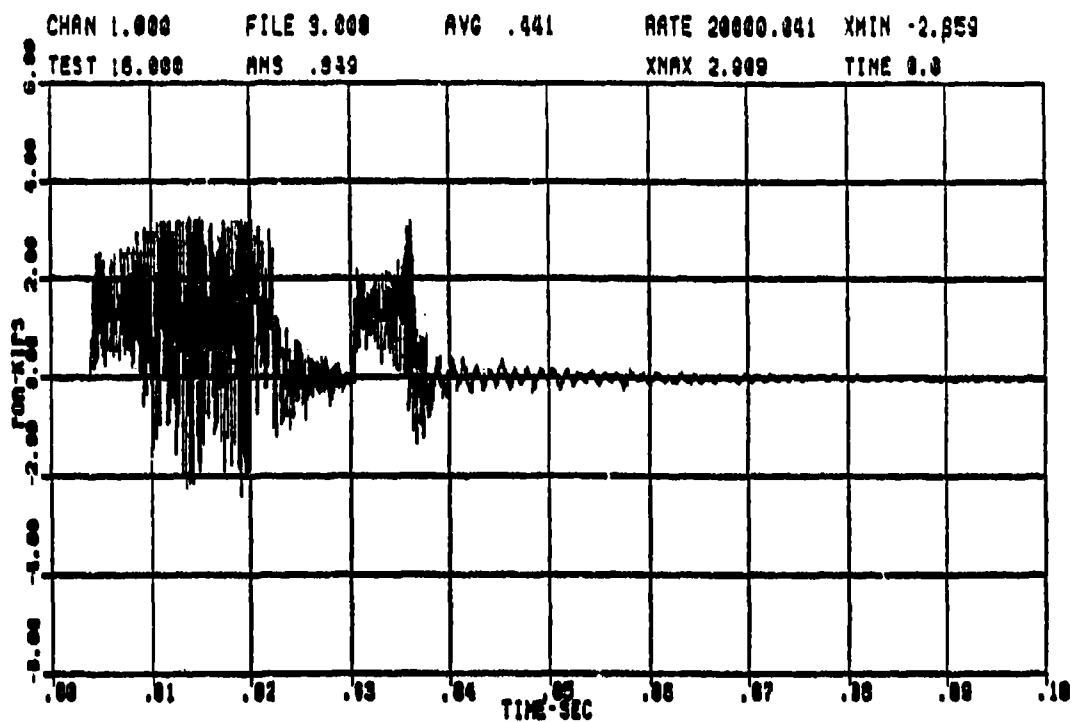
APPENDIX C: TEST 16 DATA

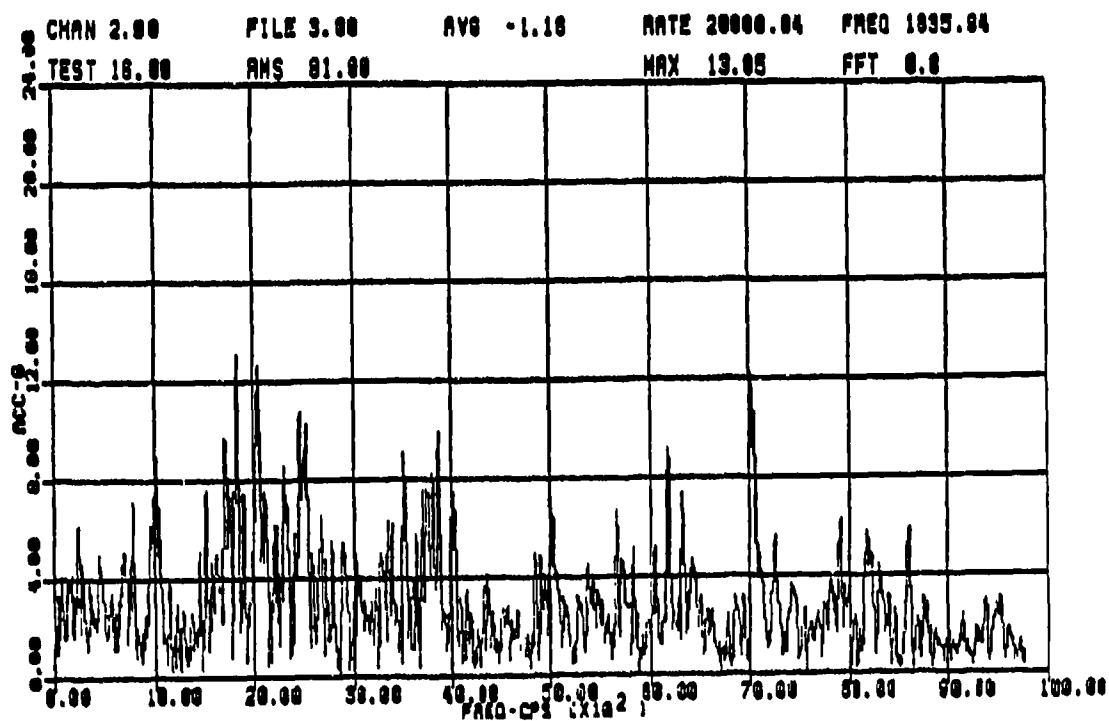
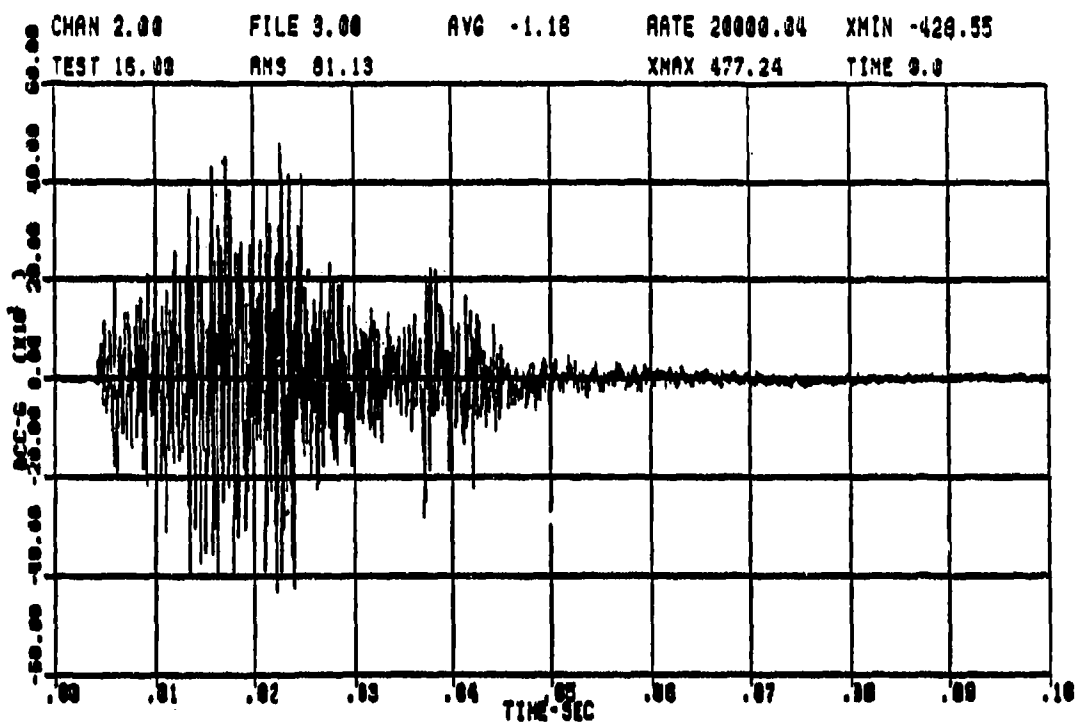
Test 16
Equipment Rack Hard-Mounted
AN/GRC-103 in Rack, Off-Line

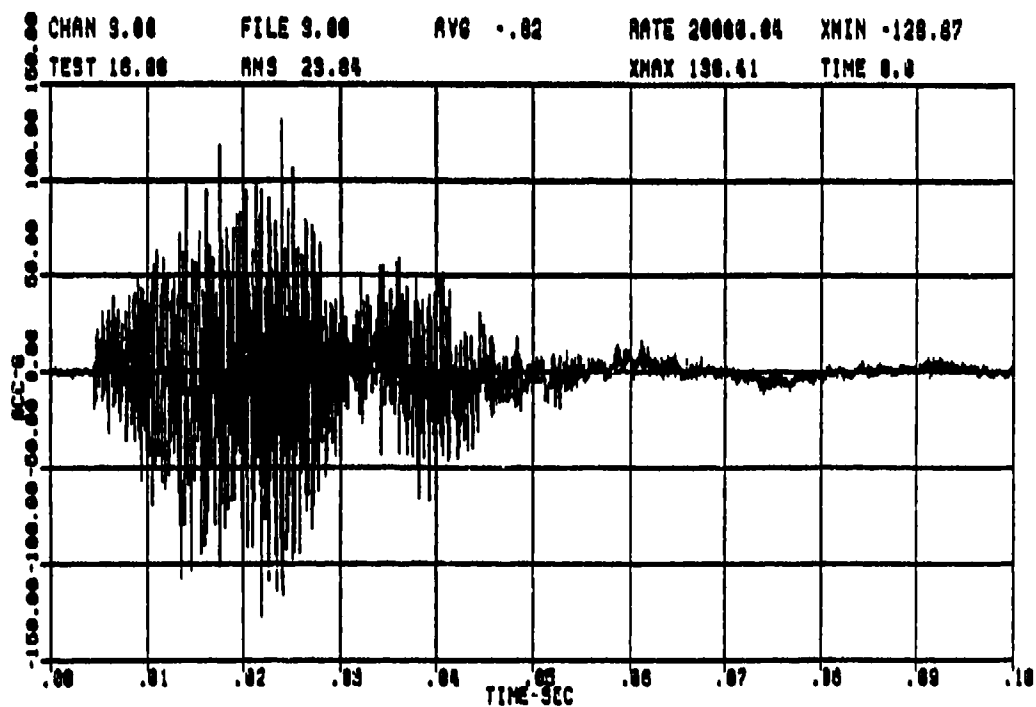
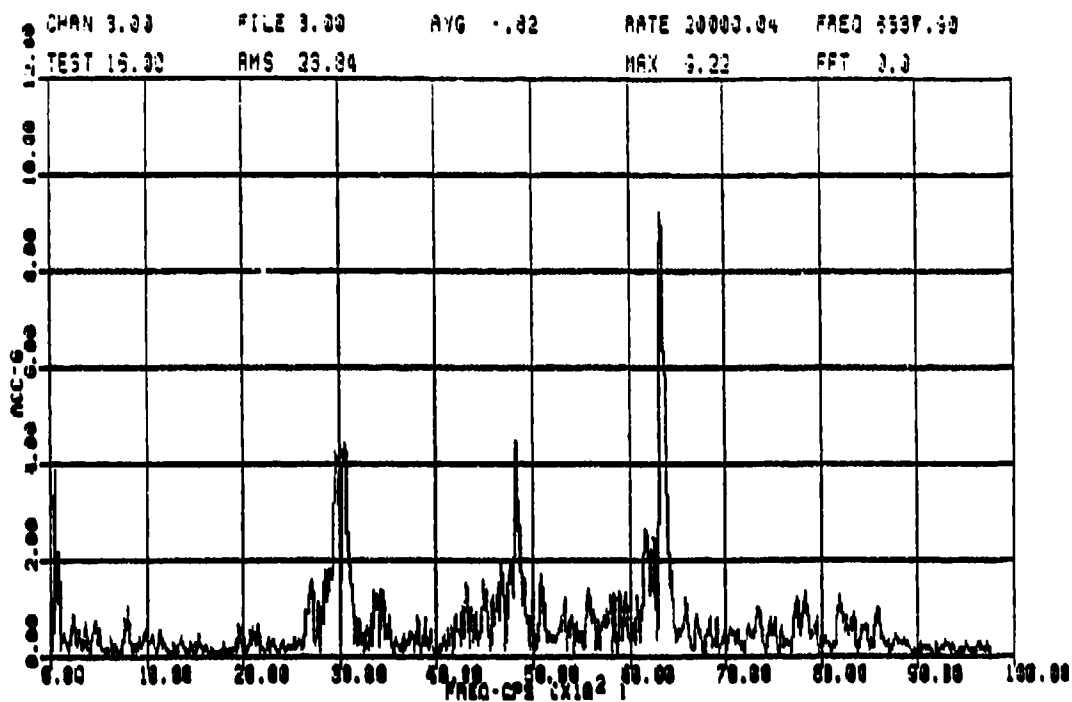


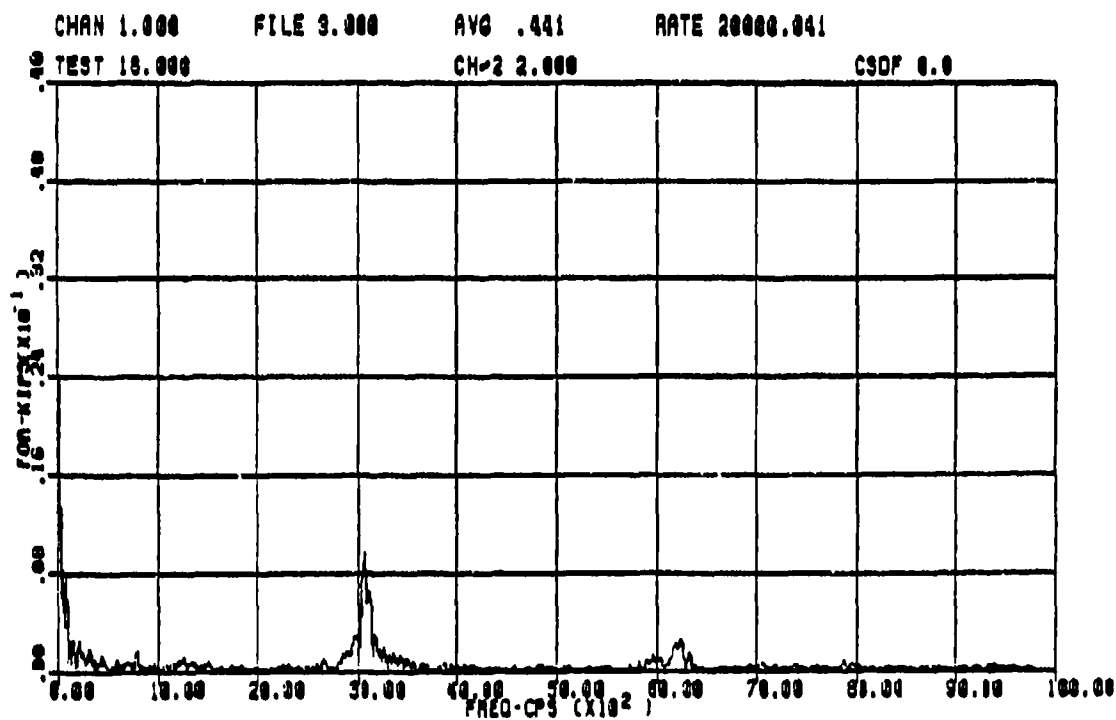
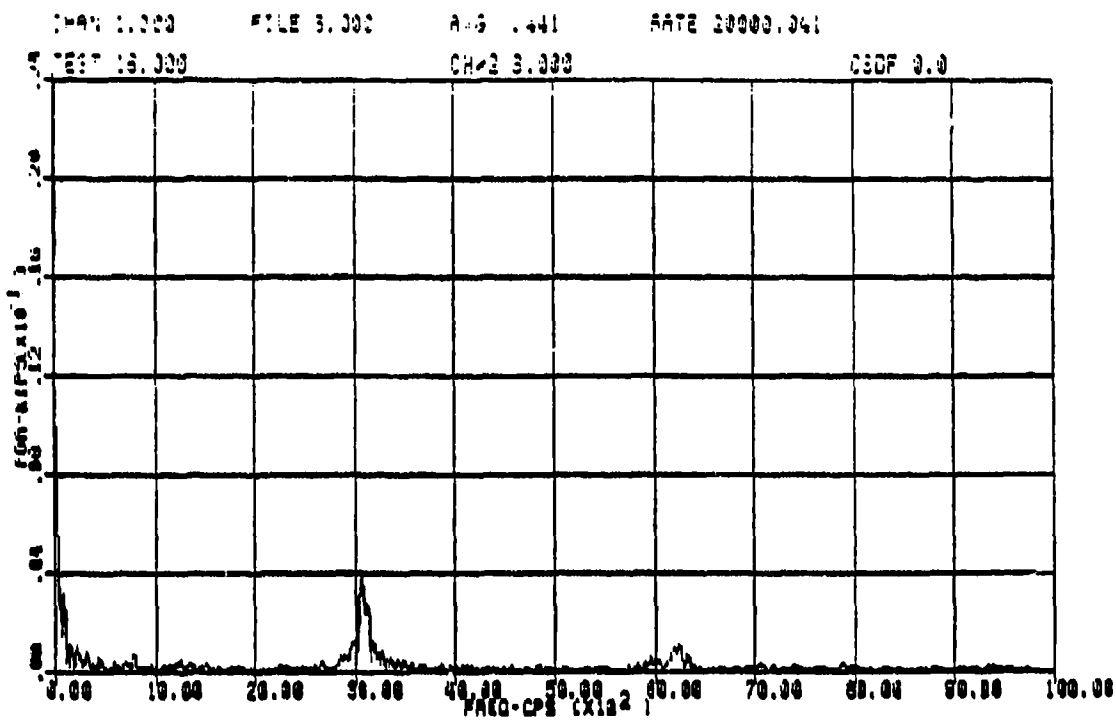
PULSE TRAIN - TEST 16

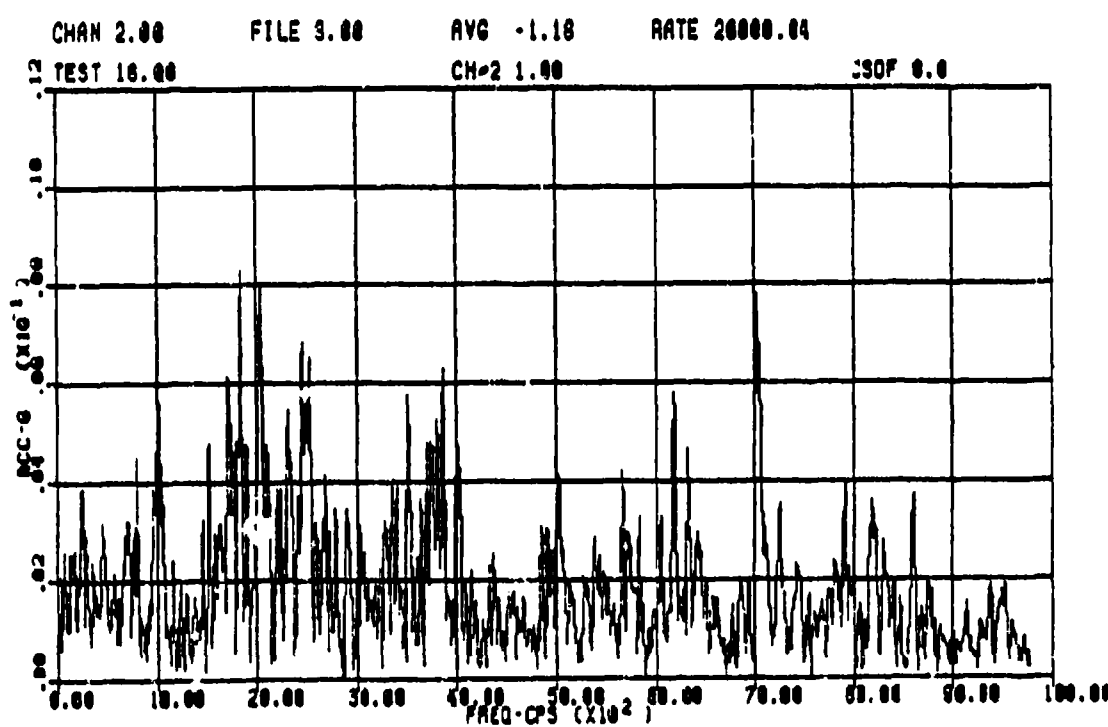
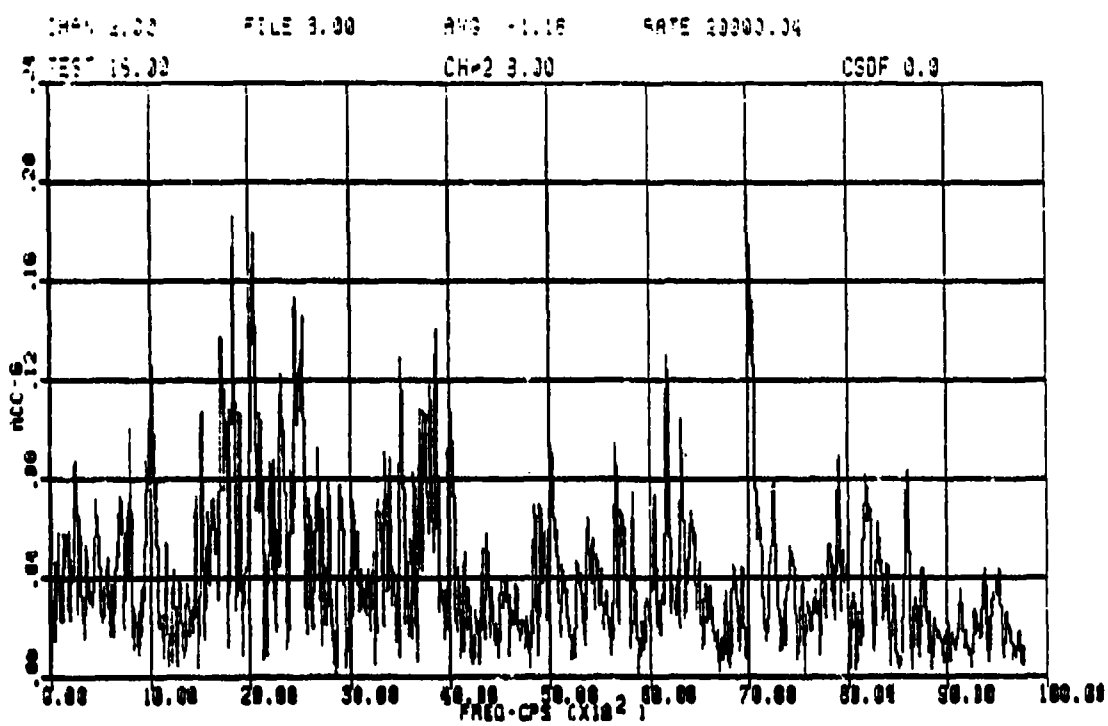
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #8%

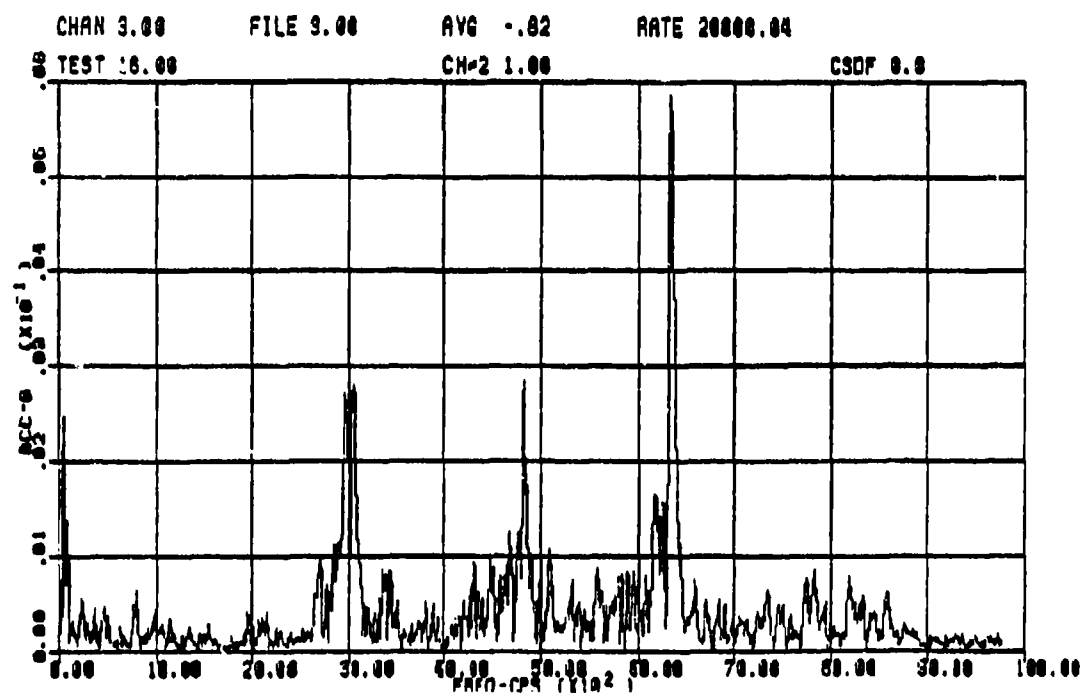
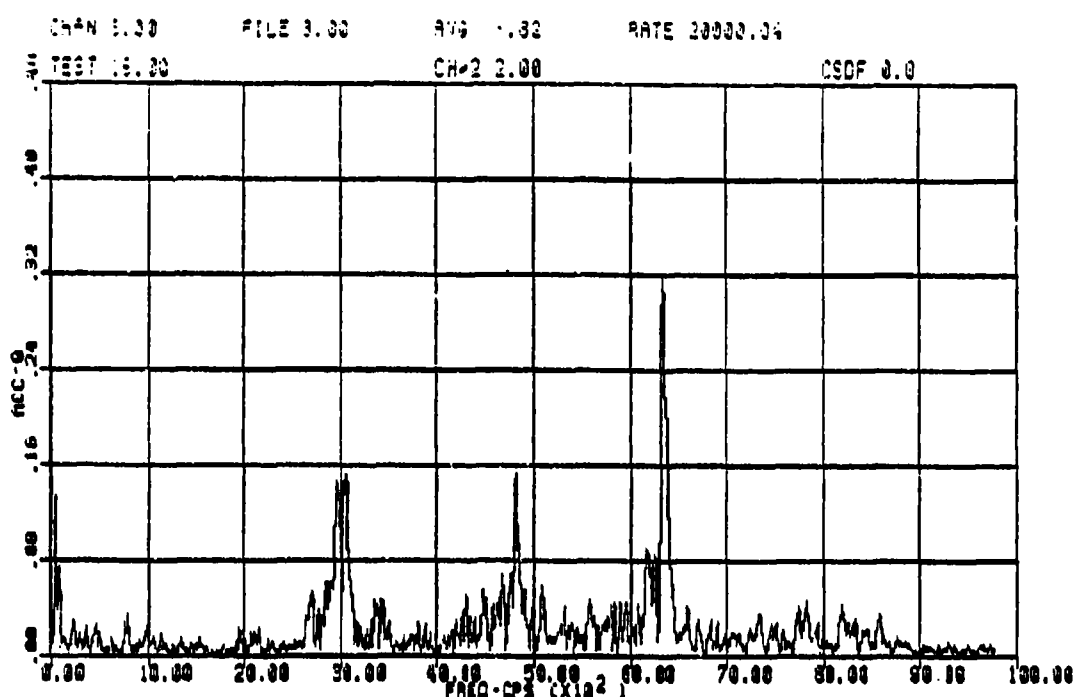








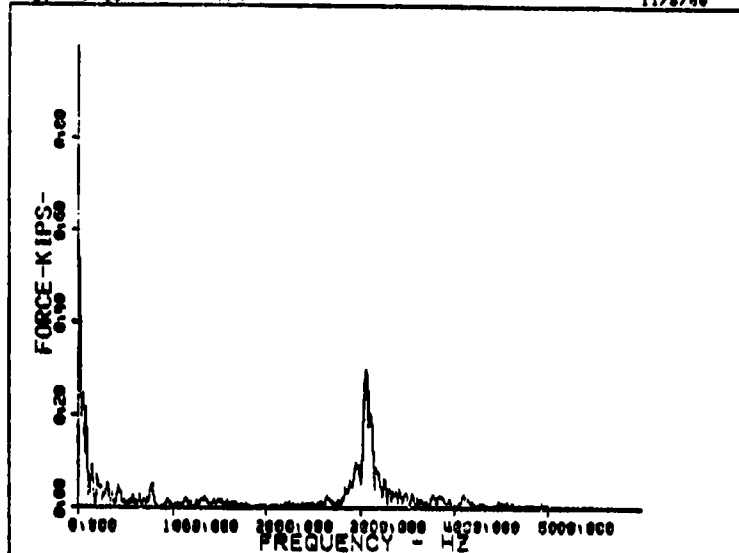




PLOT NO. 85

FFT

11/3/88



RAW

TEST NO 18

MAX = 0.0301017

RATE = 10000.000

CH NO 2

DOP = 1

POINTS= 812

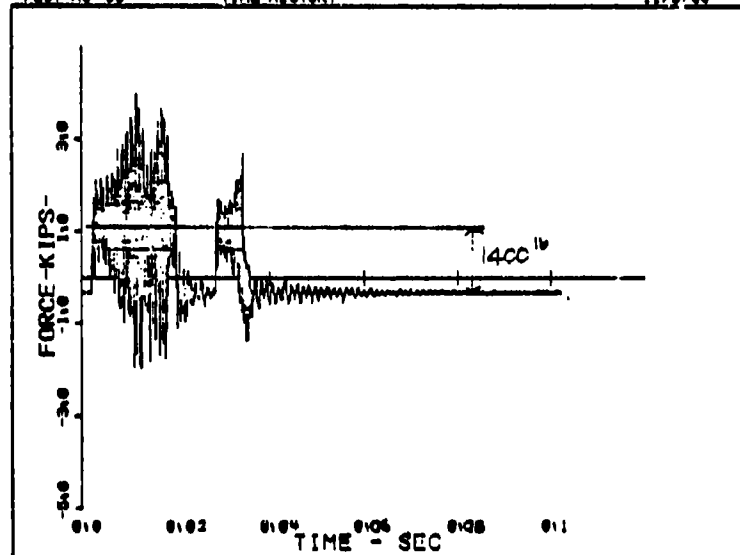
FREQ= 10.03125

RMS = 0.04020

PLOT NO. 85

TIME HISTORY

11/3/88



RAW

TEST NO 18

MAX = 3.0311810

RATE = 10000.000

CH NO 2

MEAN= 0.31030

POINTS= 1024

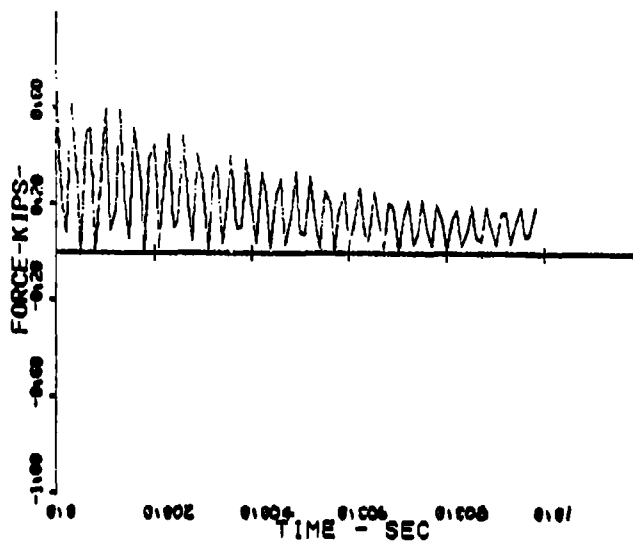
MIN = -1.00407

RMS = 0.04034

PLOT NO 88

AUTO CURVE FITTING

11/3/88



RAW

TEST NO 18
CH NO 2

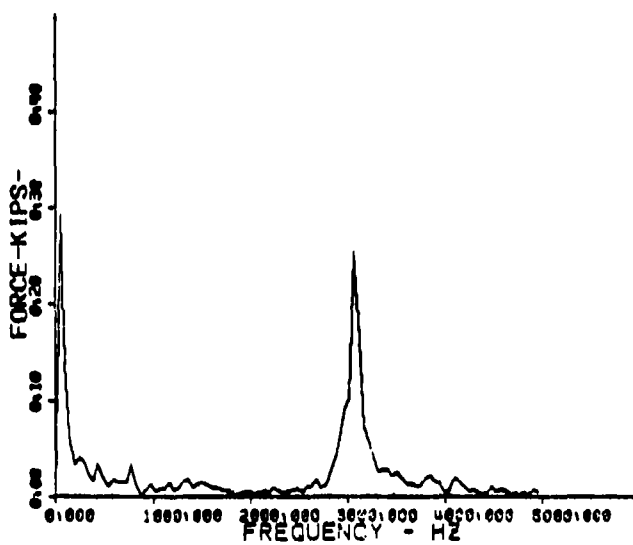
MAX = 0.5050004
MEAN = 0.11000
MIN = -0.10073

RATE = 10000.000
POINTS = 1024
RMS = 0.104103

PLOT NO 89

FFT

11/3/88



RAW

TEST NO 18
CH NO 2

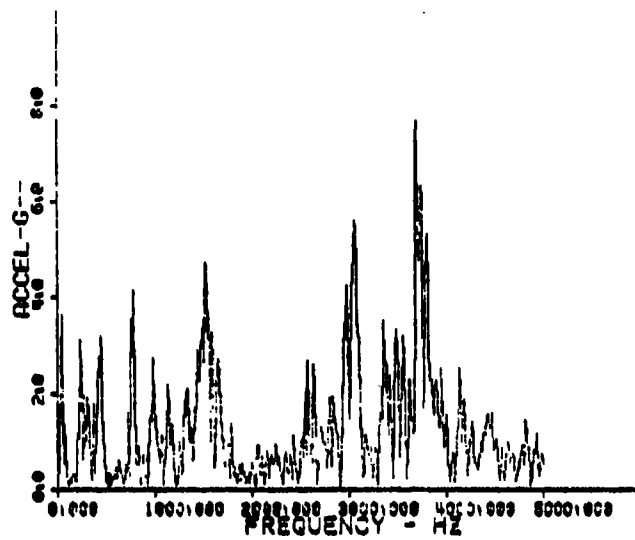
MAX = 0.2921032
DOF = 0
FREQ = 10.53125

RATE = 10000.000
POINTS = 102
RMS = 0.104320

PLOT NO 25

FFT

11/3/88



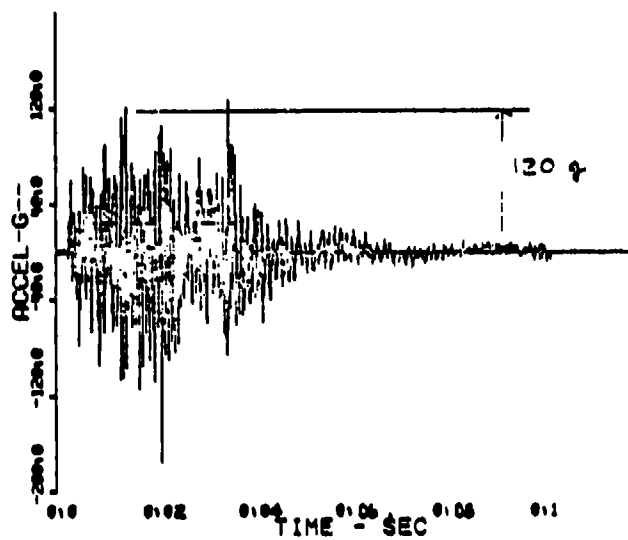
RAW

TEST NO 18
CH NO 3MAX = 7.7699122
DOF = 1
FREQ = 3761.17167RATE = 10000.000
POINTS = 512
RMS = 20.16834

PLOT NO 25

TIME HISTORY

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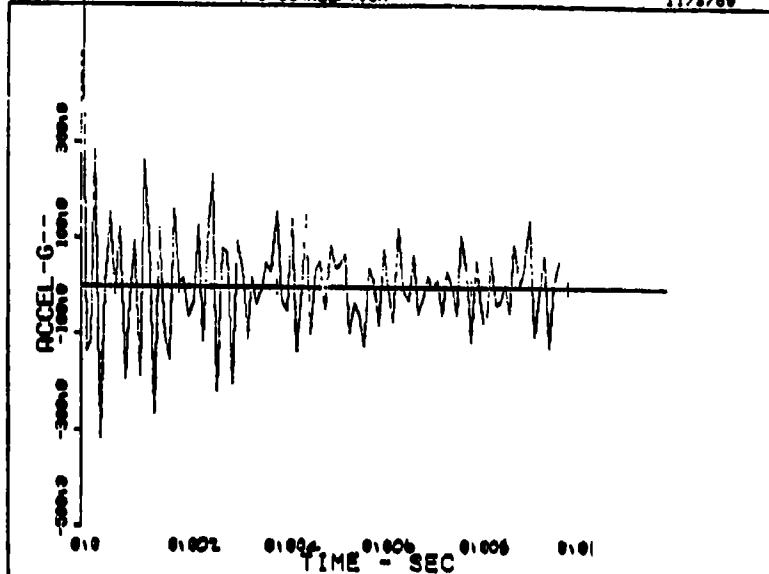
RAW

TEST NO 18
CH NO 3MAX = 126.1471748
MEAN = -9.73334
MIN = -175.38622RATE = 10000.000
POINTS = 1024
RMS = 20.16859

PLOT NO 22

AUTO CORRELATION

11/3/89



RAW

TEST NO 18
CH NO 3

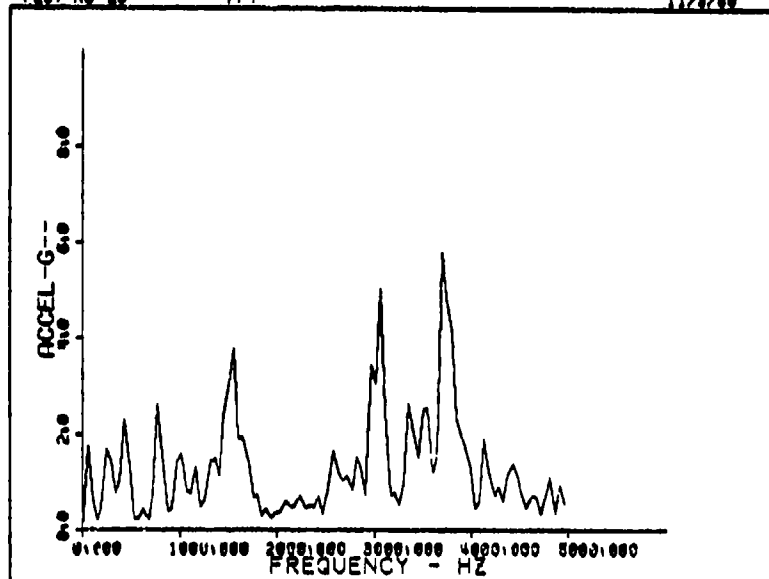
MAX = 283.4458732
MEAN = -8.73824
MIN = -318.72558

RATE = 10000.000
POINTS = 1024
RMS = 29.12732

PLOT NO 25

FFT

11/3/89



RAW

TEST NO 18
CH NO 3

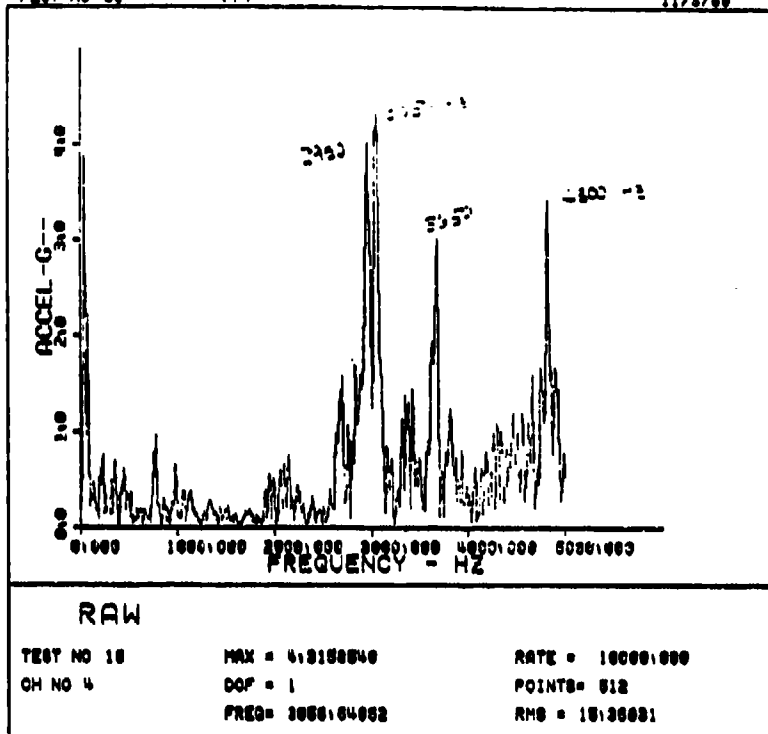
MAX = 8.7919349
DOF = 0
FREQ = 1761.17167

RATE = 10000.000
POINTS = 103
RMS = 29.18634

PLOT NO 39

FFT

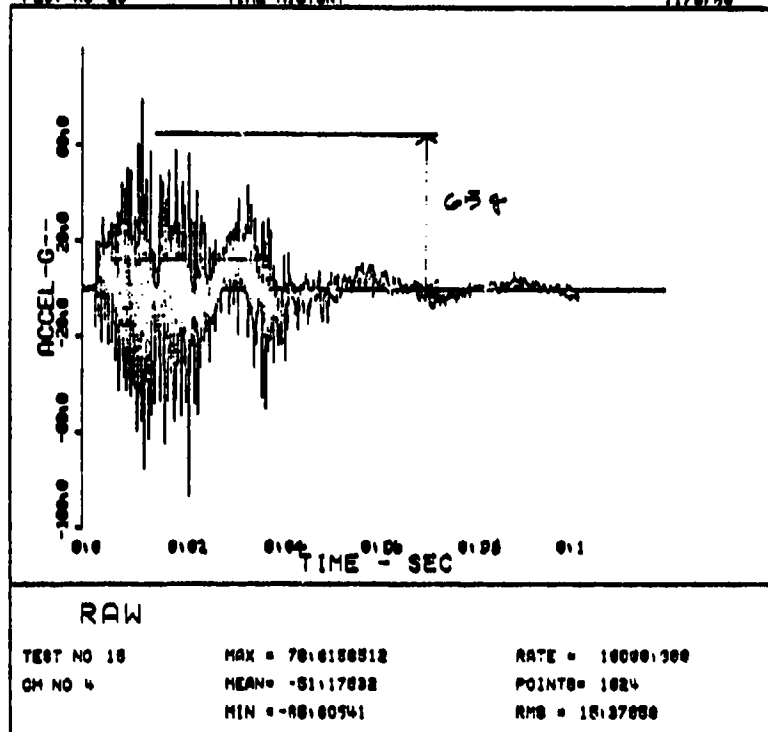
11/3/99



PLOT NO 39

TIME HISTORY

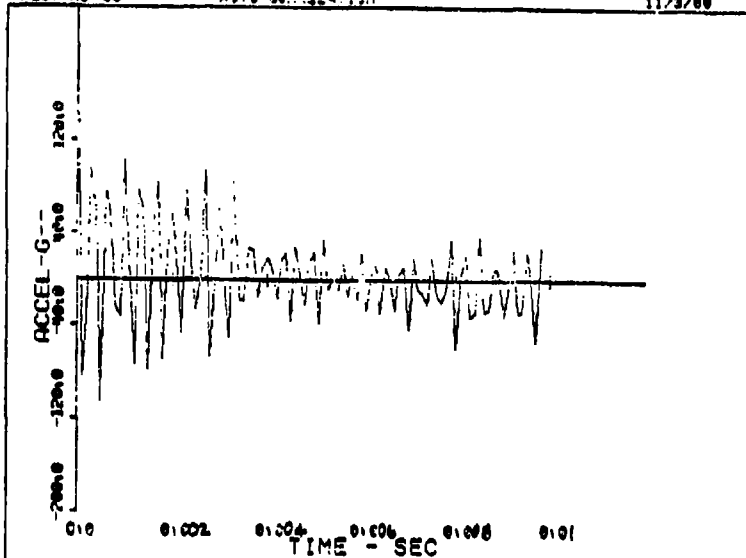
11/3/99



PLOT NO 35

AUTO CORRELATION

11/3/88



RAW

TEST NO 18

MAX = 10211487105

RATE = 10000.000

CH NO 4

MEAN = -51117632

POINTS = 1024

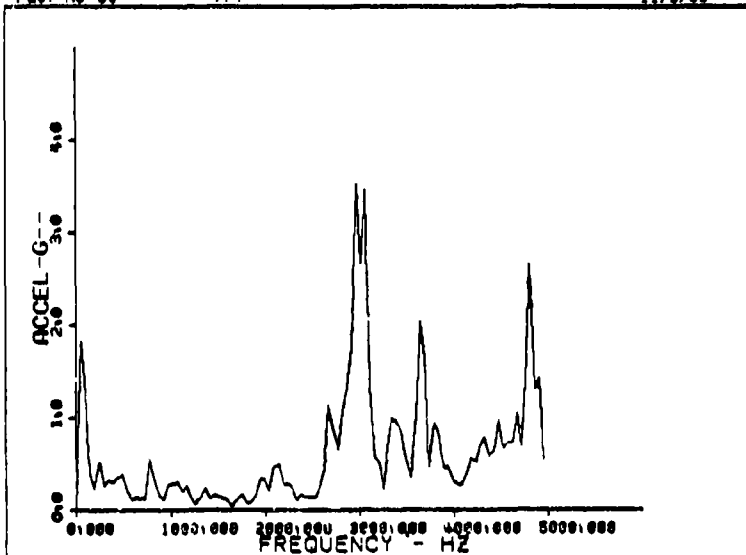
MIN = -108180174

RMS = 15134203

PLOT NO 36

FFT

11/3/88



RAW

TEST NO 18

MAX = 315237550

RATE = 10000.000

CH NO 4

DOF = 0

POINTS = 103

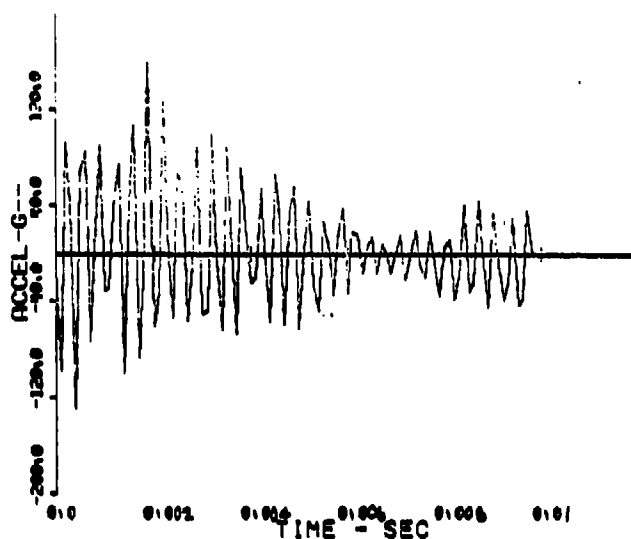
FREQ = 3050.64002

RMS = 15135031

PLOT NO 33

CROSS CORRELATION

11/3/88



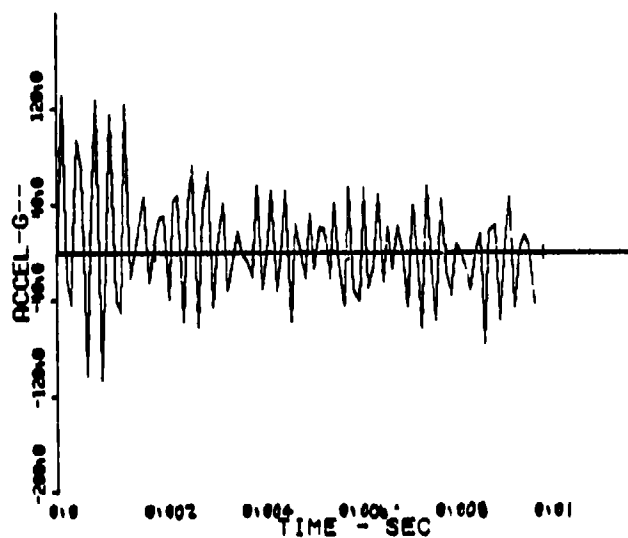
RAW

TEST NO 18
CH NO 4 & 3MAX = 180.3657488
MEAN = -81.17692
MIN = -120.79552RATE = 10000.000
POINTS = 1024
RMS = 15.87950

PLOT NO 34

CROSS CORRELATION

11/3/88



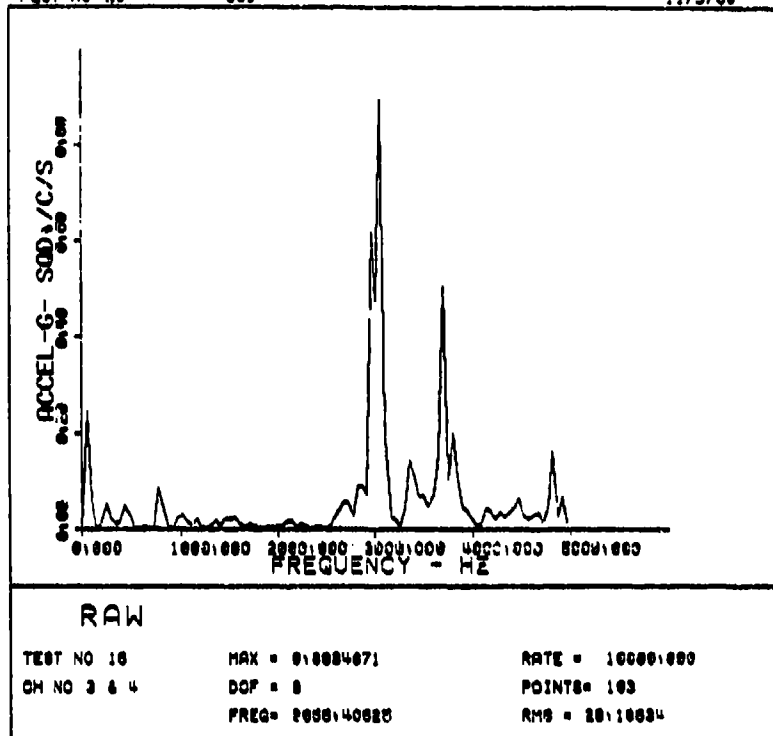
RAW

TEST NO 18
CH NO 3 & 4MAX = 132.2032020
MEAN = -8.73024
MIN = -108.86780RATE = 10000.000
POINTS = 1024
RMS = 20.18050

PLOT NO 28

CSD

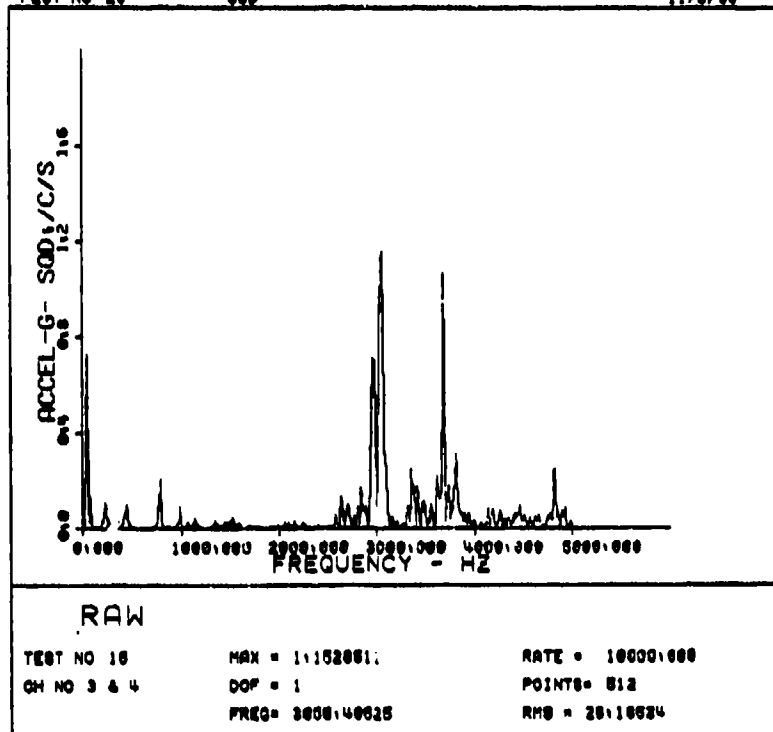
11/3/88



PLOT NO 29

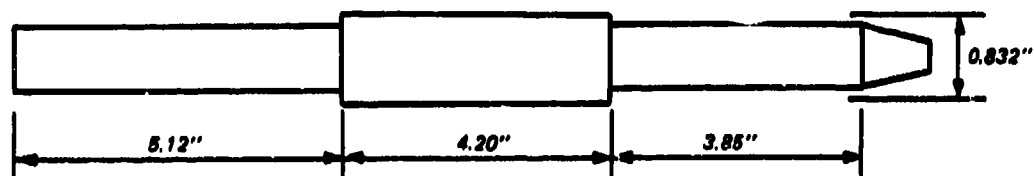
CSD

11/3/88



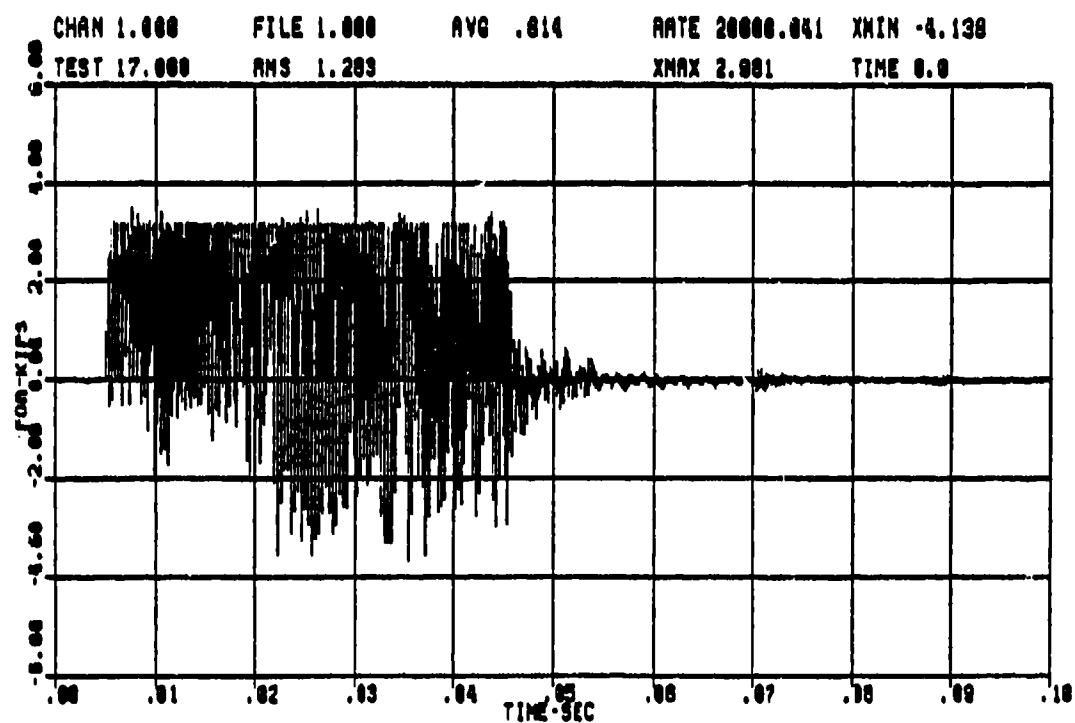
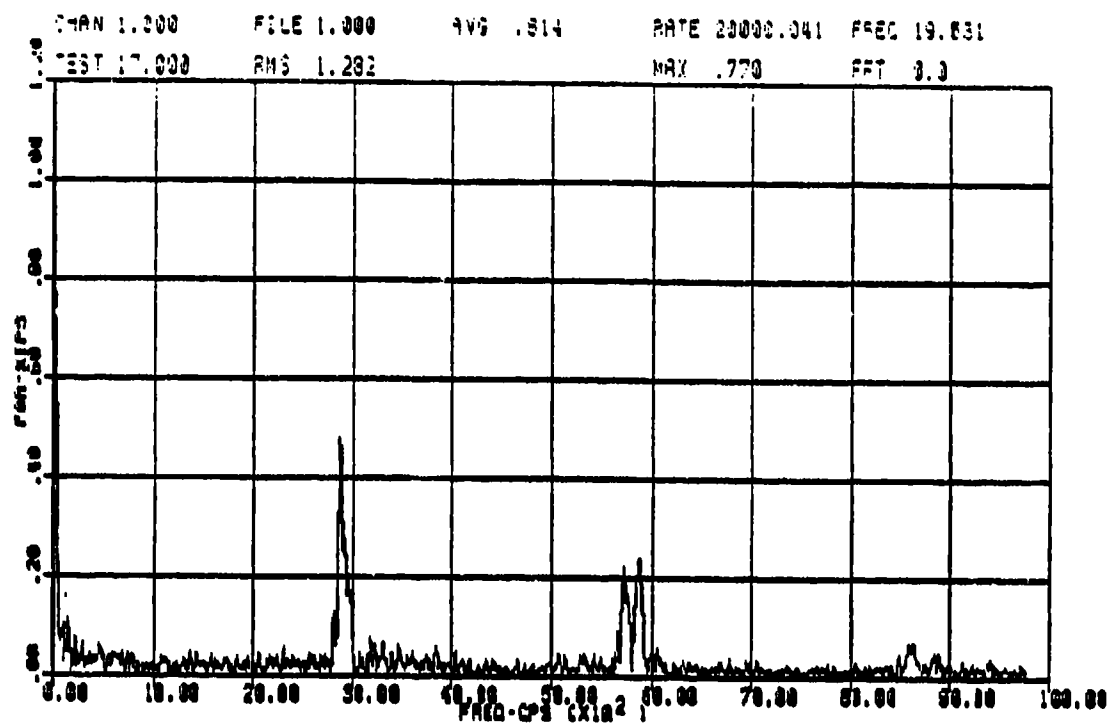
APPENDIX D: TEST 17 DATA

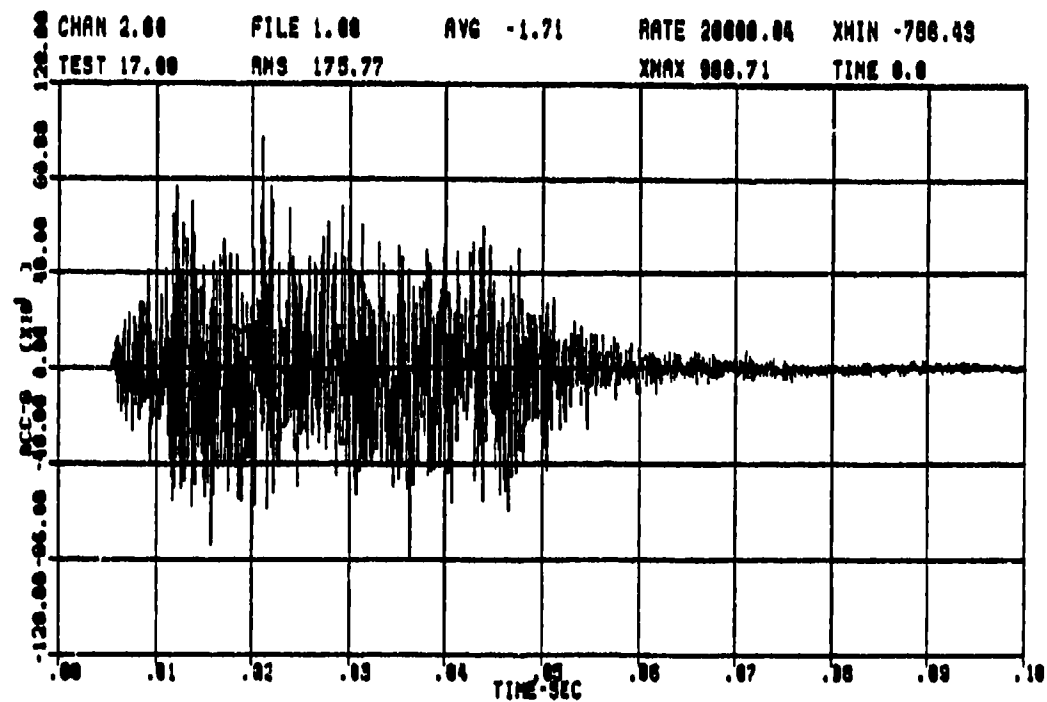
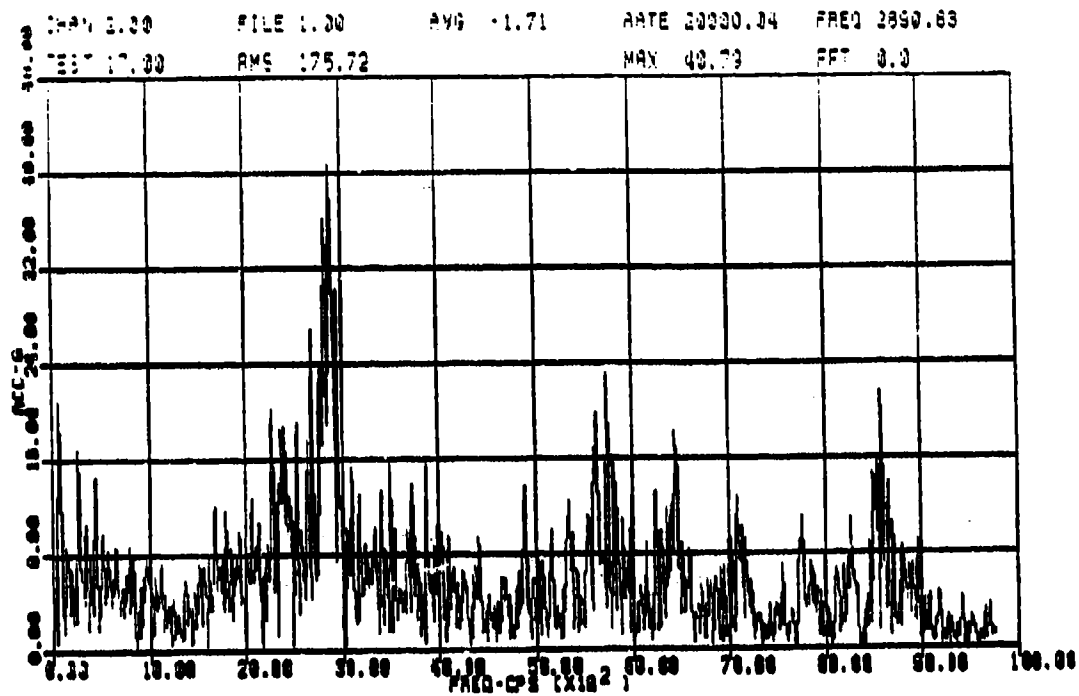
Test 17
Equipment Rack Hard-Mounted
AN/GRC-103 in Rack, Off-Line

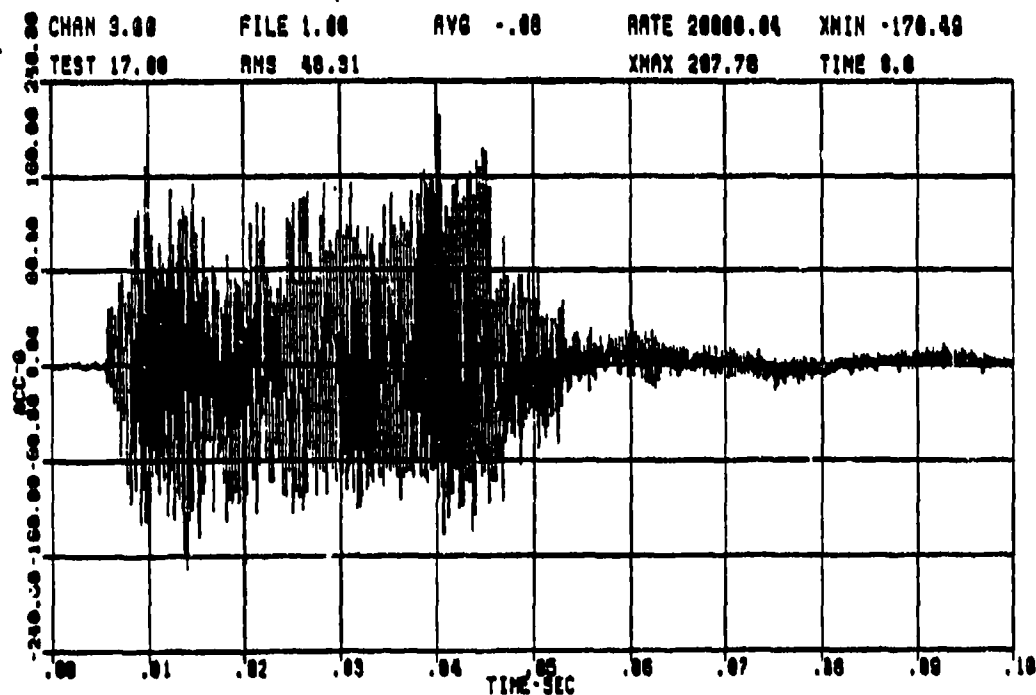
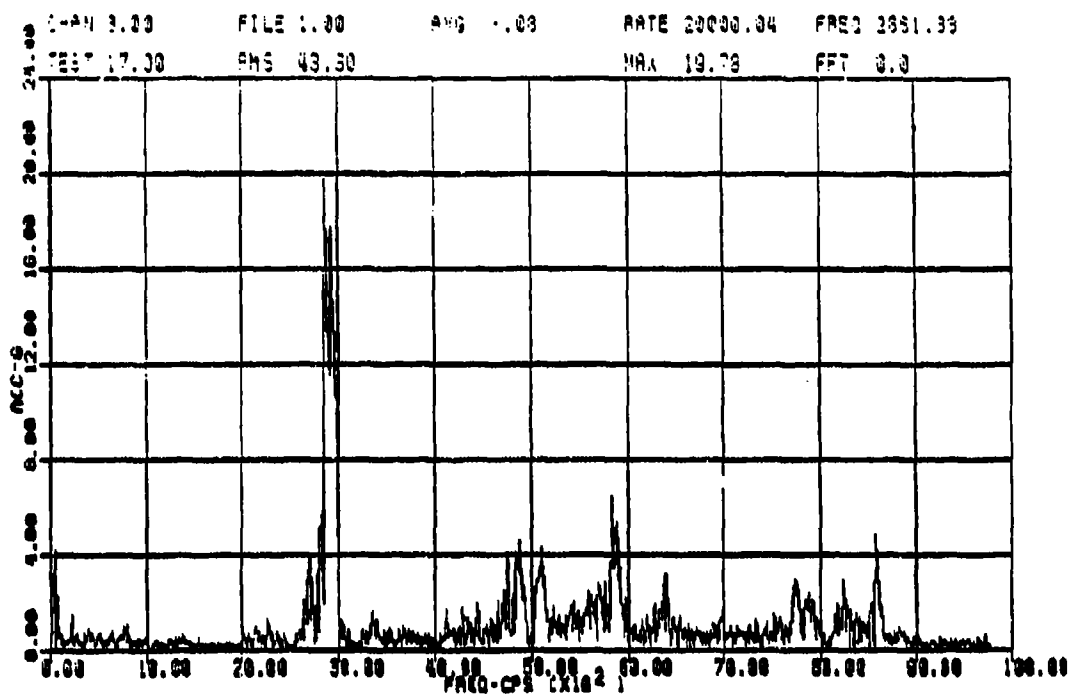


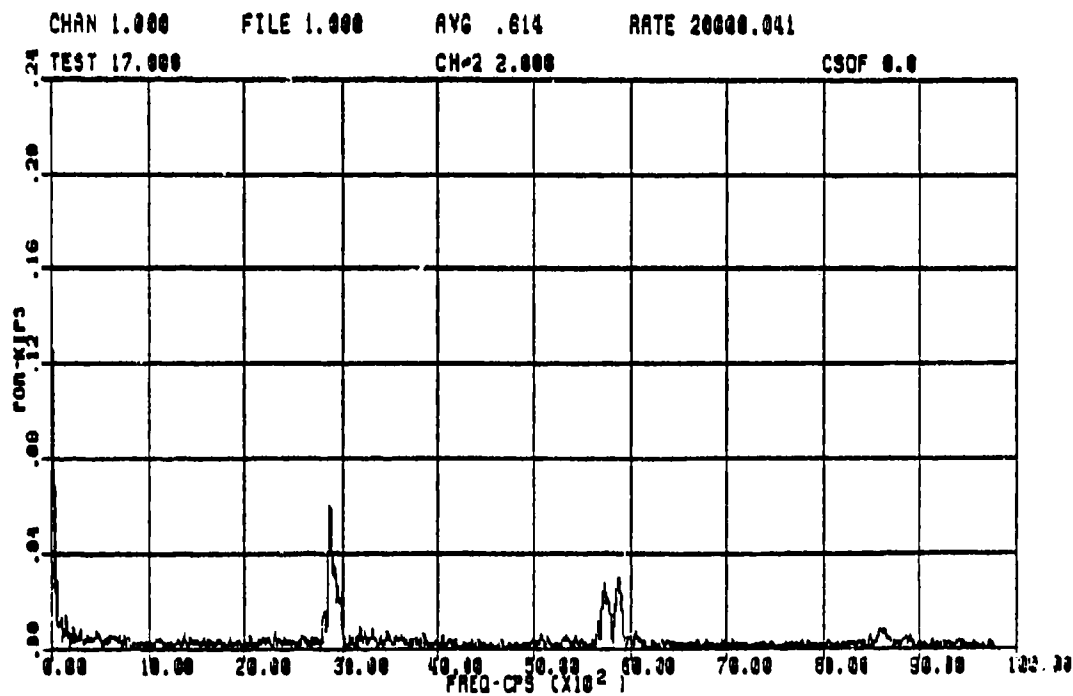
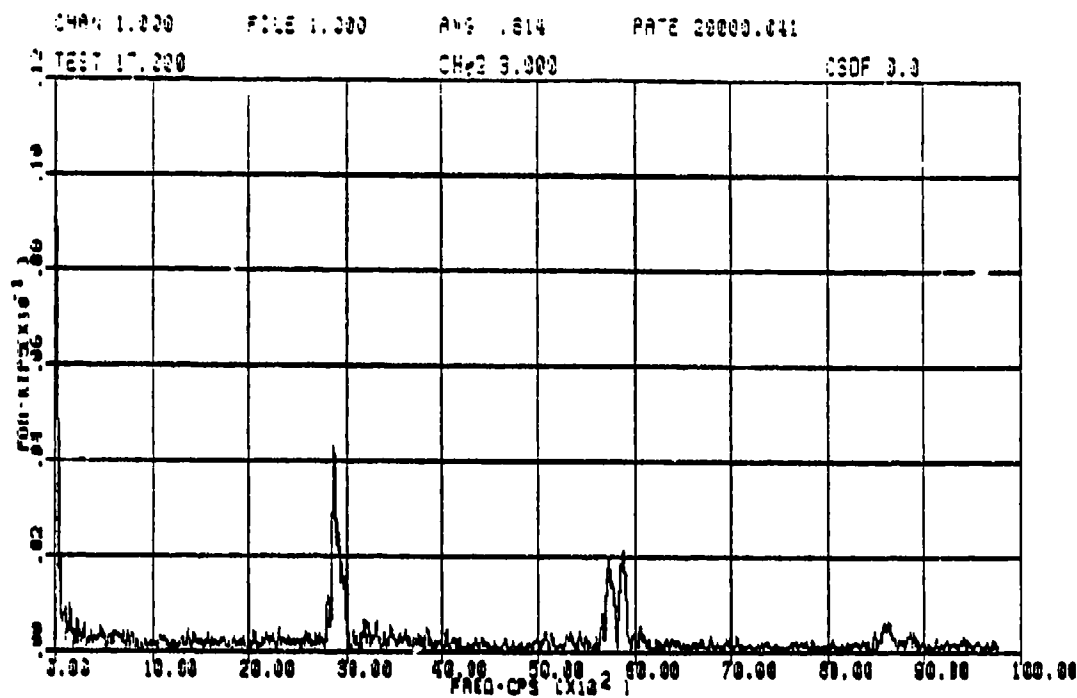
PULSE TRAIN - TEST 17

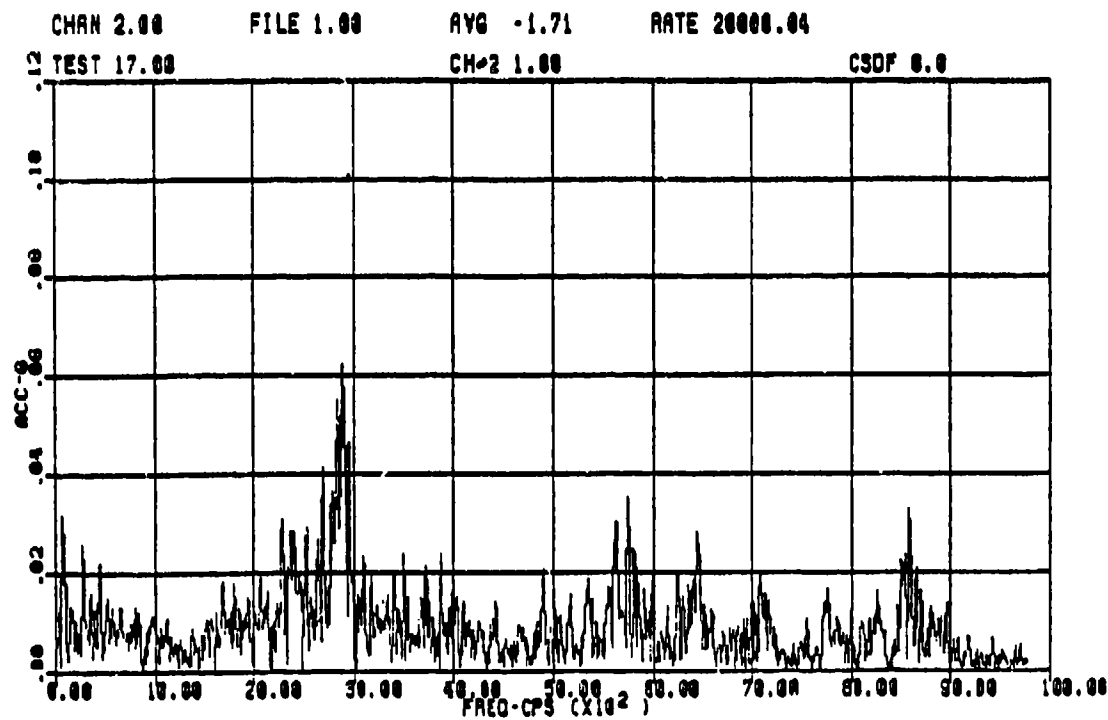
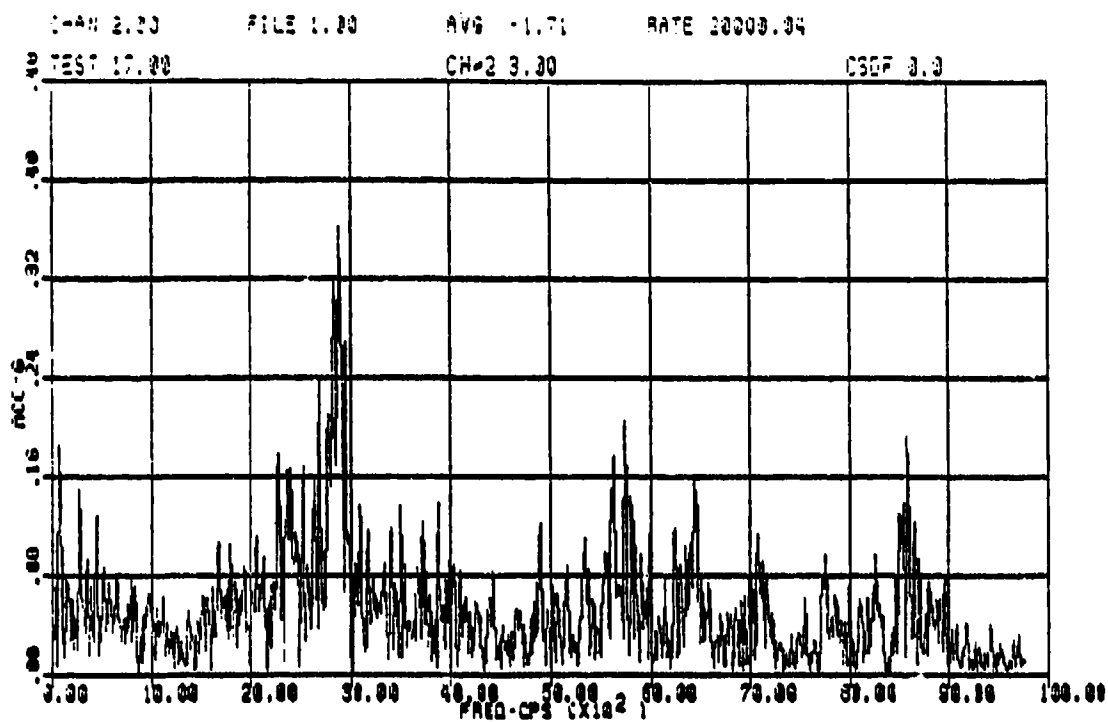
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #6%

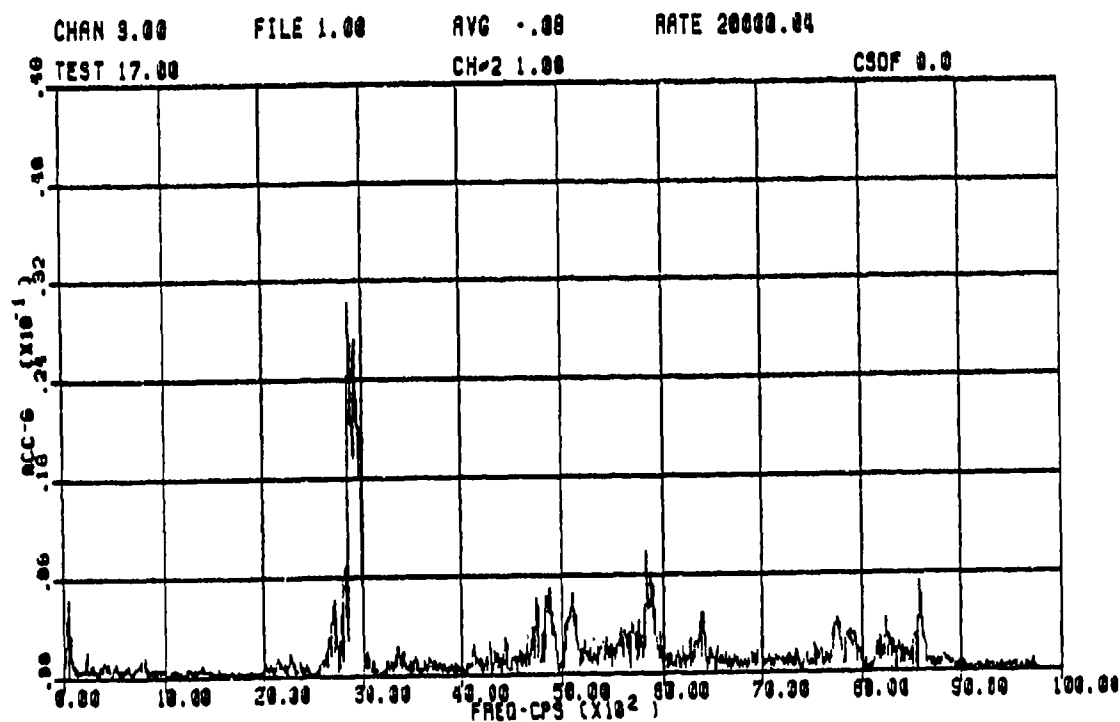
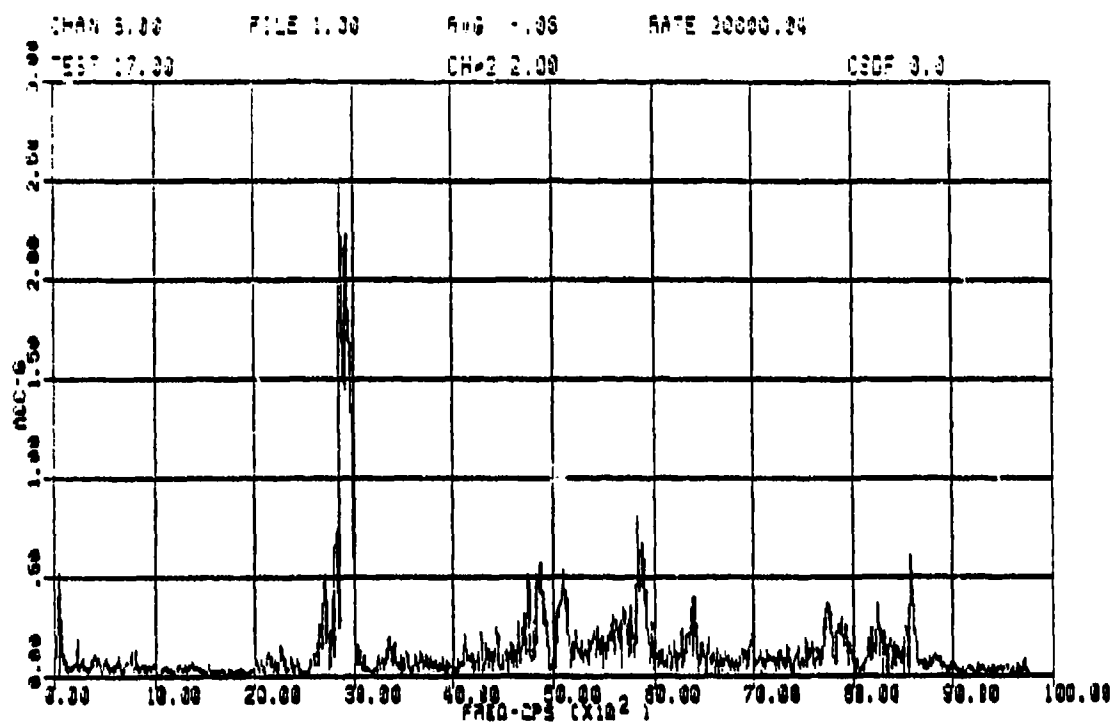








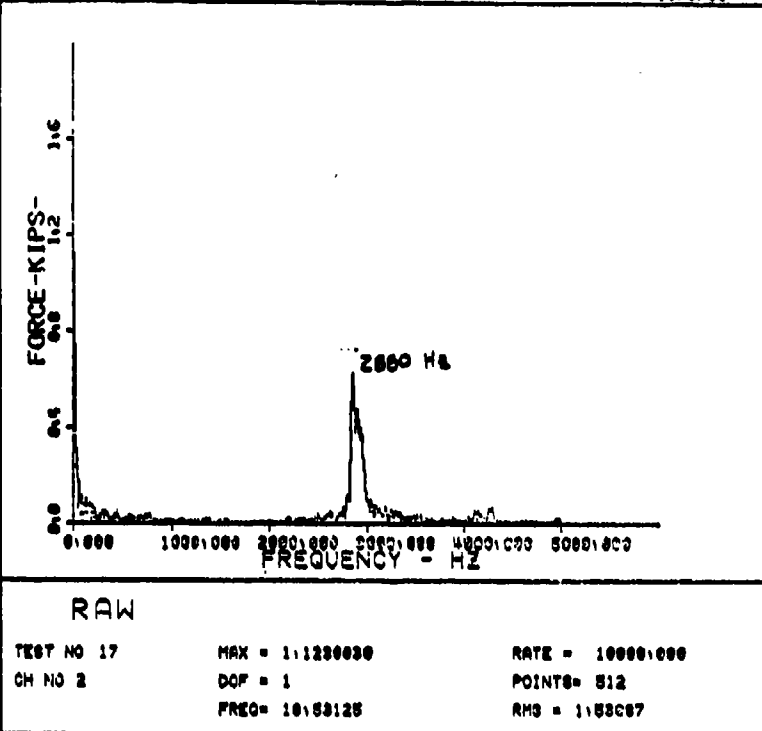




PLOT NO 02

FFT

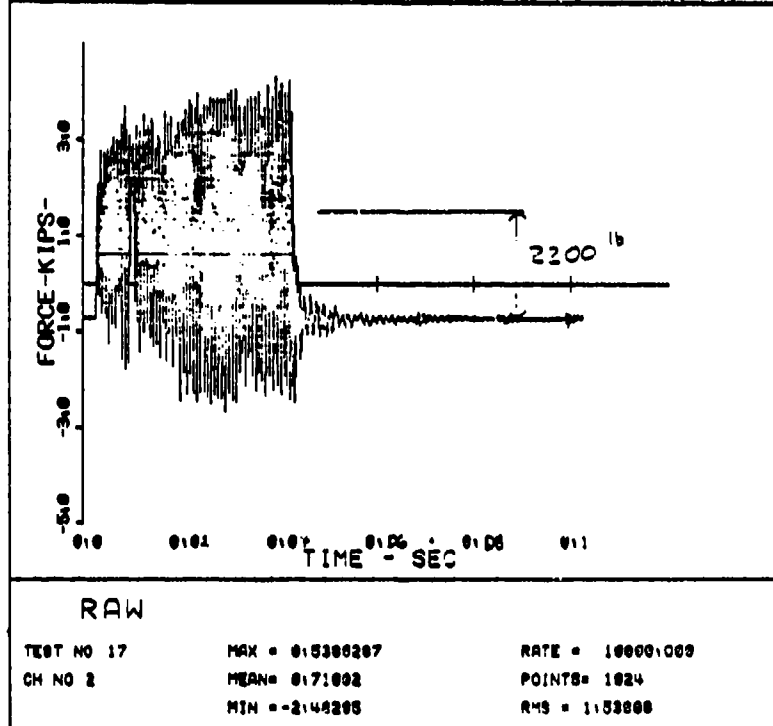
11/3/88



PLOT NO 00

TIME HISTORY

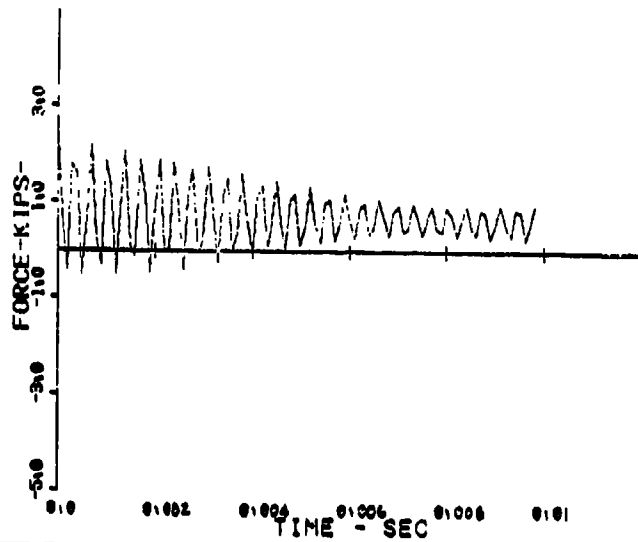
11/3/88



PLOT NO 92

AUTO CORRELATION

11/3/88



RAW

TEST NO 17

MAX = 2.1835513

RATE = 10000.000

CH NO 2

MEAN = 0.71002

POINTS = 1024

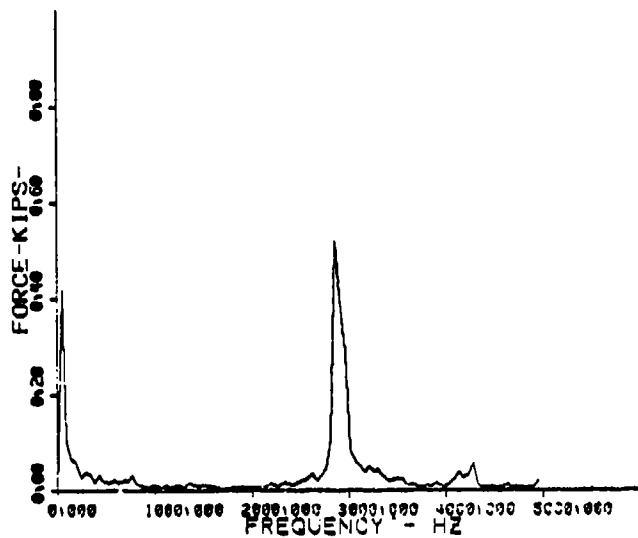
MIN = -0.75317

RMS = 1.61847

PLOT NO 99

FFT

11/3/88



RAW

TEST NO 17

MAX = 0.5208155

RATE = 10000.000

CH NO 2

DOF = 0

POINTS = 103

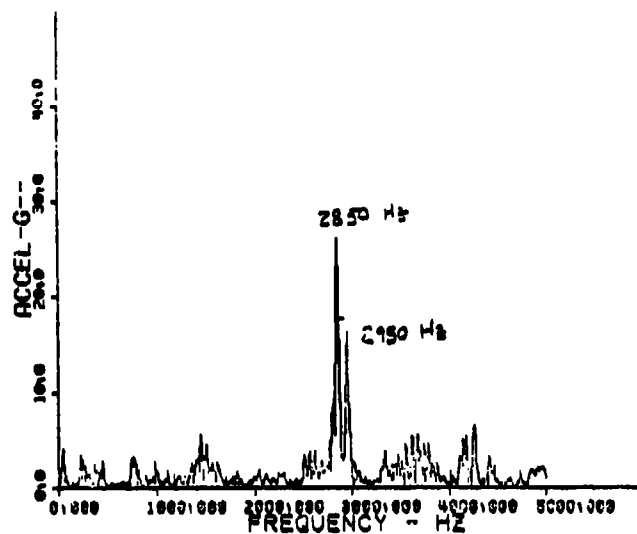
FREQ = 10.53125

RMS = 1.53097

PLOT NO 38

FFT

11/3/88



RAW

TEST NO 17

MAX = 26.1618784

RATE = 10000.000

CH NO 3

DOF = 1

POINTS = 512

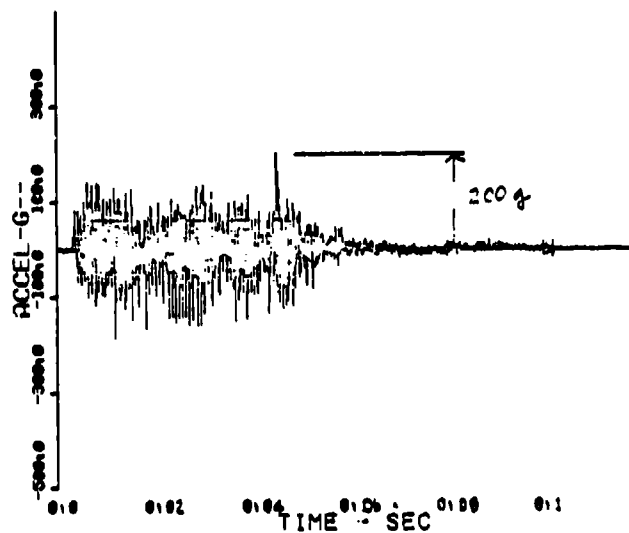
FREQ = 2861.82812

RMS = 46.63300

PLOT NO 37

TIME HISTORY

11/3/88



RAW

TEST NO 17

MAX = 202.6517346

RATE = 10000.000

CH NO 3

MEAN = -9.34183

POINTS = 1024

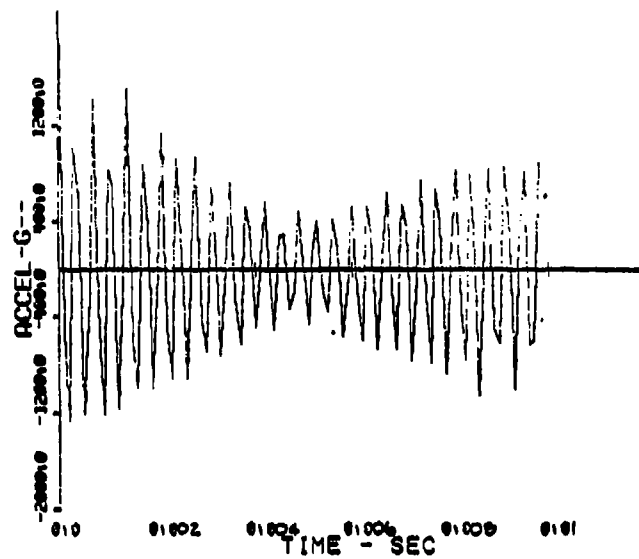
MIN = -182.87781

RMS = 46.64635

PLOT NO 48

AUTO CORRELATION

11/3/88



RAW

TEST NO 17

MAX = 1818.485842

RATE = 10000.000

CH NO 3

MEAN = -8.34295

POINTS = 1024

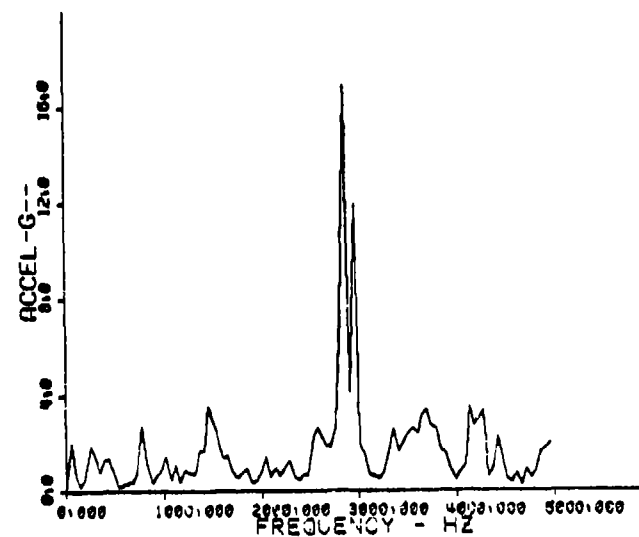
MIN = -1200.53871

RMS = 46.37692

PLOT NO 38

FFT

11/3/88



RAW

TEST NO 17

MAX = 16.6832170

RATE = 10000.000

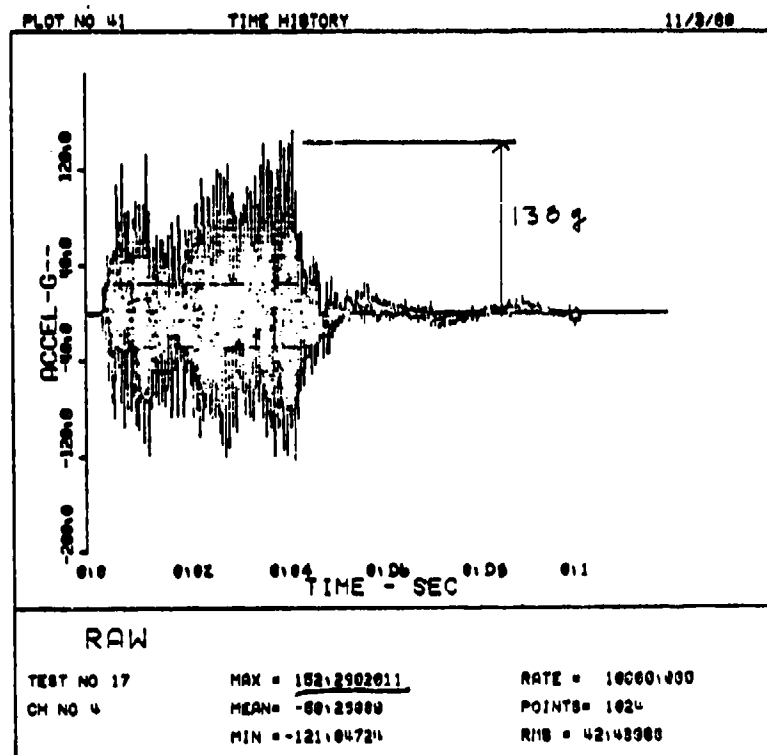
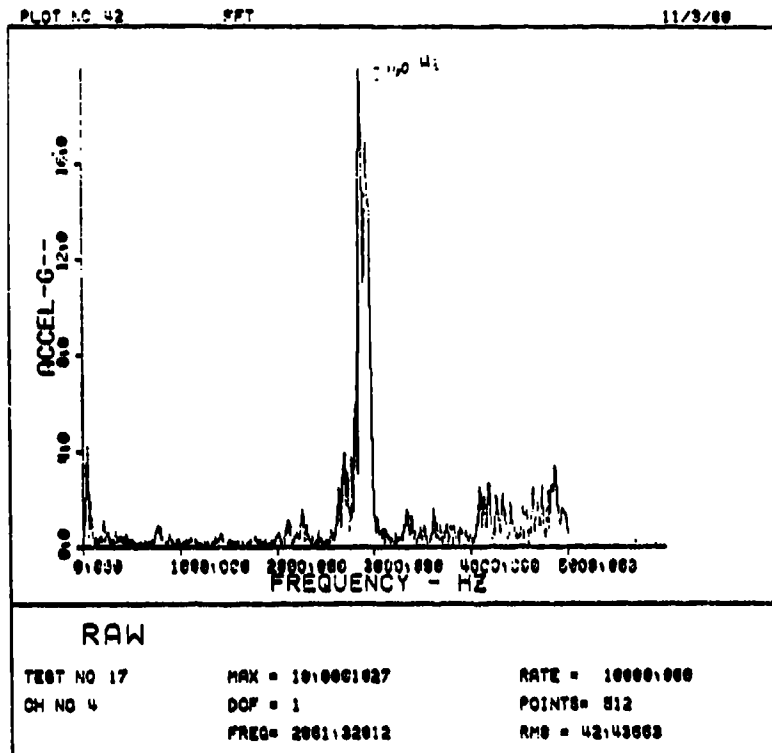
CH NO 3

DCF = 0

POINTS = 103

FREQ = 2801.32612

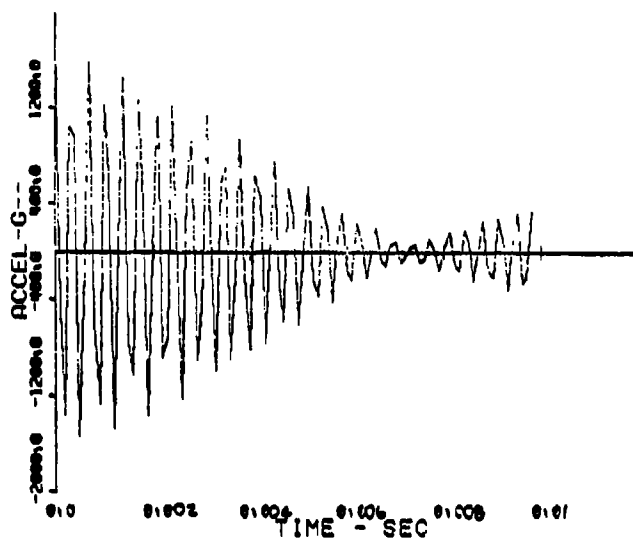
RMS = 46.63596



PLOT NO 47

AUTO CORRELATION

11/3/88



RAW

TEST NO 17

MAX = 1551.5320575

RATE = 10000.000

CH NO 4

MEAN = -50.25000

POINTS = 1024

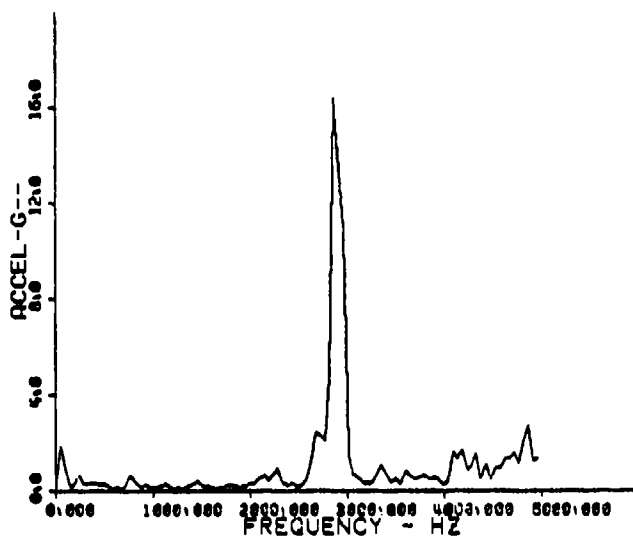
MIN = -1530.54007

RMS = 42.24612

PLOT NO 48

FFT

11/3/88



RAW

TEST NO 17

MAX = 15.3550255

RATE = 10000.000

CH NO 4

DOF = 9

POINTS = 103

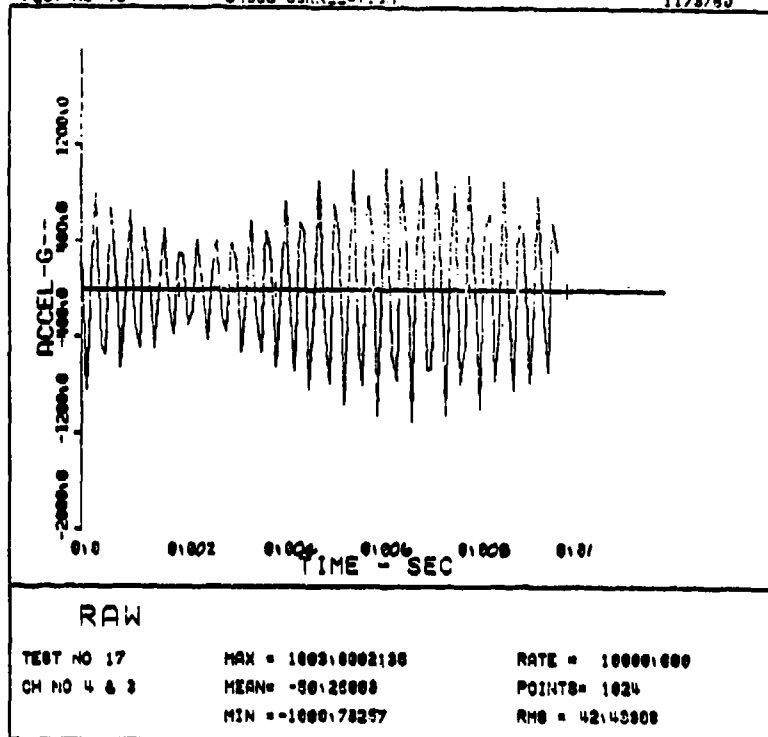
FREQ = 2501.32012

RMS = 42.43553

PLOT NO 48

CROSS CORRELATION

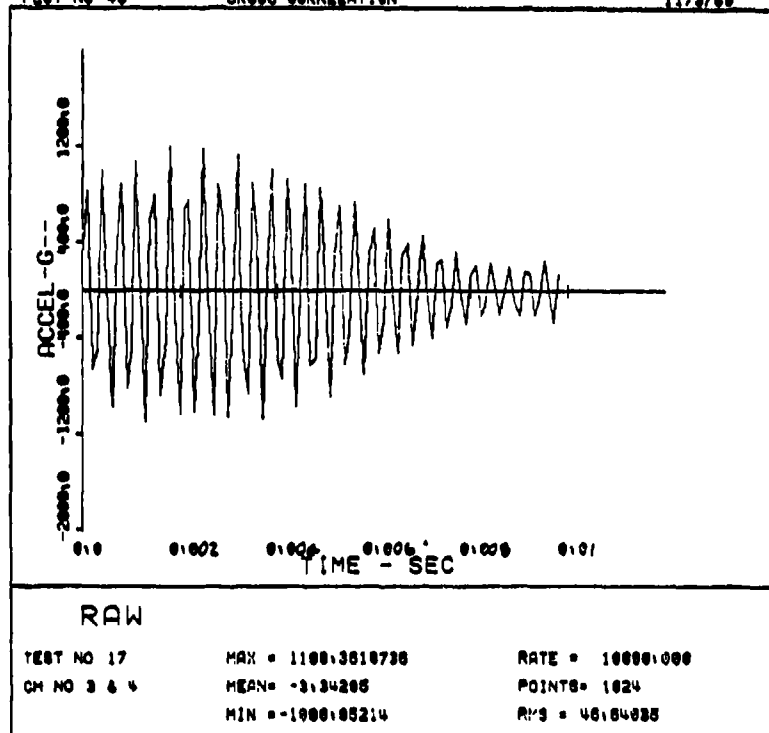
11/3/88

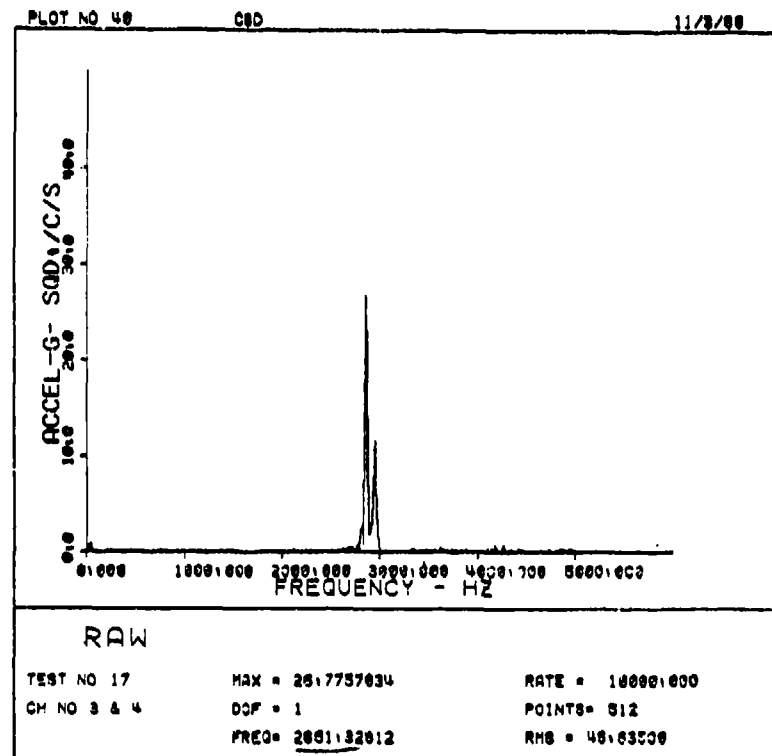
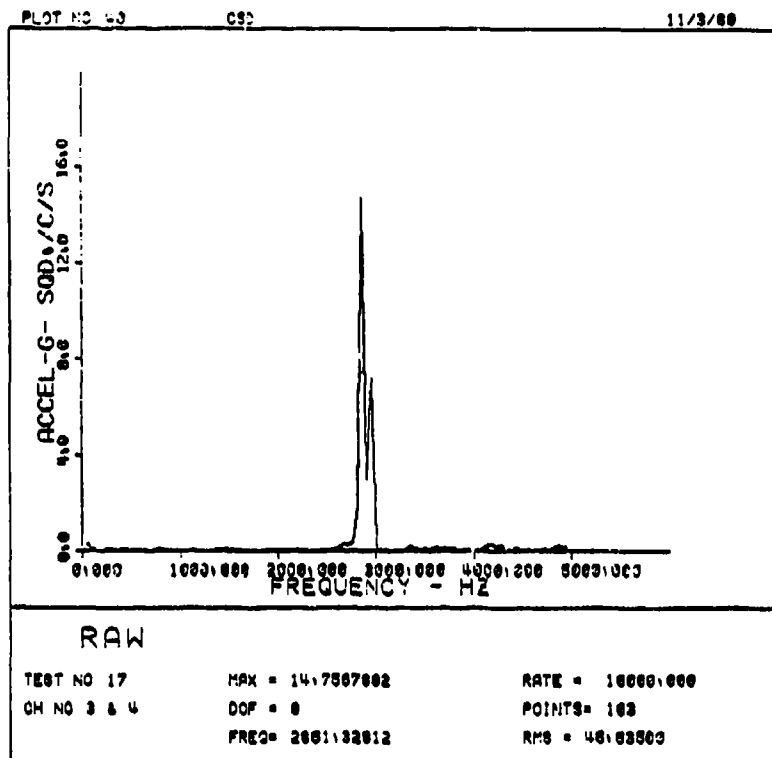


PLOT NO 48

CROSS CORRELATION

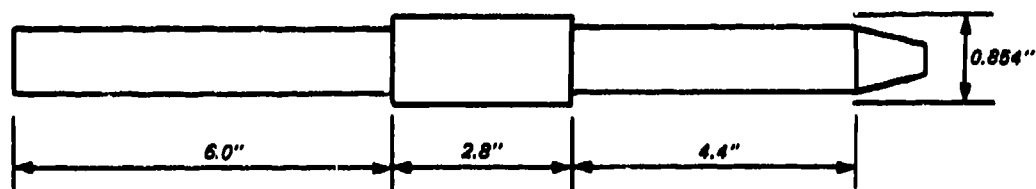
11/3/88





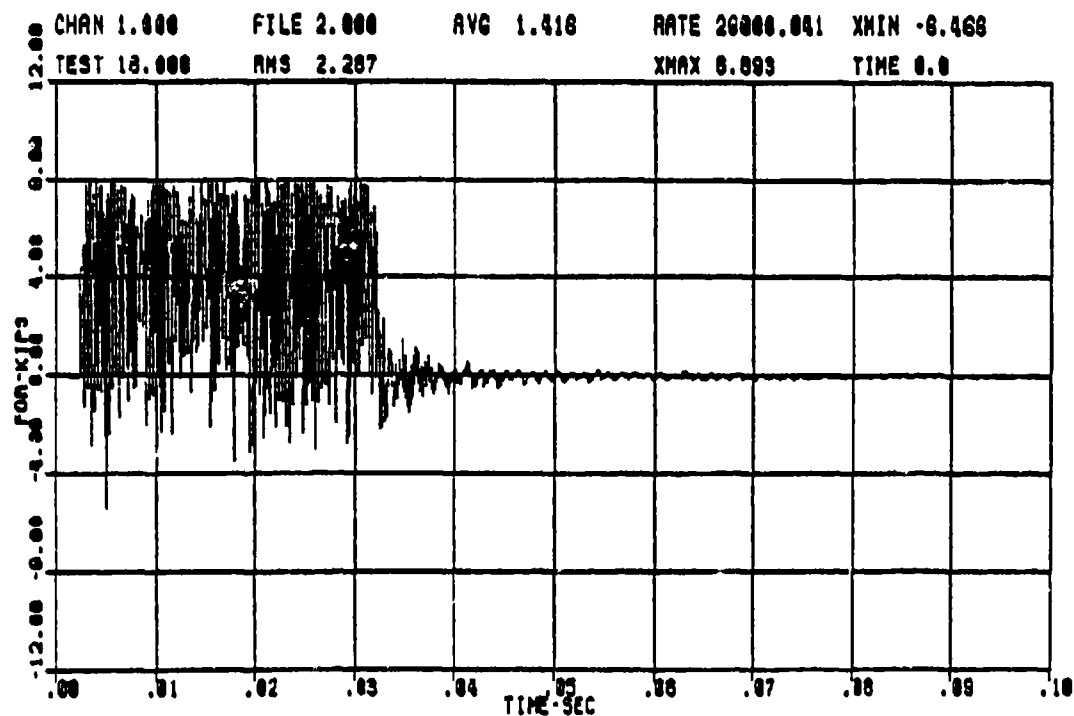
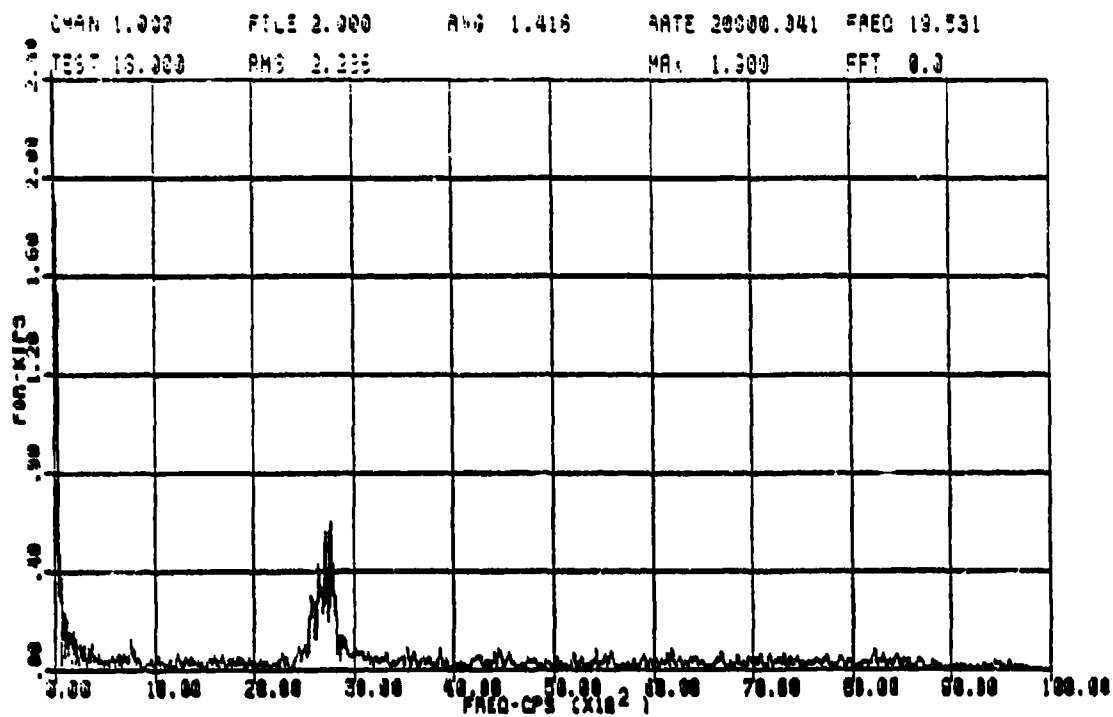
APPENDIX E: TEST 18 RESULTS

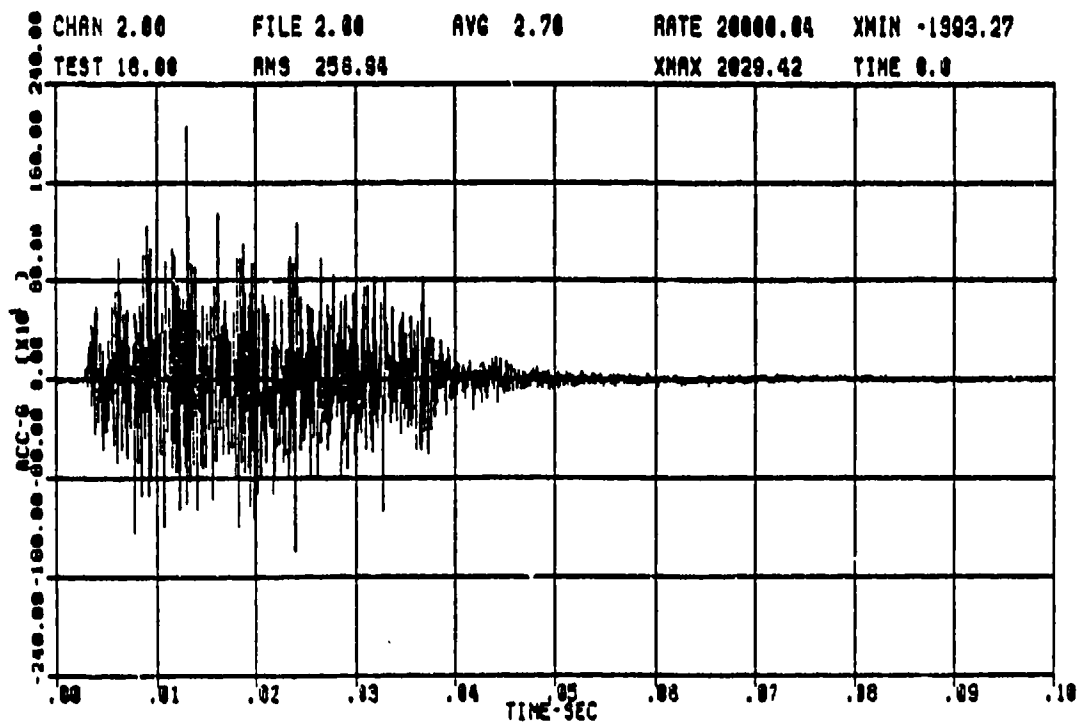
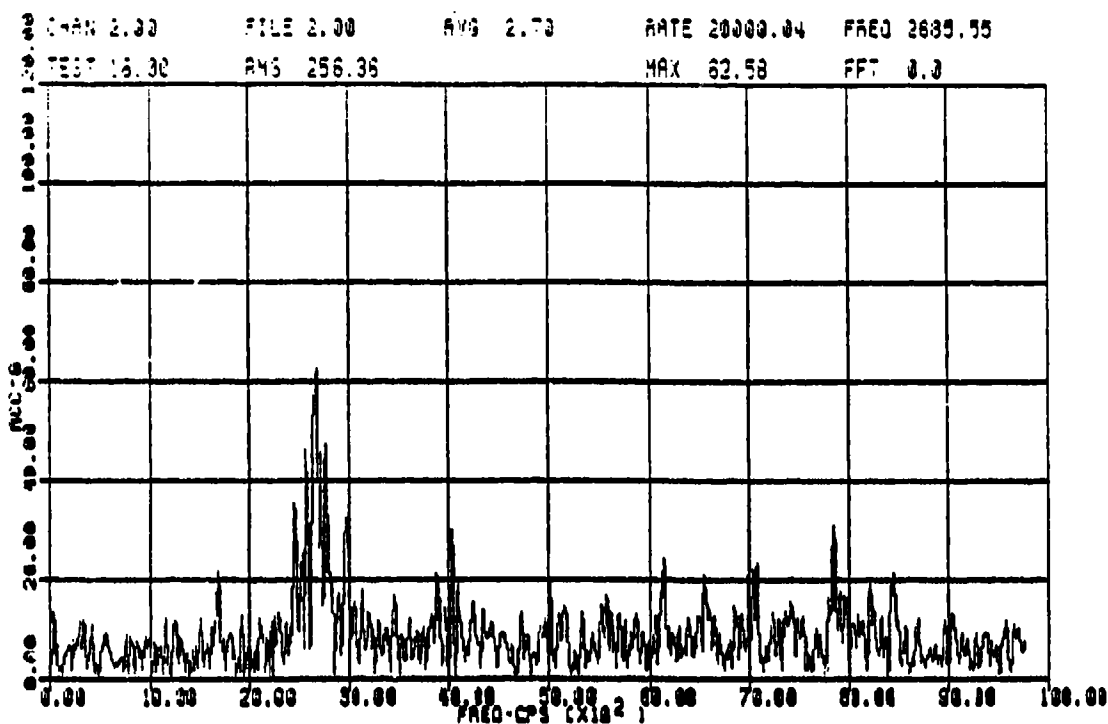
Test 18
Equipment Rack Hard-Mounted
AN/GRC-103 in Rack, On-Line

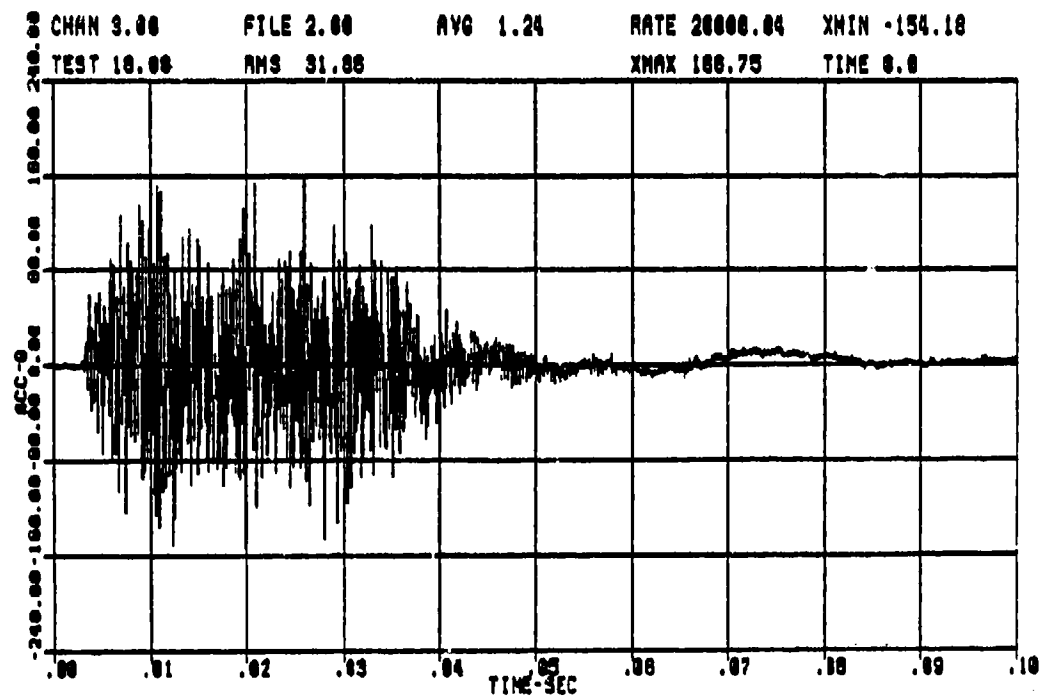
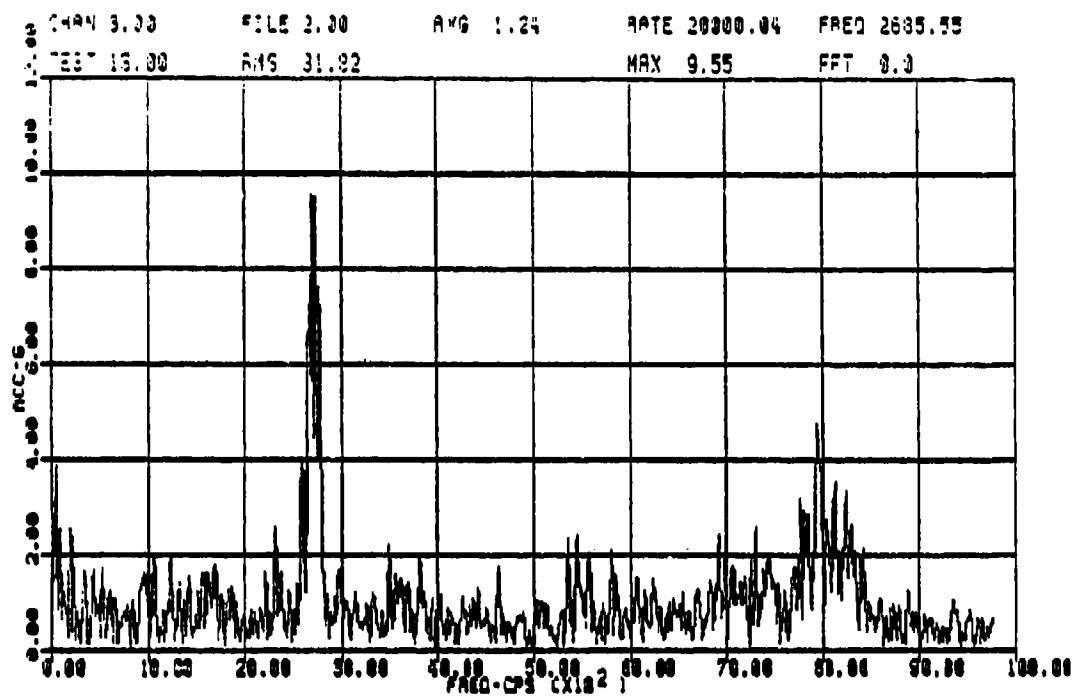


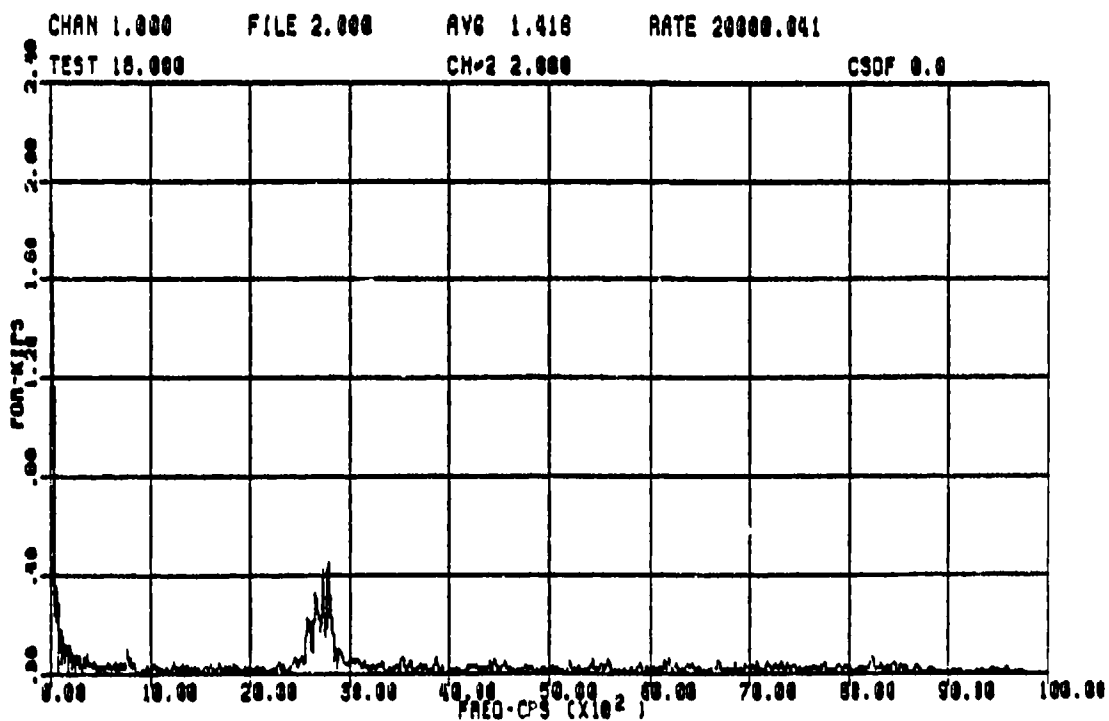
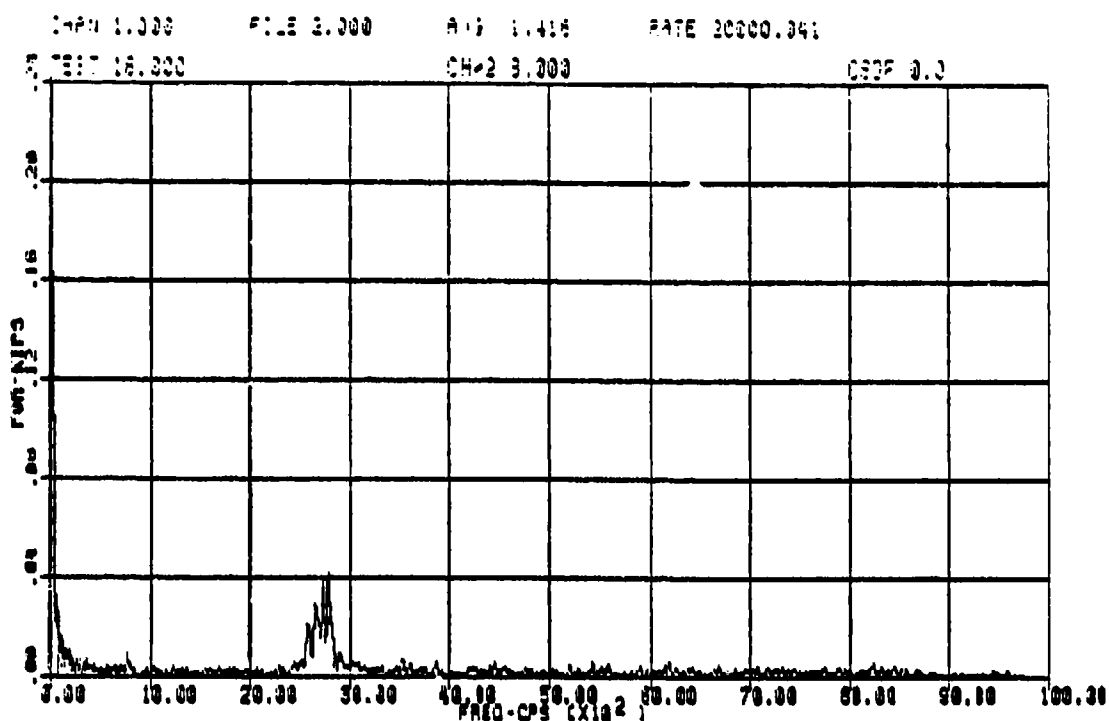
PULSE TRAIN - TEST 18

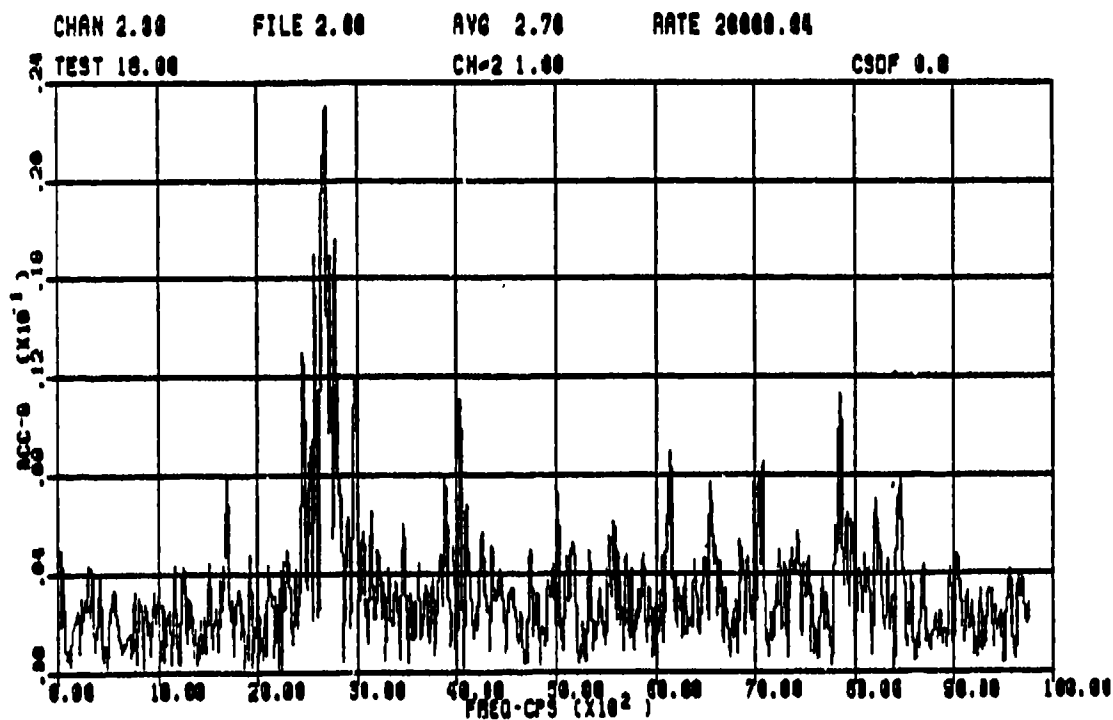
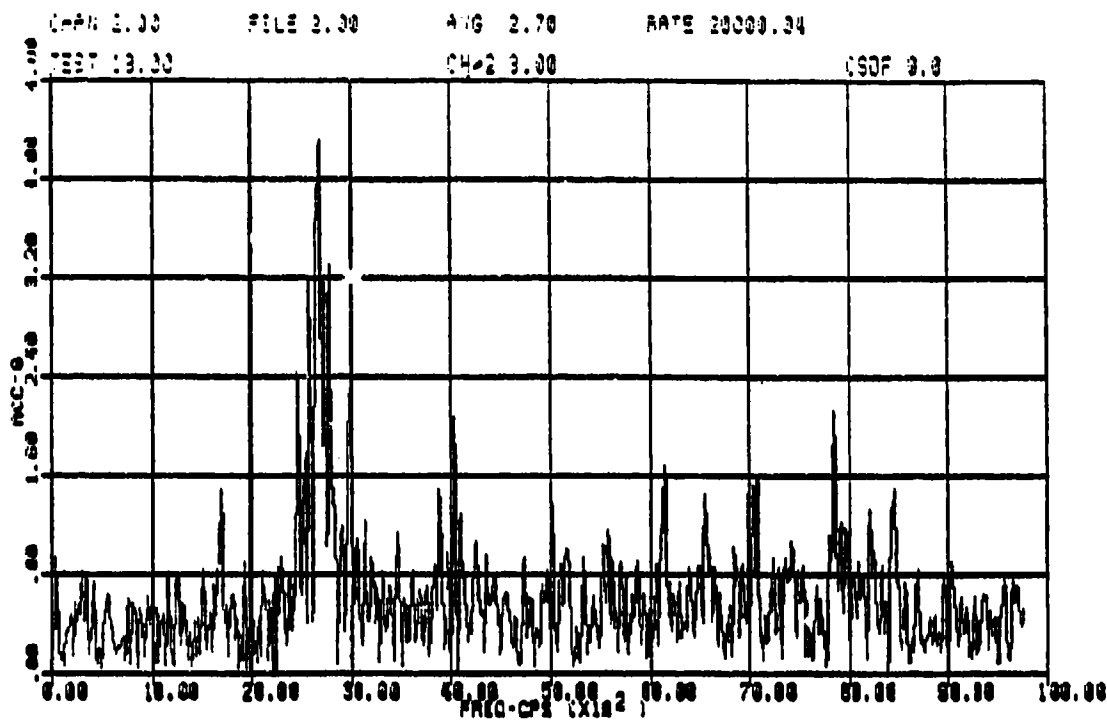
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #8½

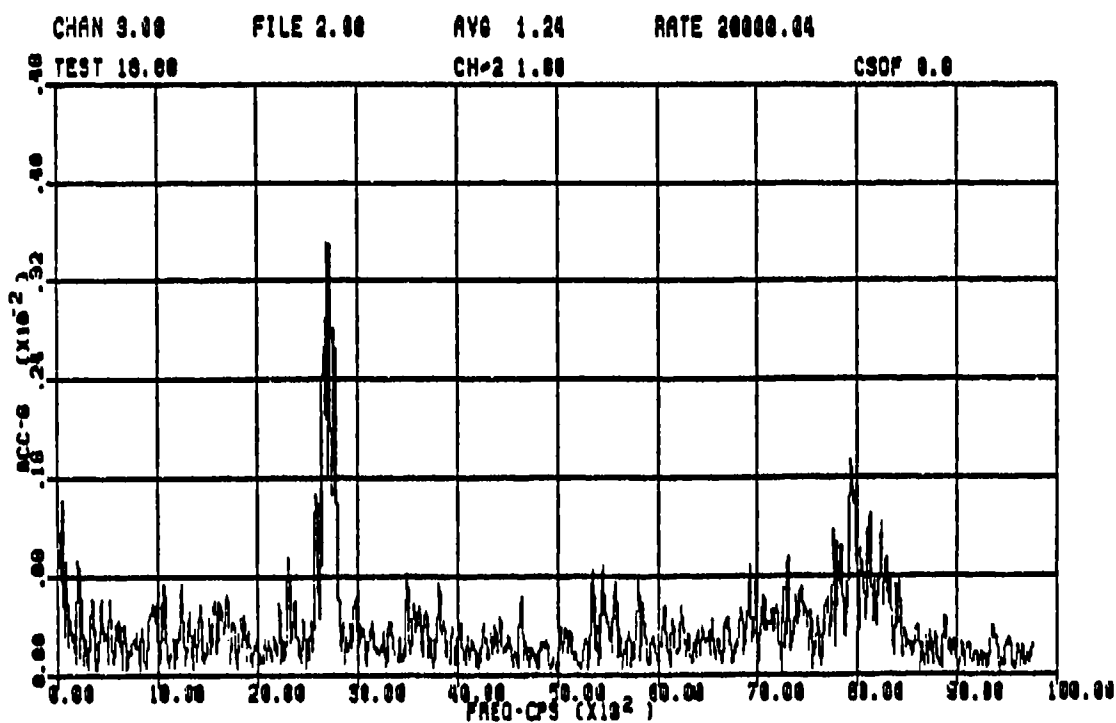
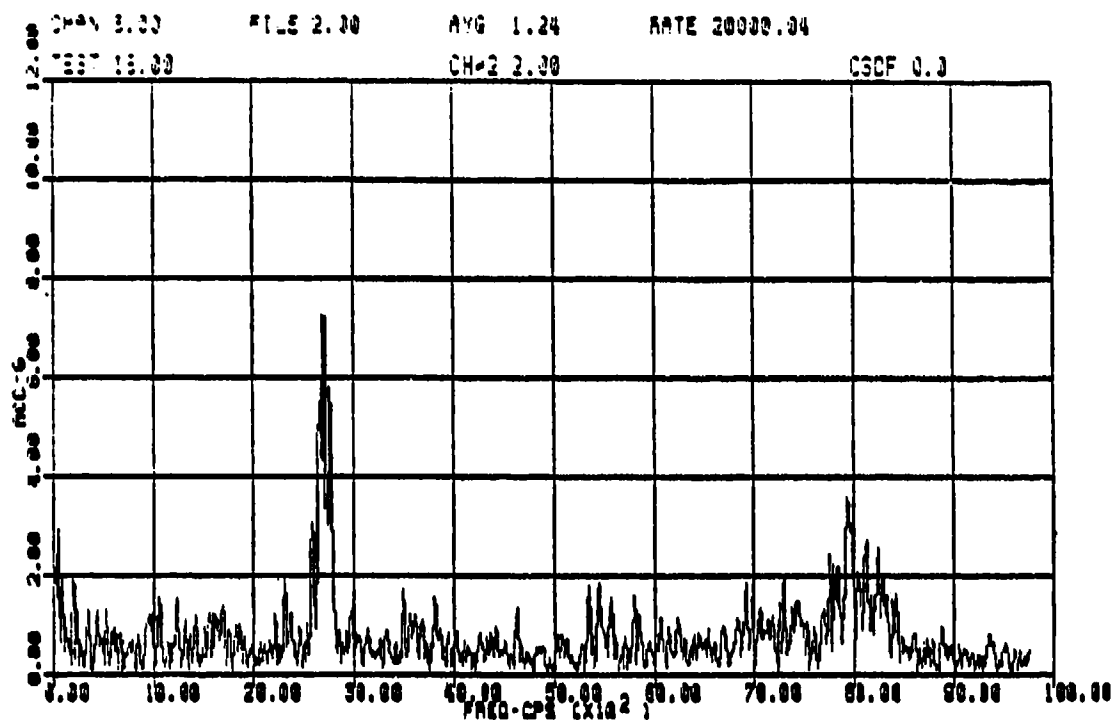


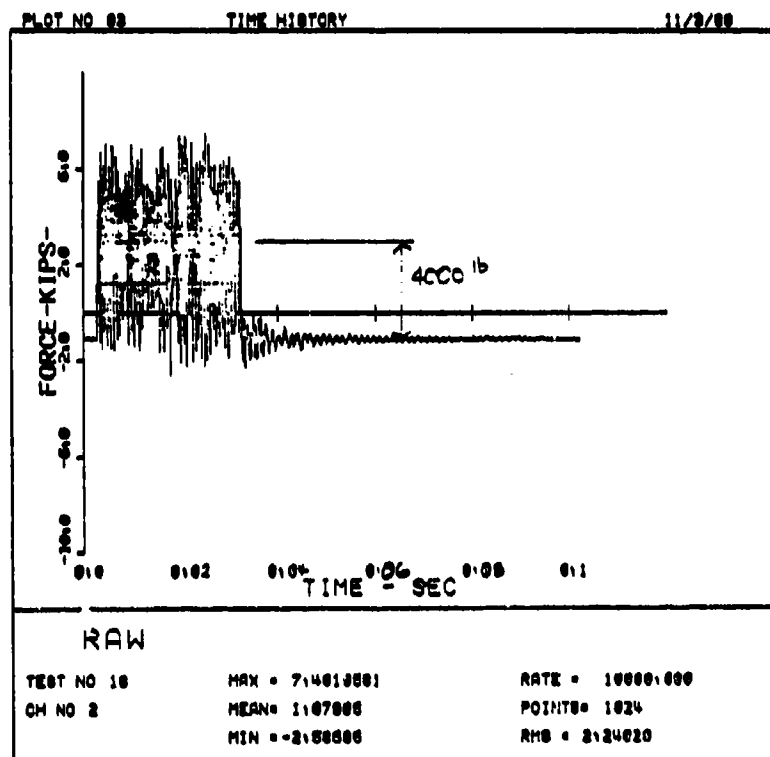
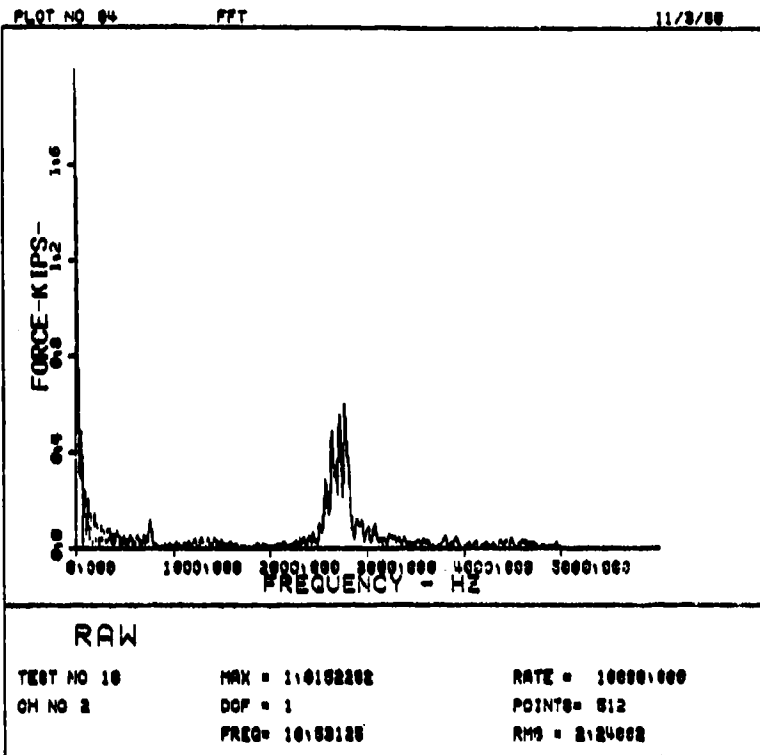








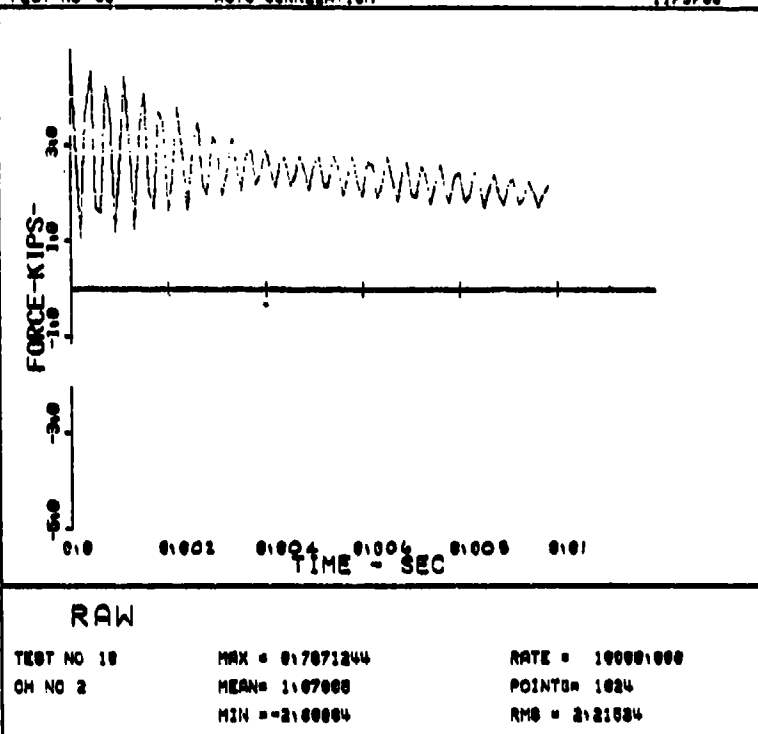




PLOT NO 83

AUTO CORRELATION

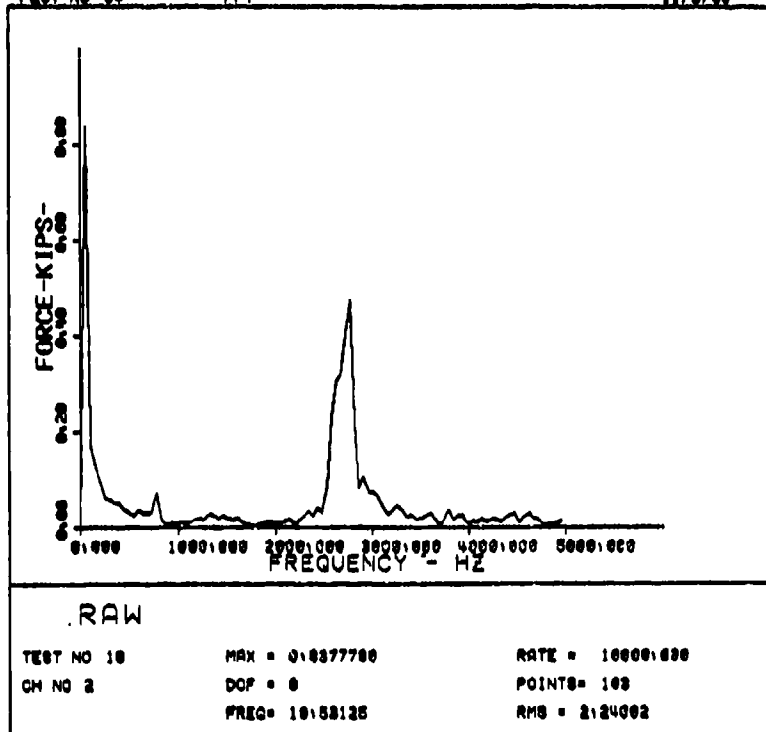
11/3/88

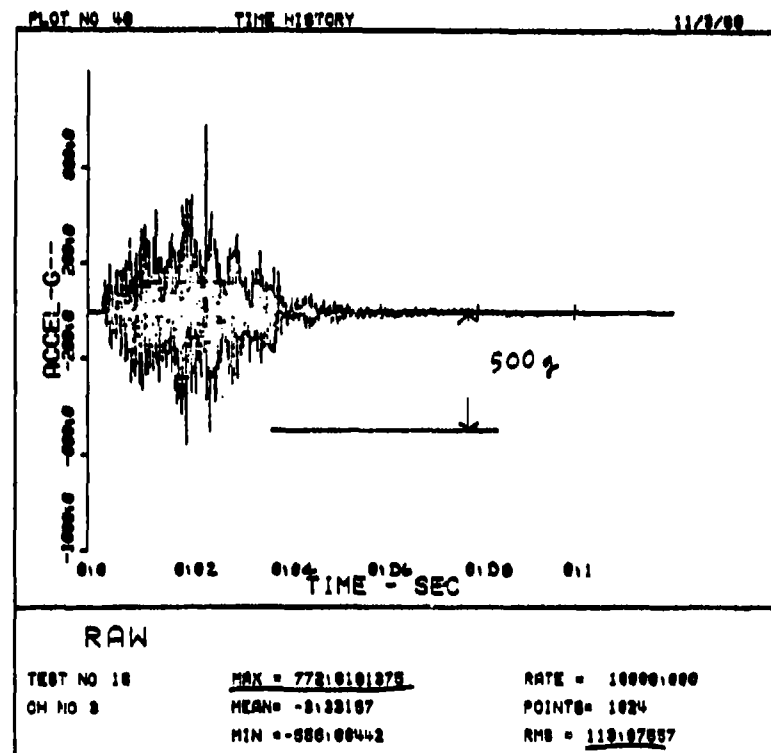
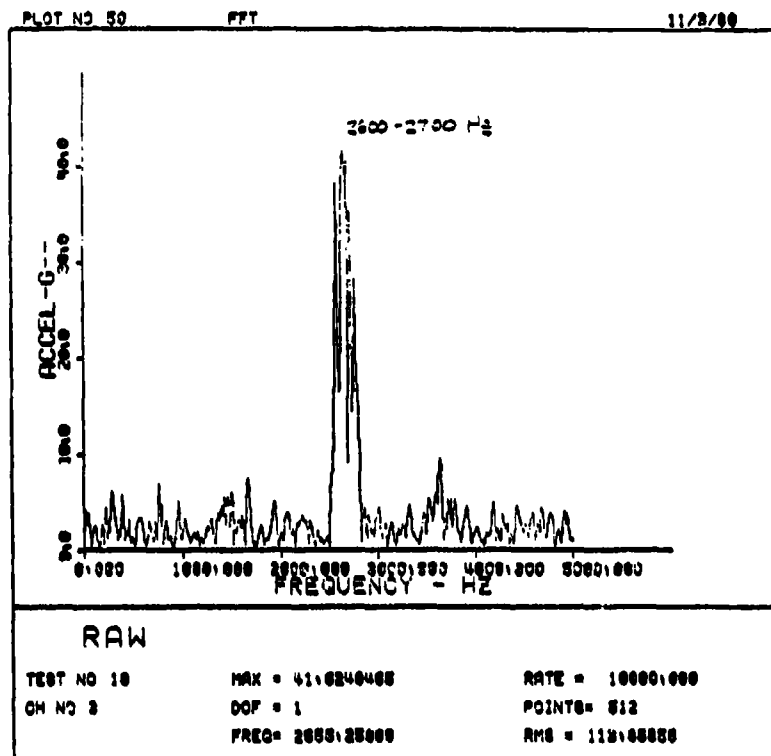


PLOT NO 84

FFT

11/3/88

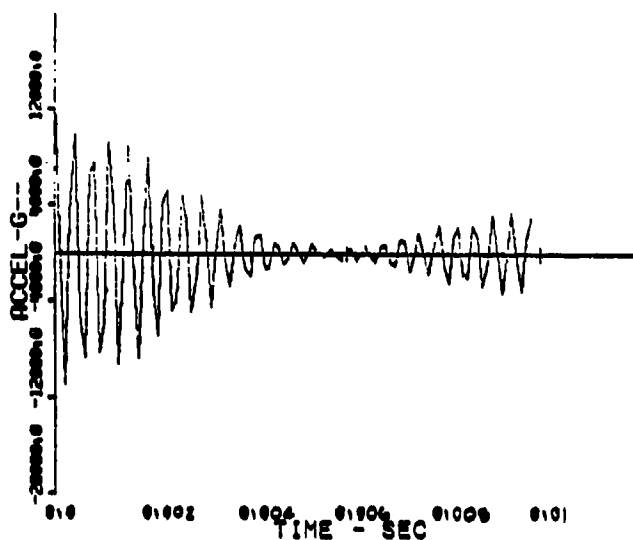




PLOT NO 57

AUTO CORRELATION

11/3/88



RAW

TEST NO 18

MAX = 8888.8722100

RATE = 10000.000

CH NO 3

MEAN = -2.33157

POINTS = 1024

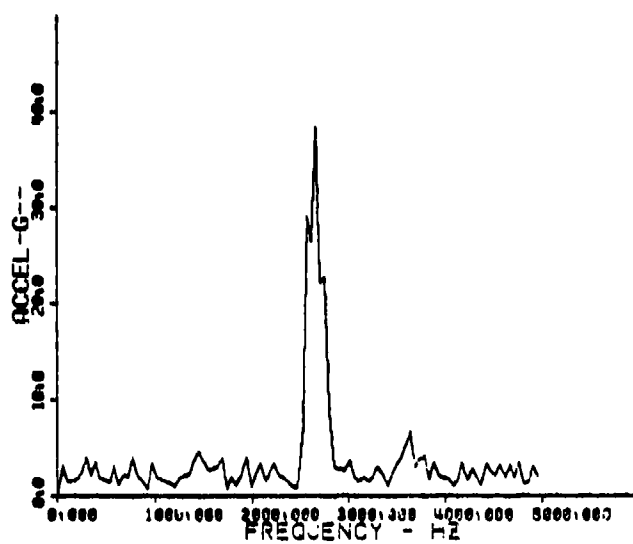
MIN = -10882.12535

RMS = 113.68858

PLOT NO 59

FFT

11/3/88



RAW

TEST NO 18

MAX = 38.4813503

RATE = 10000.000

CH NO 3

DOF = 8

POINTS = 1024

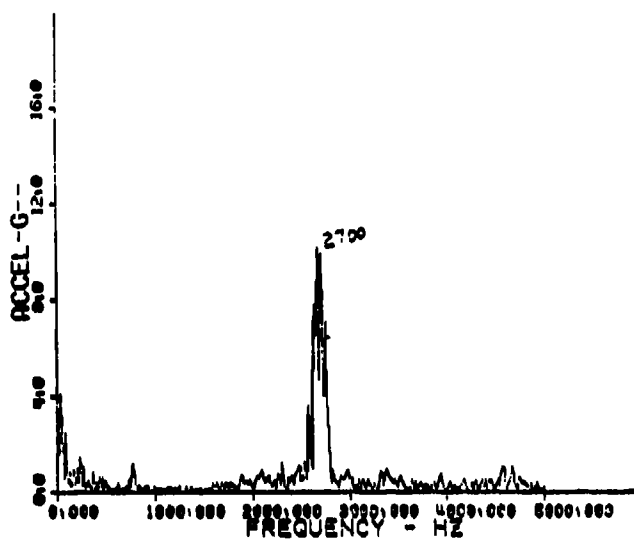
FREQ = 2500.25000

RMS = 113.68858

PLOT NO 54

FFT

11/3/89



RAW

TEST NO 10

MAX = 10.1000007

RATE = 10000.000

CH NO 4

DDF = 1

POINTS= 512

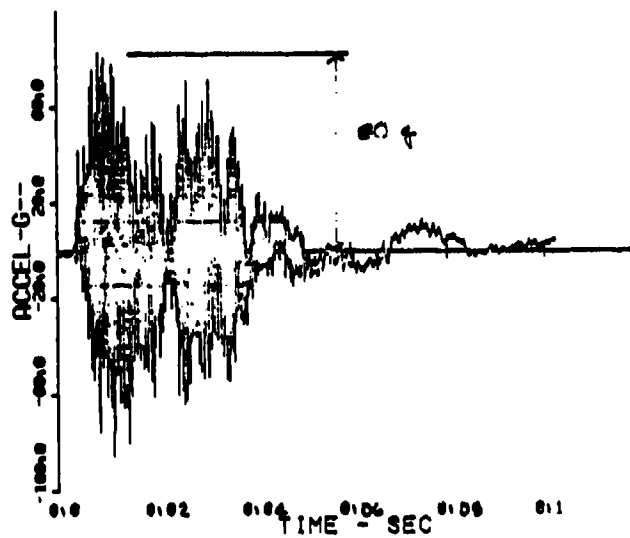
FREQ= 2000.54007

RMS = 21.00481

PLOT NO 53

TIME HISTORY

11/3/89



RAW

TEST NO 10

MAX = 42.0100040

RATE = 10000.000

CH NO 4

MEAN= -40.23000

POINTS= 1024

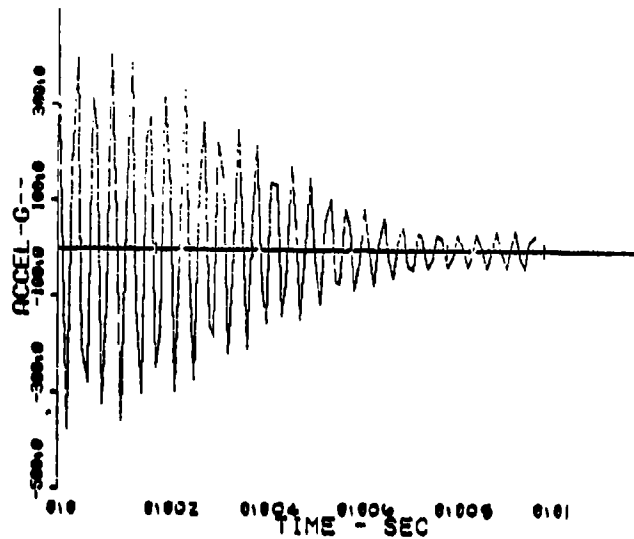
MIN = -85.40004

RMS = 21.00570

PLOT NO 53

AUTO CORRELATION

11/3/88



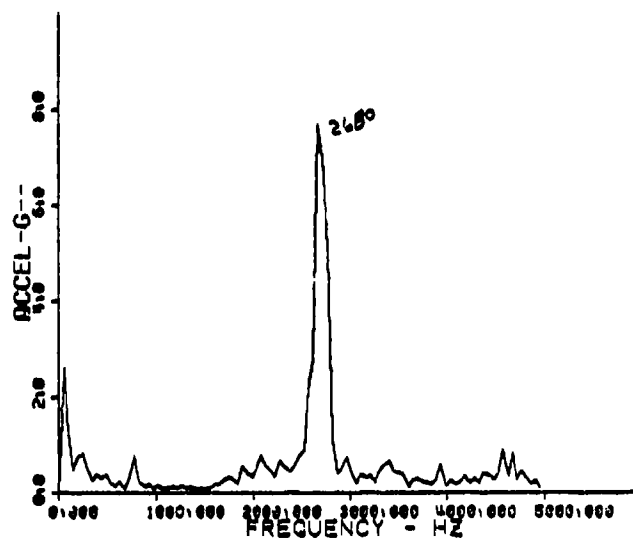
RAW

TEST NO 10
CH NO 4MAX = 488.0734003
MEAN = -48.23530
MIN = -378.66411RATE = 10000.000
POINTS = 1024
RMS = 21.72510

PLOT NO 54

FFT

11/3/88



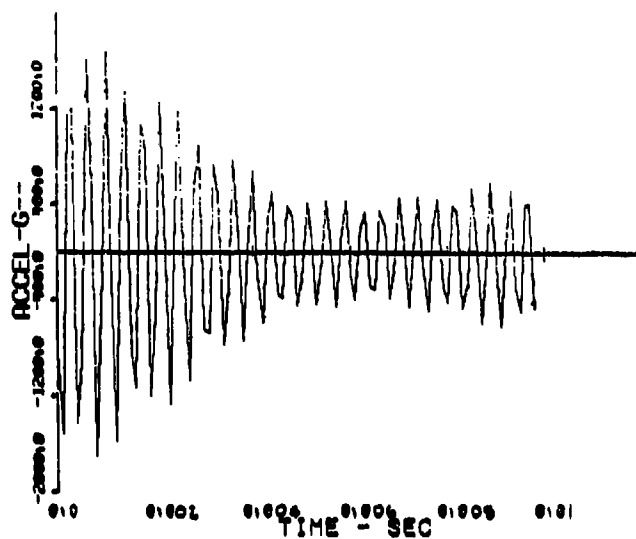
RAW

TEST NO 10
CH NO 4MAX = 7.7056200
DCP = 0
FREQ = 2680.54607RATE = 10000.000
POINTS = 1024
RMS = 21.02431

PLOT NO 59

CROSS CORRELATION

11/3/89



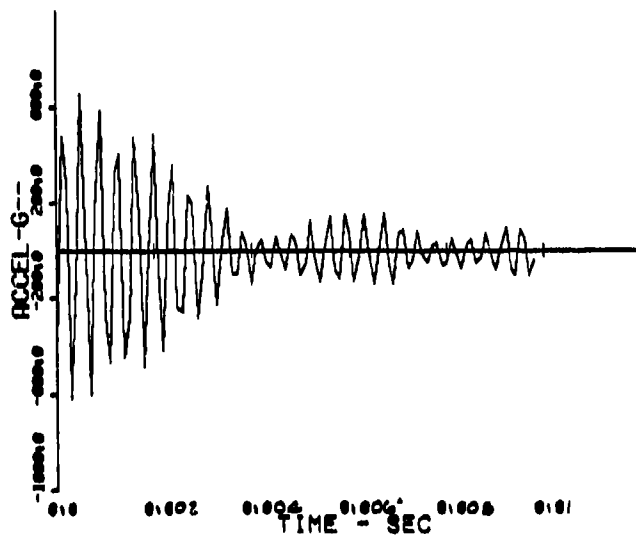
RAW

TEST NO 18
CH NO 4 & 3MAX = 1874.258281
MEAN = -48.88830
MIN = -1788.88182RATE = 10000.000
POINTS = 1024
RMS = 21.83878

PLOT NO 59

CROSS CORRELATION

11/3/89



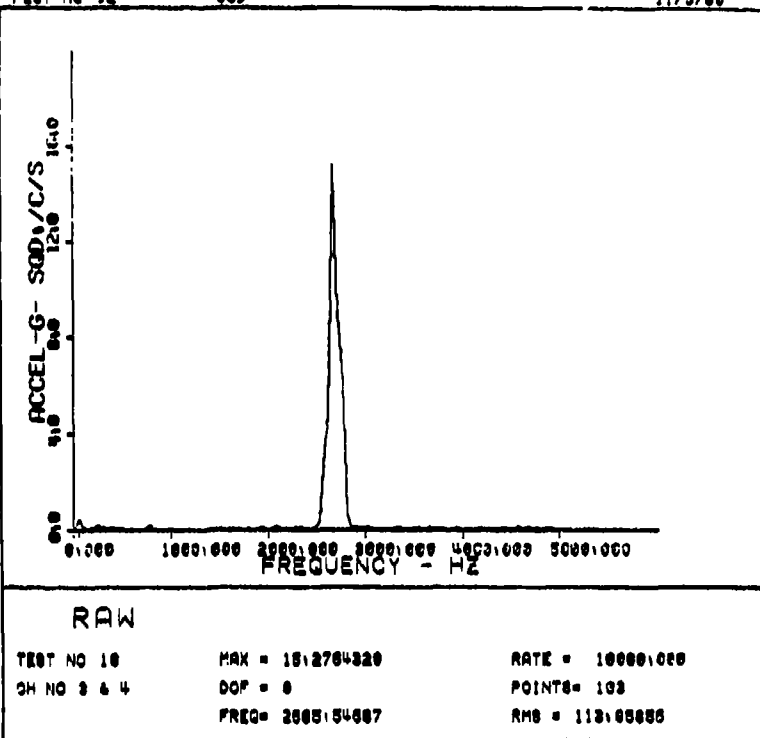
RAW

TEST NO 18
CH NO 3 & 4MAX = 686.888878
MEAN = -3.83167
MIN = -818.87388RATE = 10000.000
POINTS = 1024
RMS = 113.87557

PLOT NO 52

C80

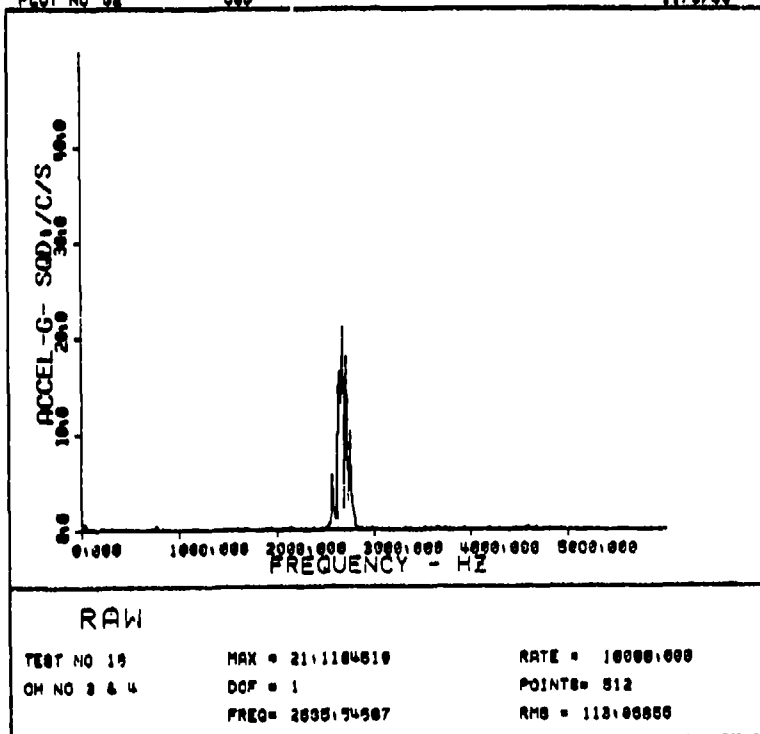
11/3/88



PLOT NO 52

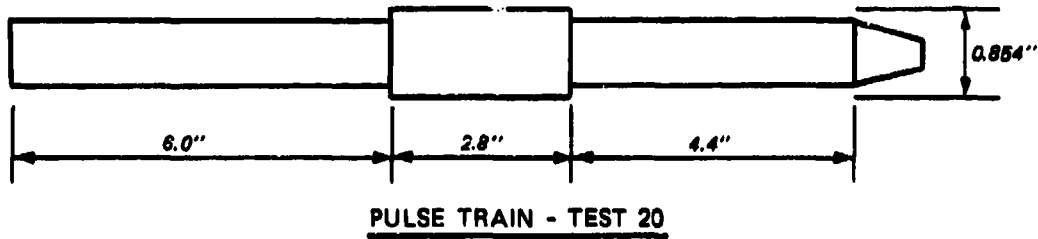
C80

11/3/88

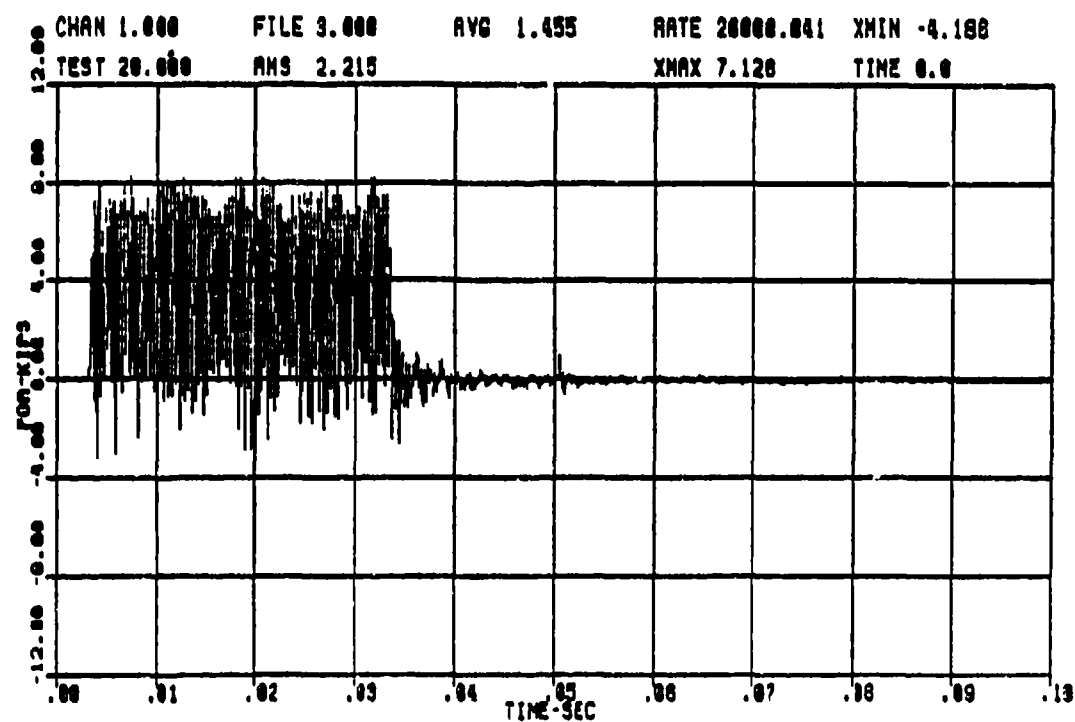
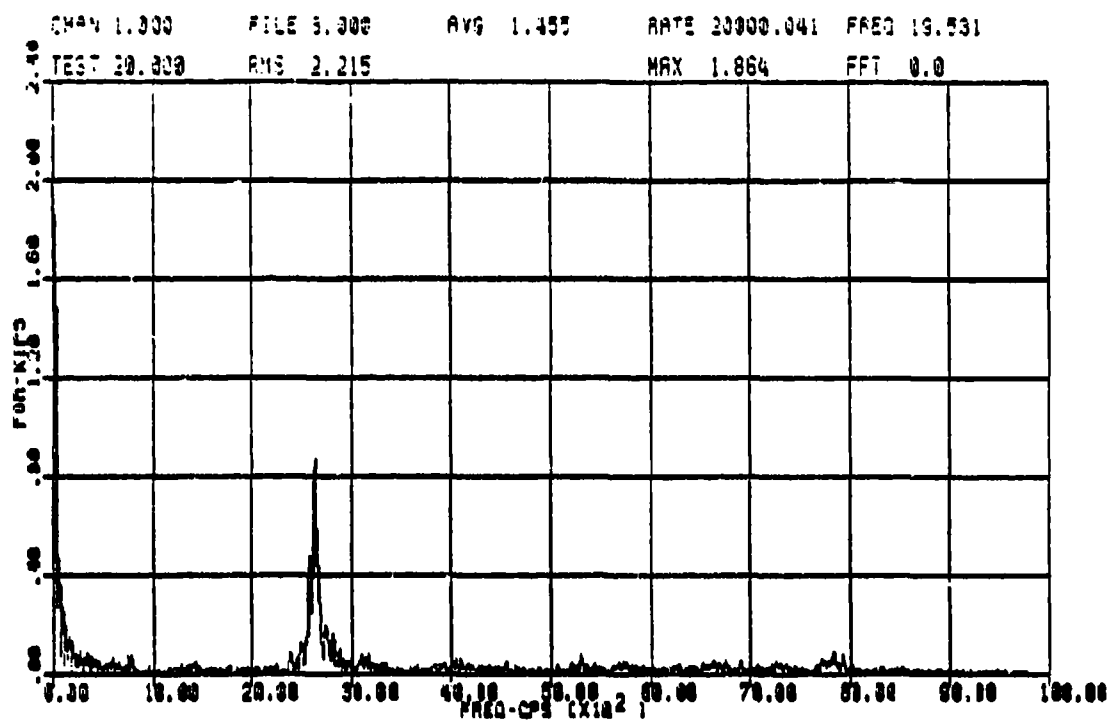


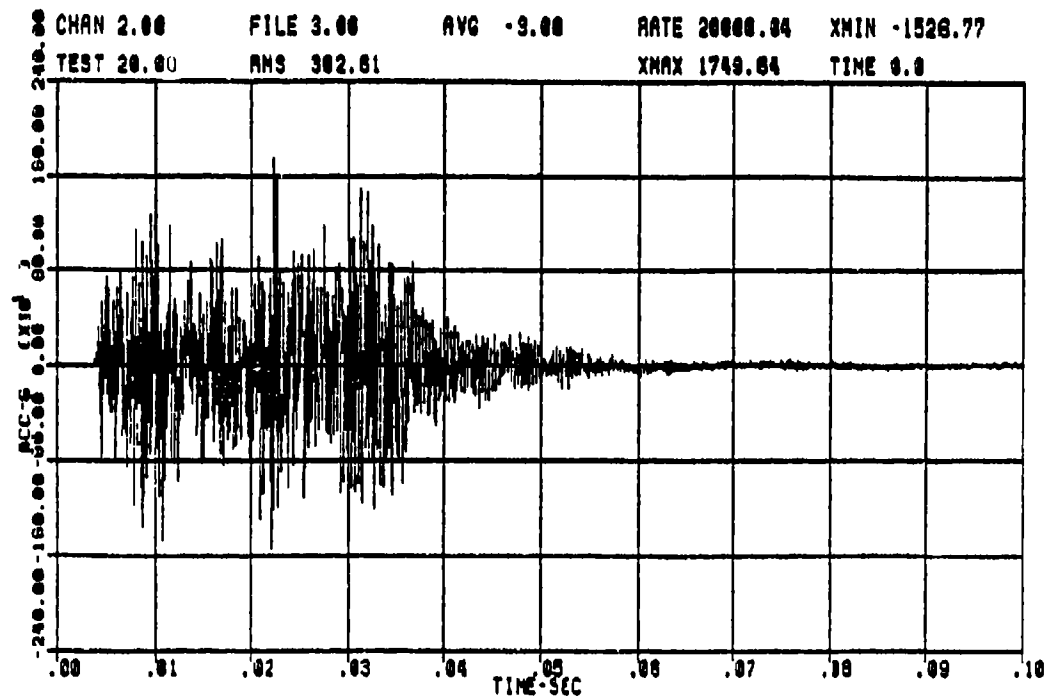
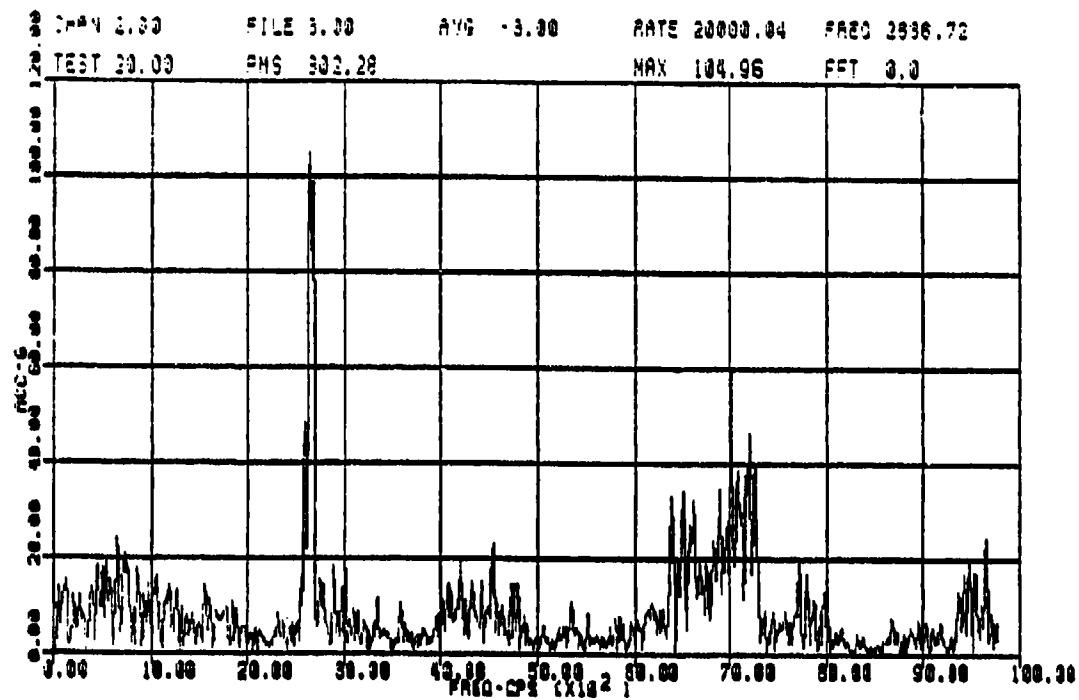
APPENDIX F: TEST 20 RESULTS

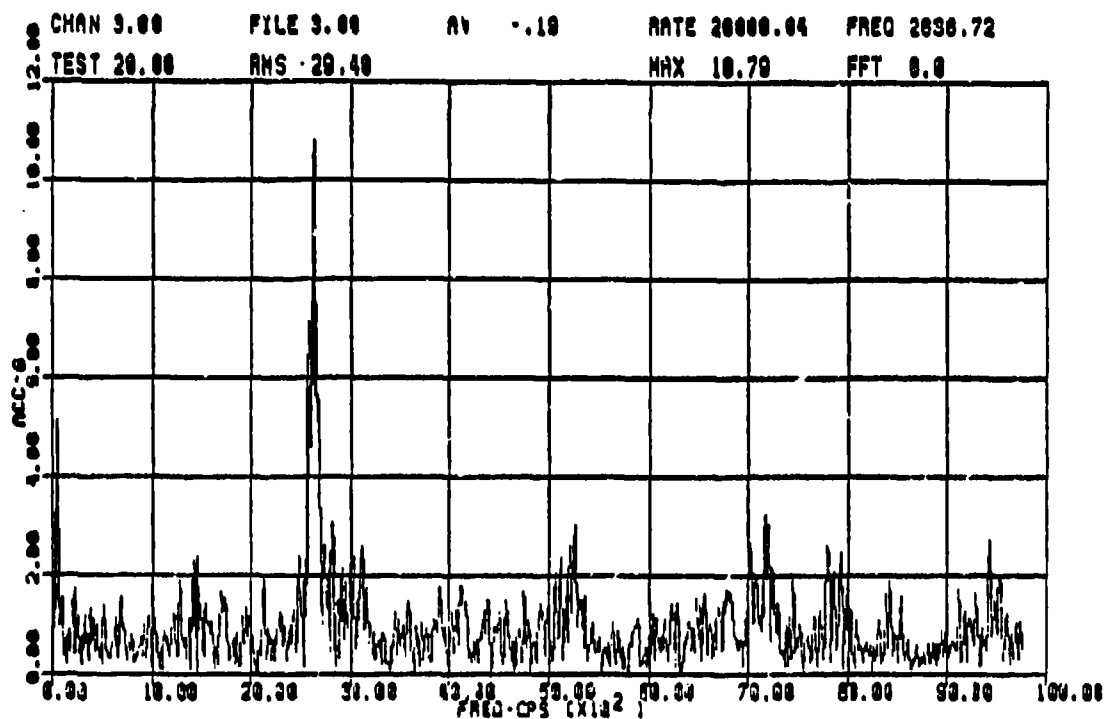
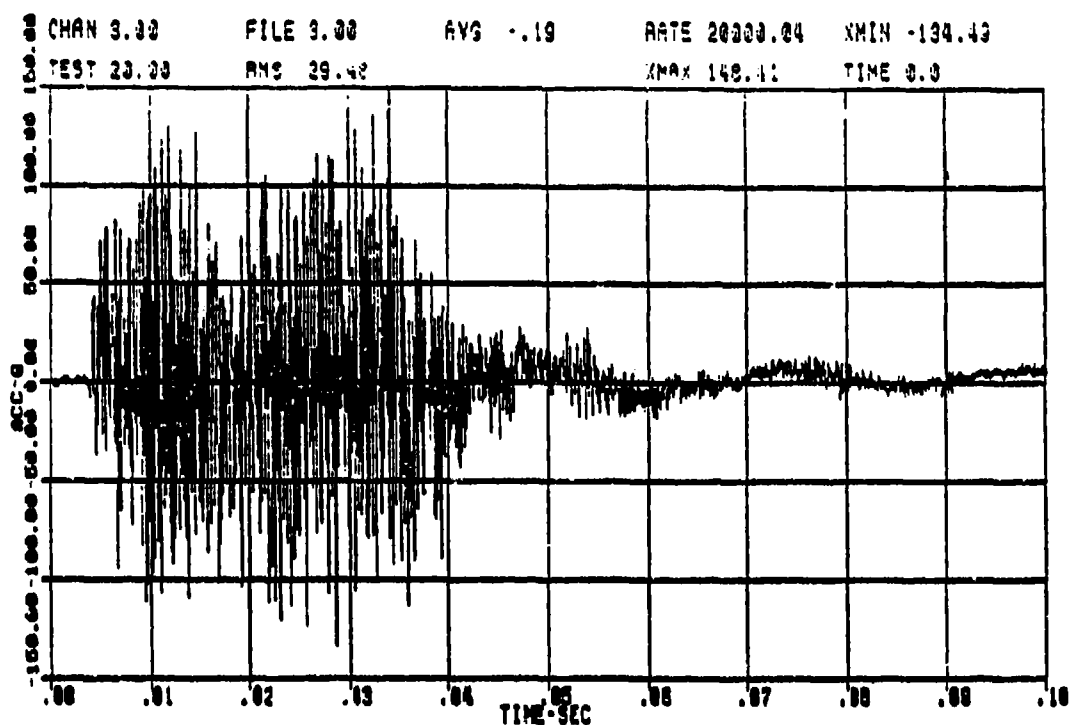
Test 20
Equipment Rack Hard-Mounted
TD660 in Rack, On-Line

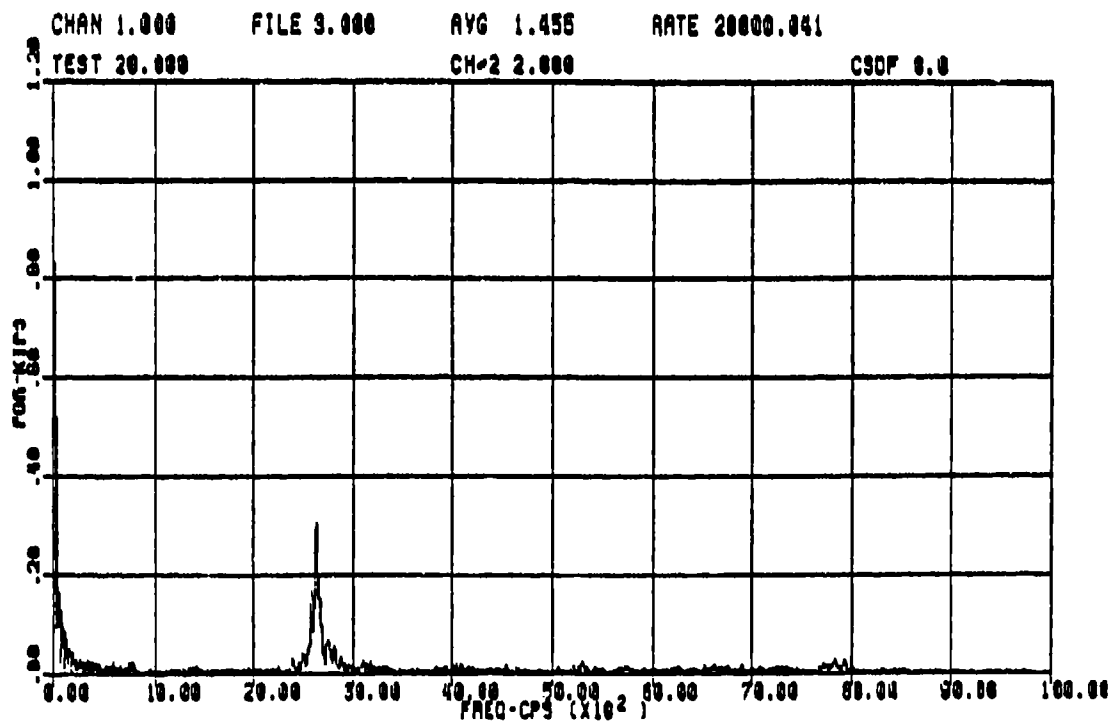
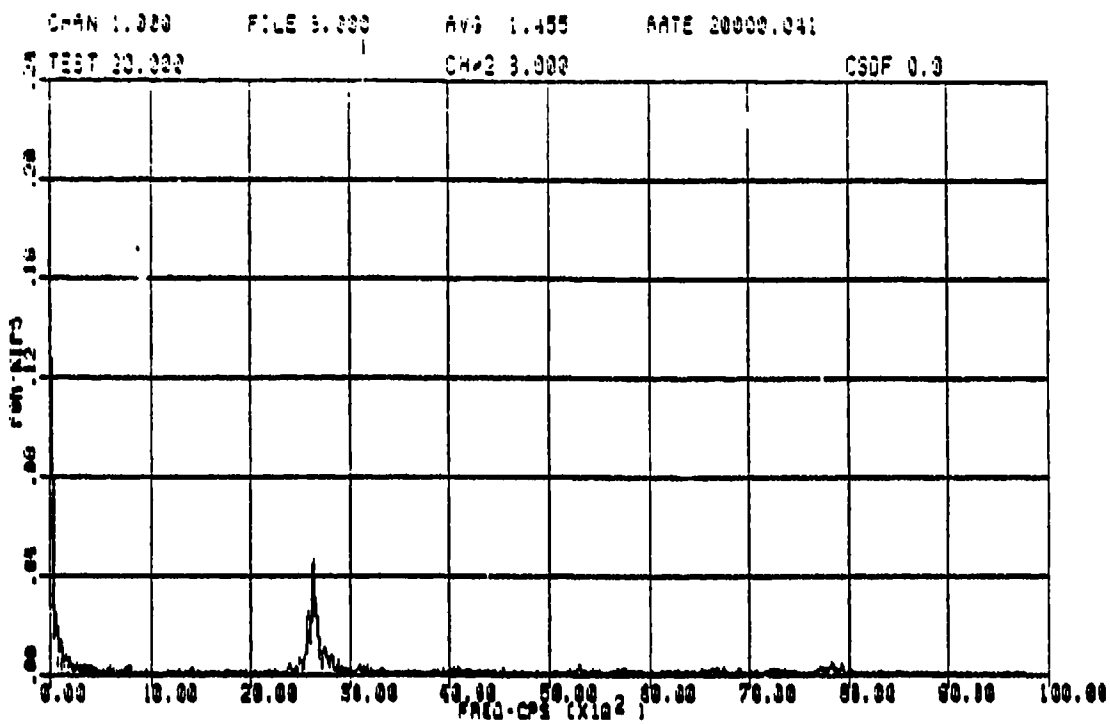


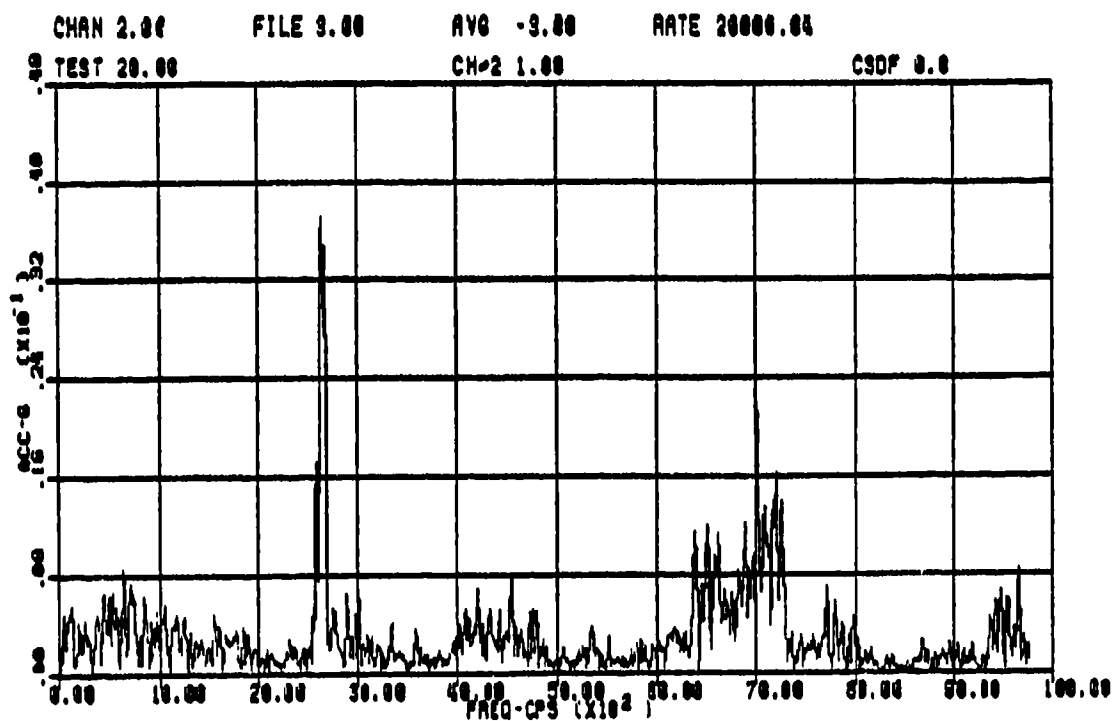
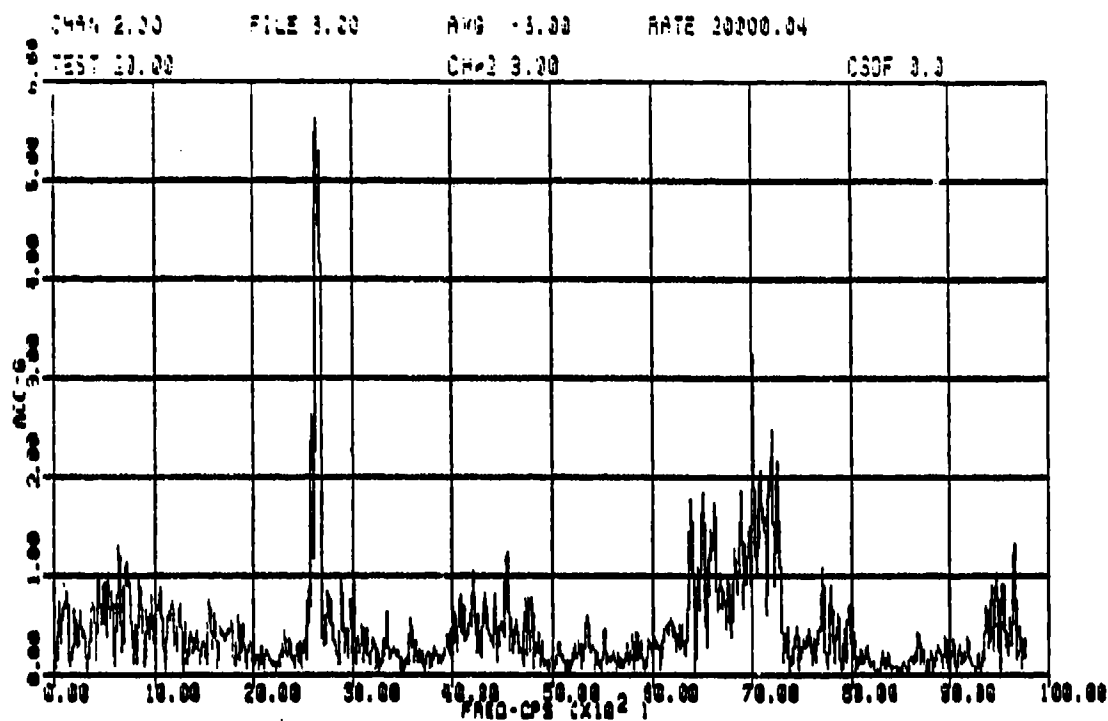
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #8½

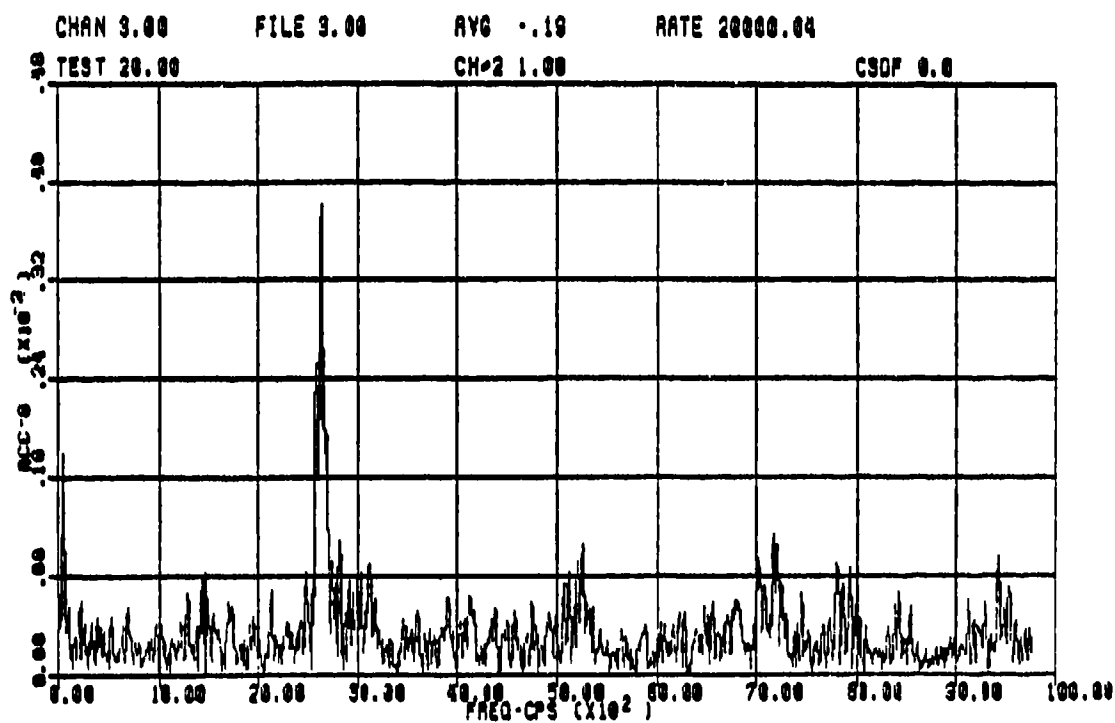
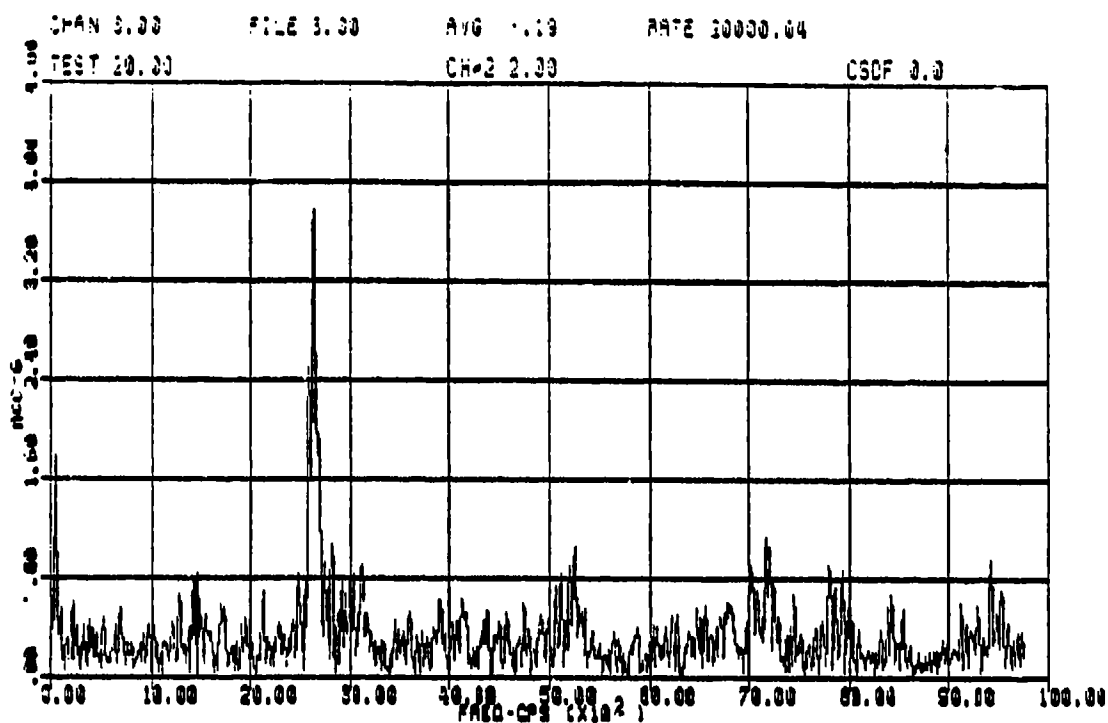








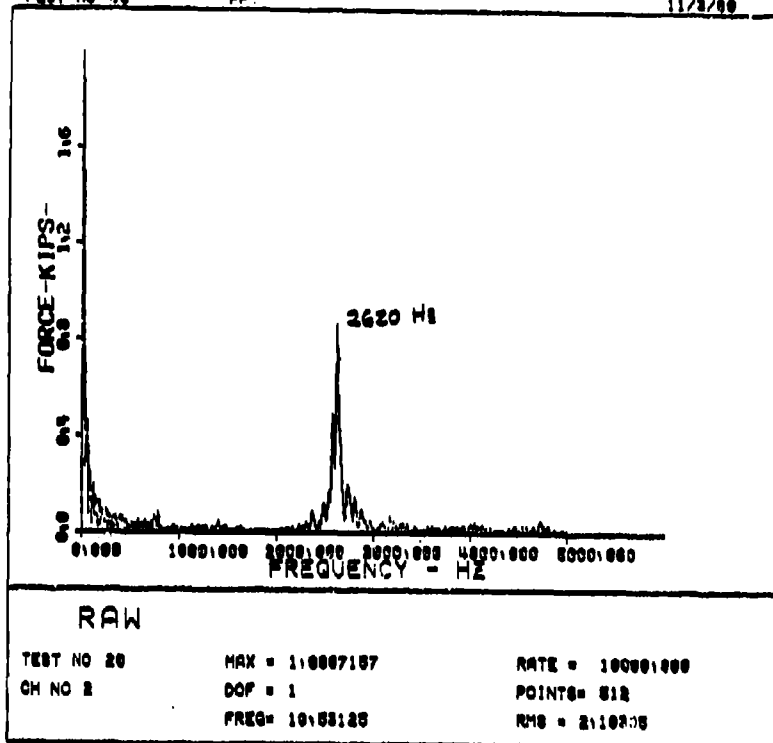




PLOT NO 88

FFT

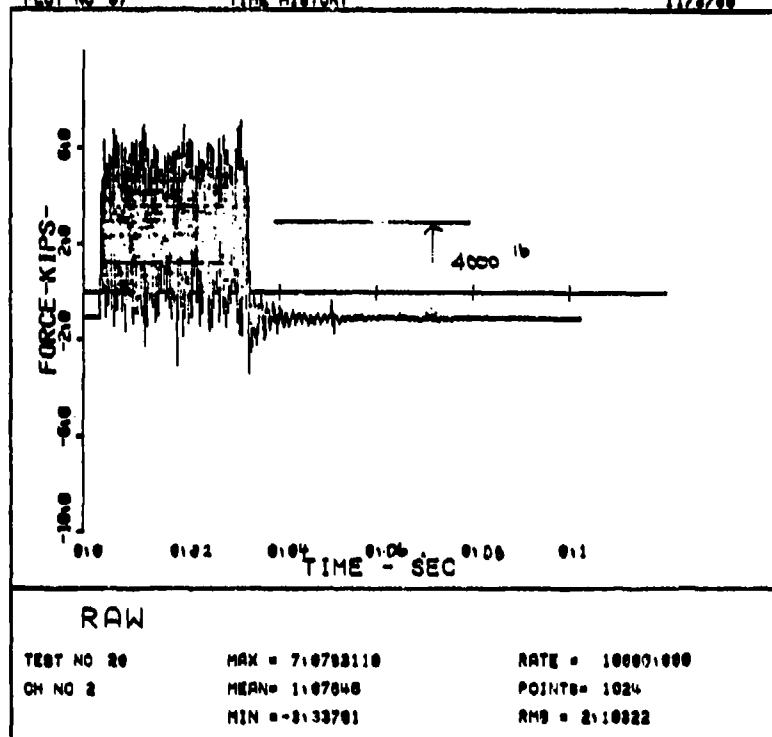
11/2/88



PLOT NO 87

TIME HISTORY

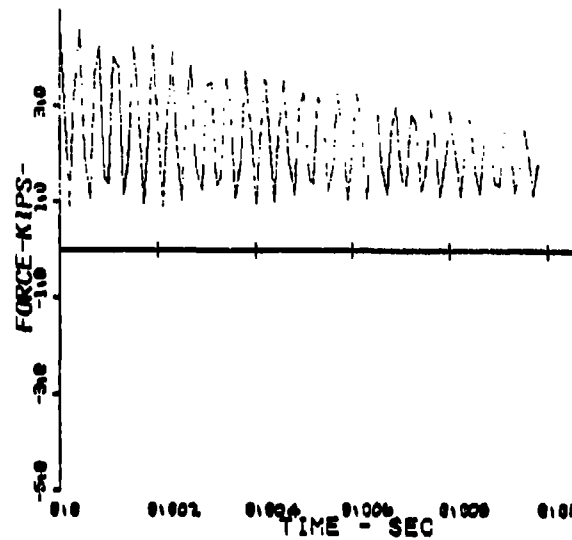
11/2/88



PLOT NO 100

AUTO CORRELATION

11/3/88



RAW

TEST NO 20
CH NO 2

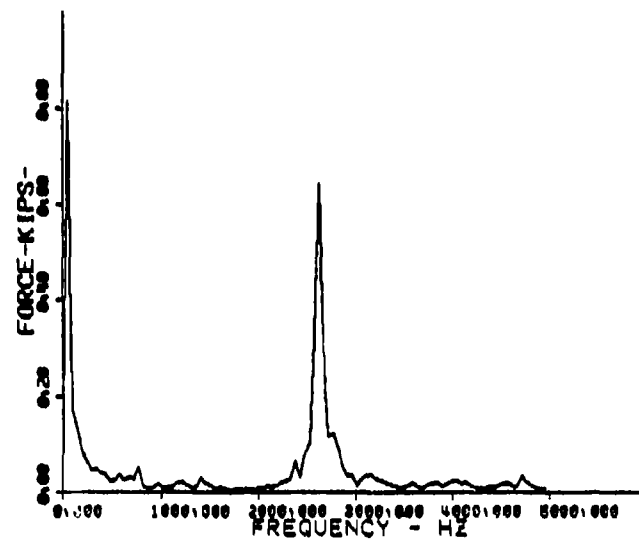
MAX = 1.0220004
MEAN = 1.07048
MIN = -2.41078

RATE = 10000.000
POINTS = 1024
RMS = 2.11748

PLOT NO 00

FFT

11/3/88



RAW

TEST NO 20
CH NO 2

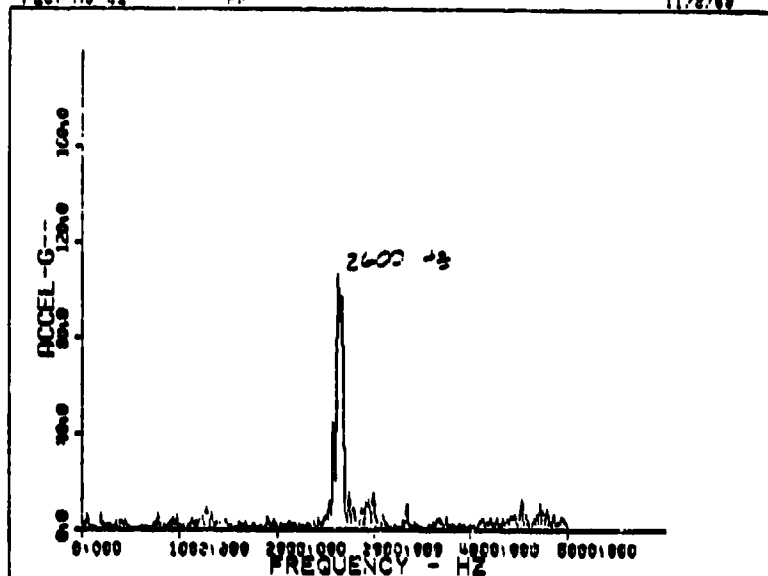
MAX = 0.6121108
DOF = 0
FREQ = 19.53125

RATE = 10000.000
POINTS = 1024
RMS = 2.110305

PLOT NO 52

FFT

11/2/89



RAW

TEST NO 20

MAX = 108.140020

RATE = 10000.000

CH NO 8

DCP = 1

POINTS= 512

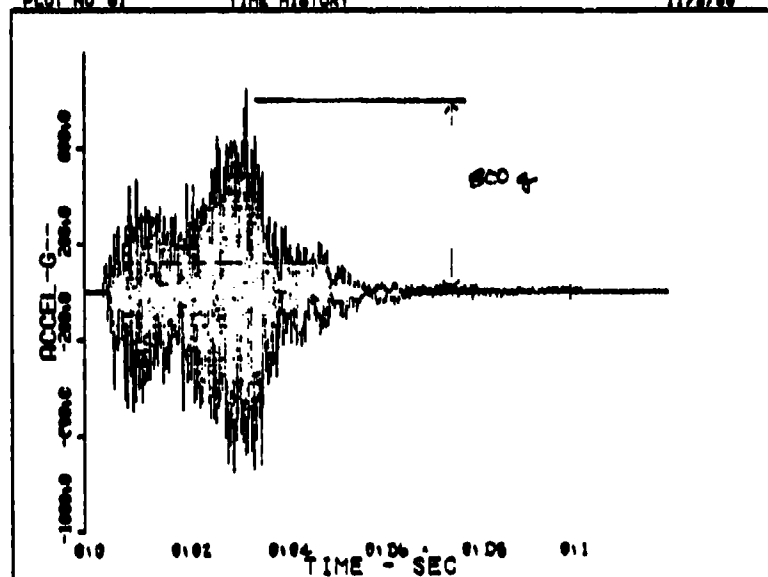
FREQ= 2626.71875

RMS = 184.27840

PLOT NO 51

TIME HISTORY

11/2/89



RAW

TEST NO 20

MAX = 844.870020

RATE = 10000.000

CH NO 8

MEAN= -6.78629

POINTS= 1024

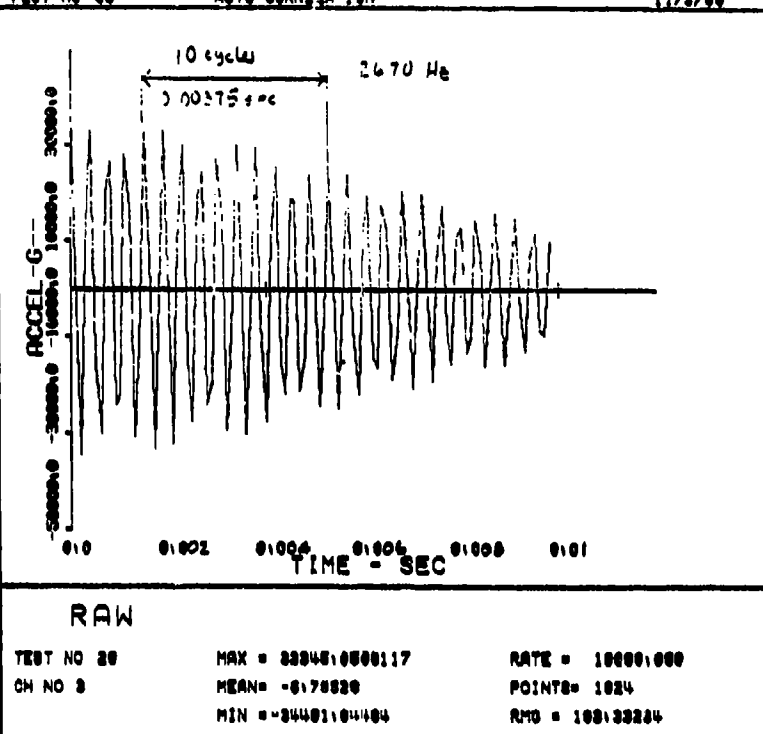
MIN = -782.12411

RMS = 194.13734

PLOT NO 00

AUTO CORRELATION

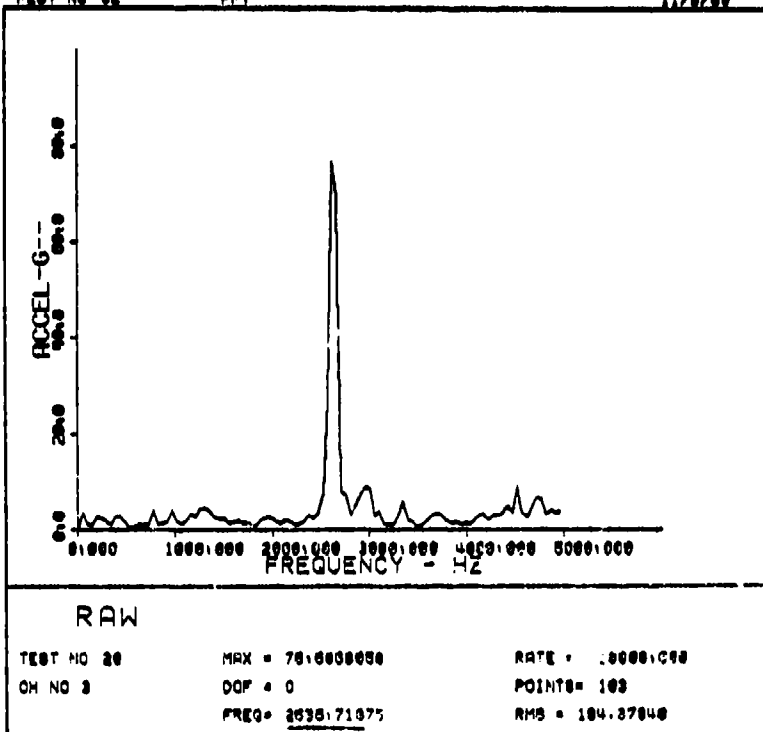
11/2/88



PLOT NO 00

FFT

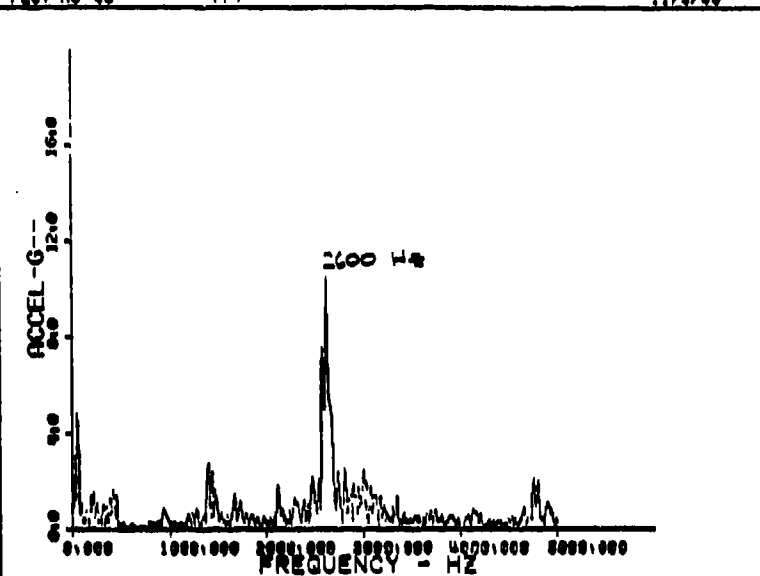
11/2/88



PLOT NO 88

FFT

11/2/88



RAW

TEST NO 30

MAX = 10.817000

RATE = 10000.000

CH NO 4

DOF = 1

POINTS = 512

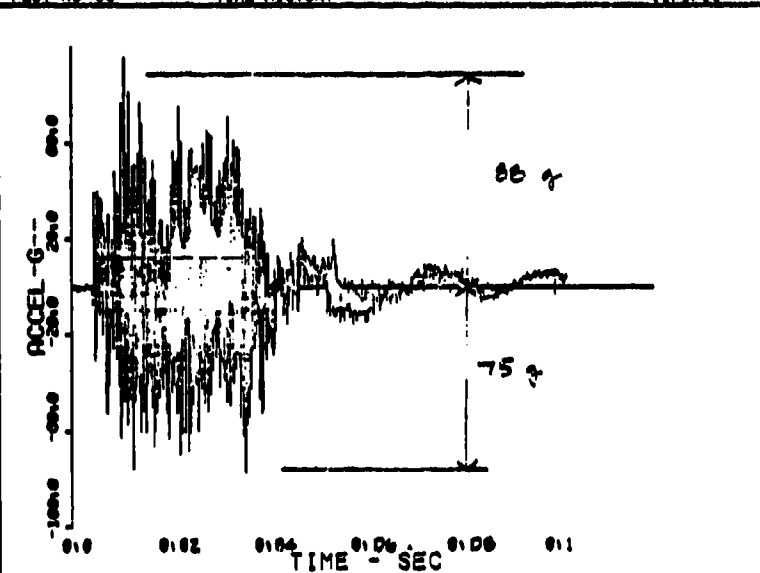
FREQ = 2620.00312

RMS = 21.03040

PLOT NO 88

TIME HISTORY

11/2/88



RAW

TEST NO 30

MAX = 85.888204

RATE = 10000.000

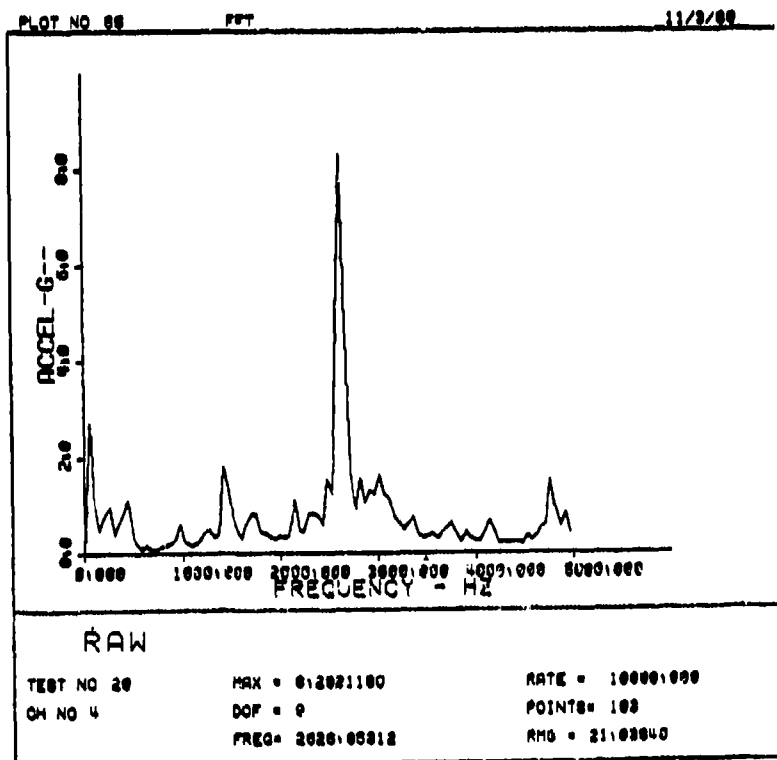
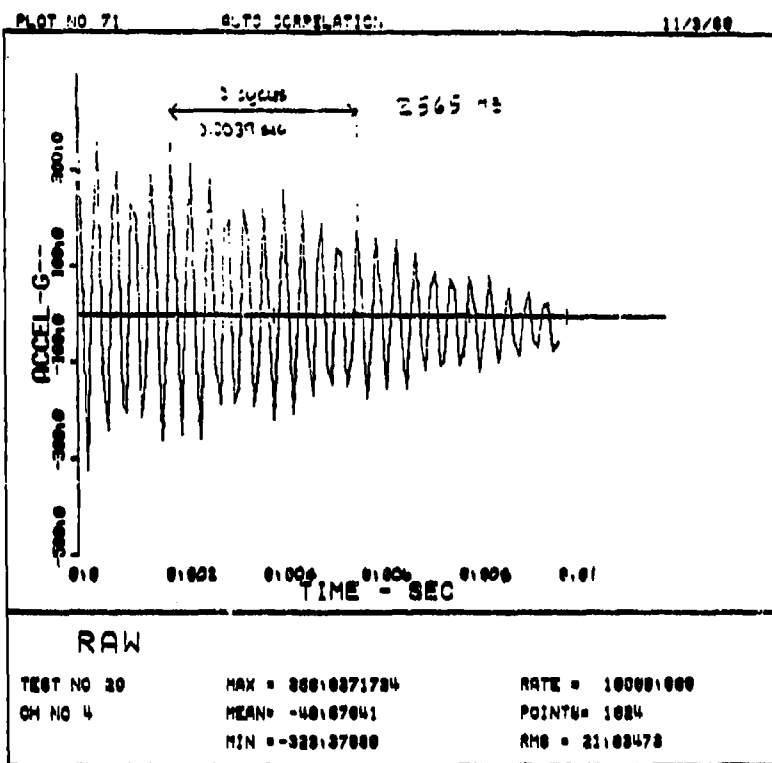
CH NO 4

MEAN = -40.67041

POINTS = 1024

MIN = -78.00300

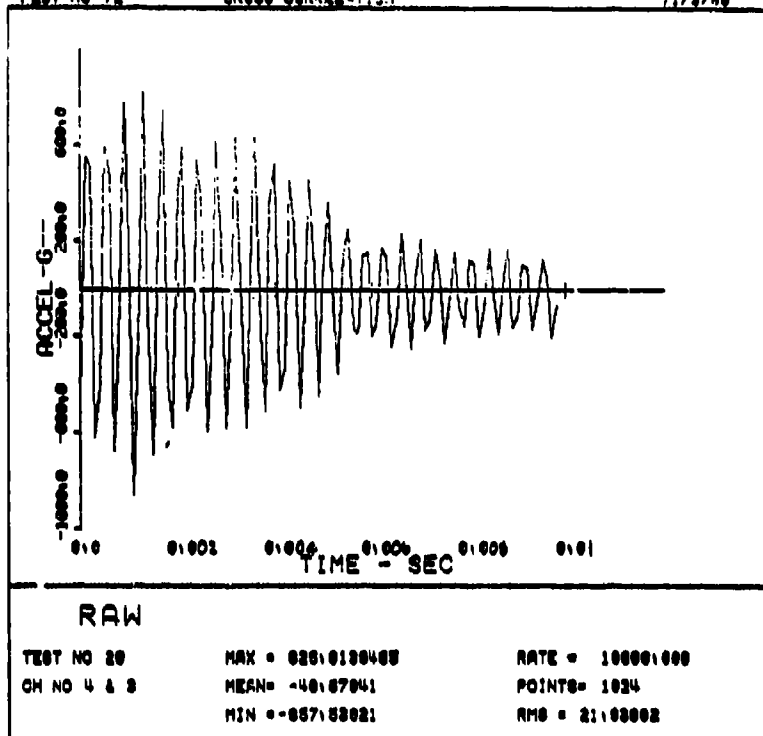
RMS = 21.03002



PLOT NO 72

CROSS CORRELATION

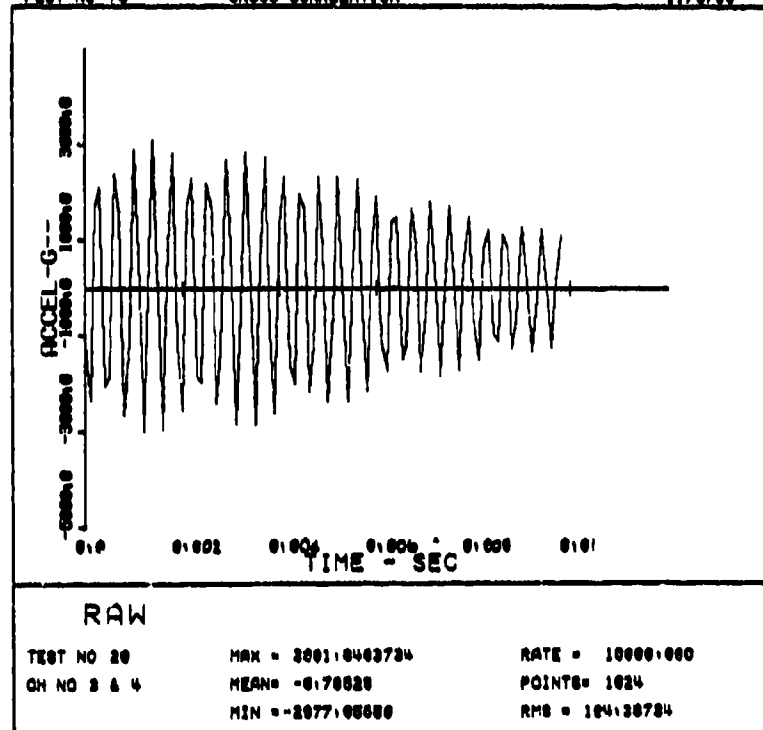
11/3/88



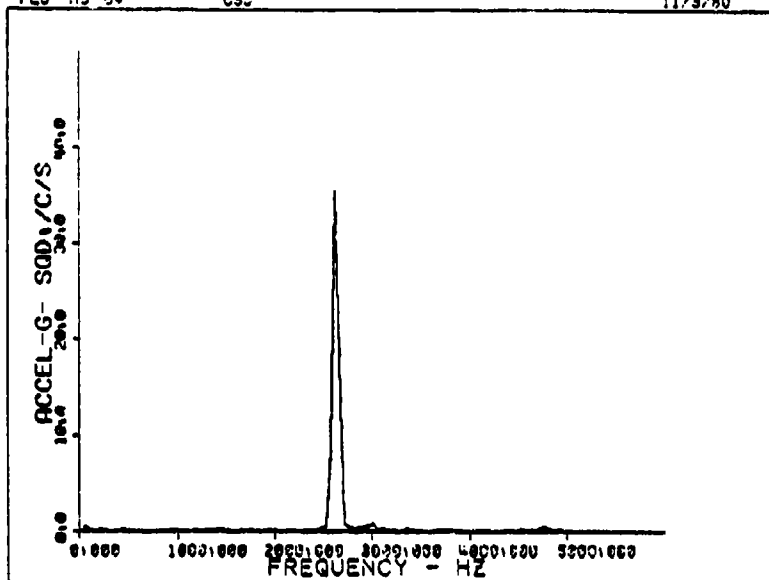
PLOT NO 73

CROSS CORRELATION

11/3/88



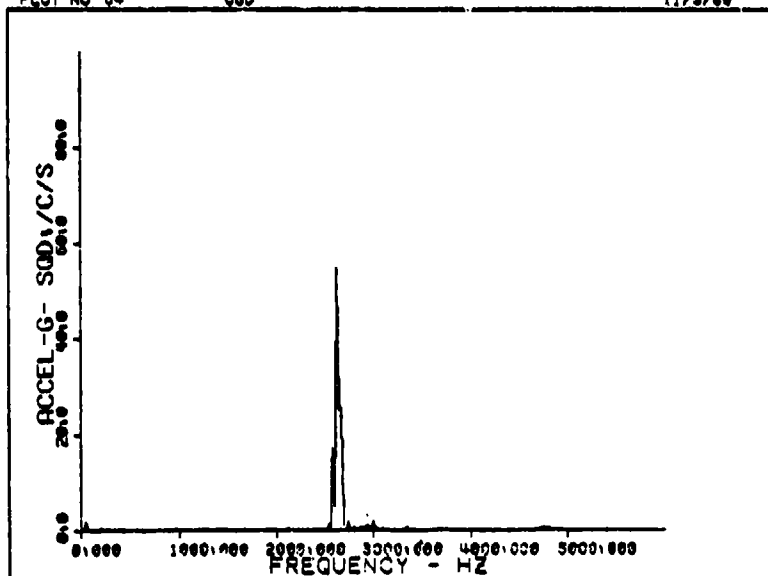
PLOT NO 54 CSD 11/3/80



RAW

TEST NO 20	MAX = 35.4580804	RATE = 10000.000
CH NO 3 & 4	DOF = 0	POINTS= 103
	FREQ= 2538.71875	RMS = 104.37840

PLOT NO 54 CSD 11/3/80



RAW

TEST NO 20	MAX = 54.7763008	RATE = 10000.000
CH NO 3 & 4	DOF = 1	POINTS= 512
	FREQ= 2538.71875	RMS = 104.37840

APPENDIX G: TEST 21 RESULTS

Test 21
Equipment Rack Soft-Mounted
AN/GRC-103 in Rack, Off-Line

Plot Heading Nomenclature (Tests 21-25)

CHAN 1 - Input force

CHAN 2 - Rack acceleration

CHAN 3 - Equipment acceleration

RMS, AVG, MAX, XMAX, XMIN - RMS, average, maximum, and minimum values
of data plots

FREQ - Frequency at which maximum value occurs

FFT 0.0 - Fast Fourier transform of time history

TIME 0.0 - Time history record

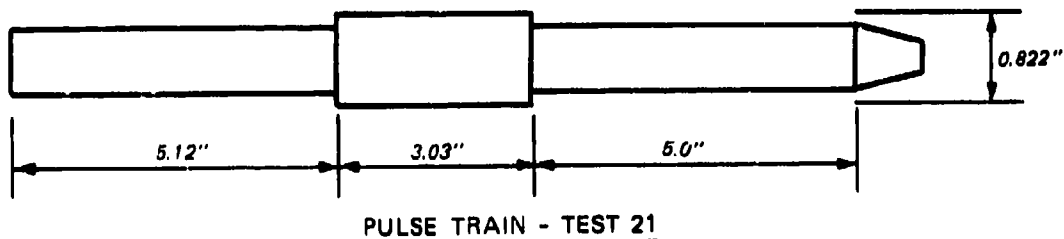
CSDF 0.0 - Cross spectral density function

CH/2 1.0 Channel number of the second channel for plots involving

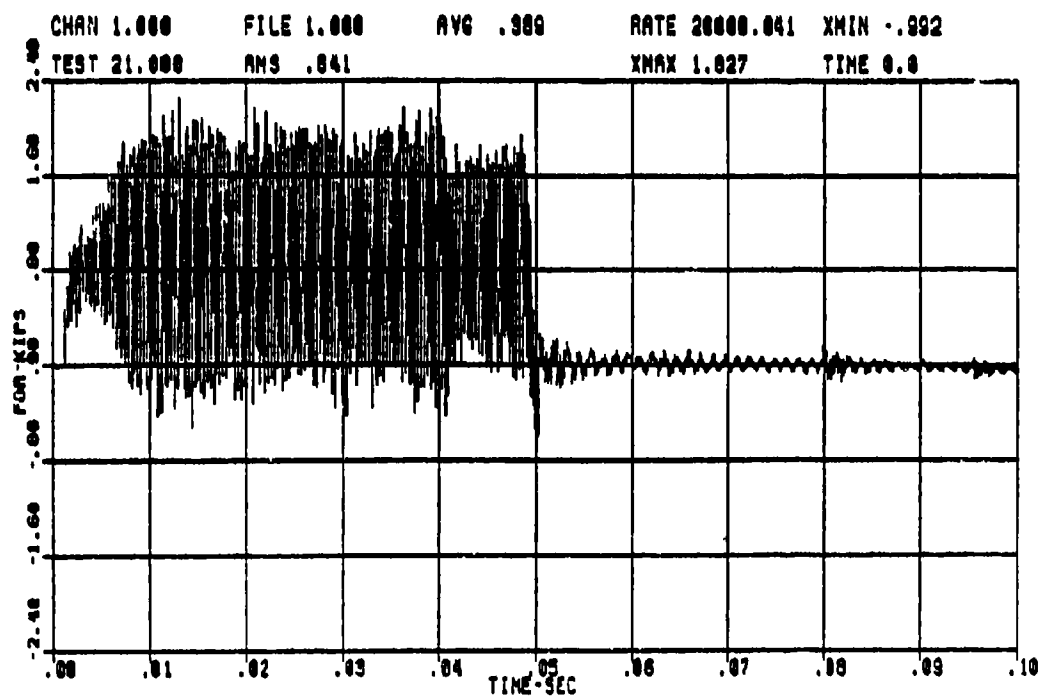
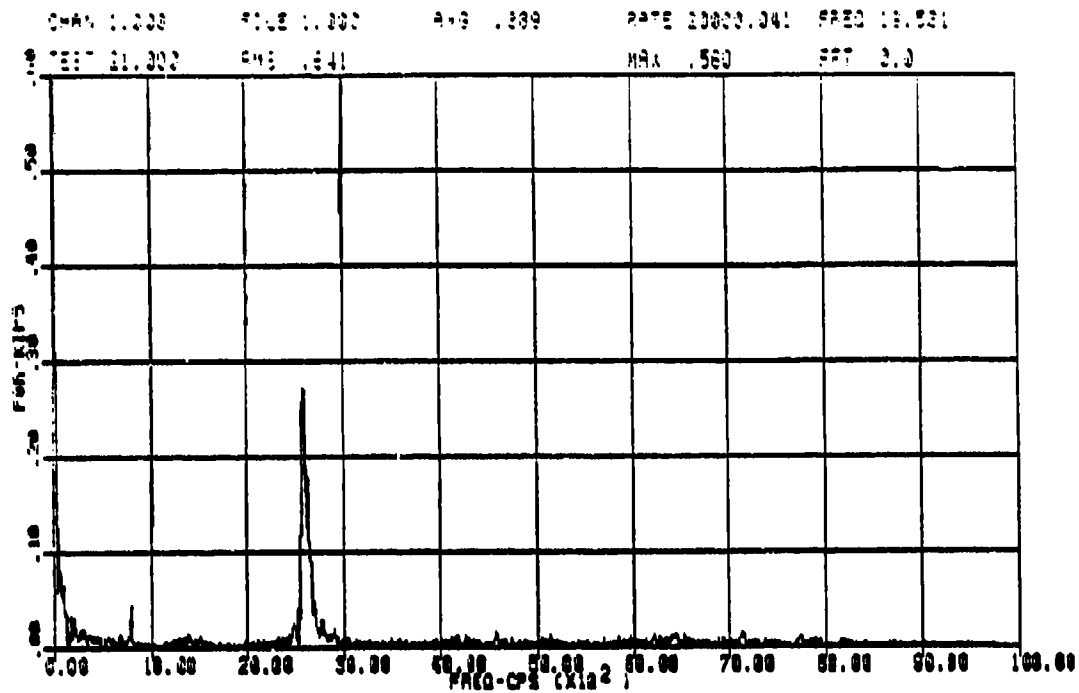
CH/2 2.0 two-channel functions (CSDF)

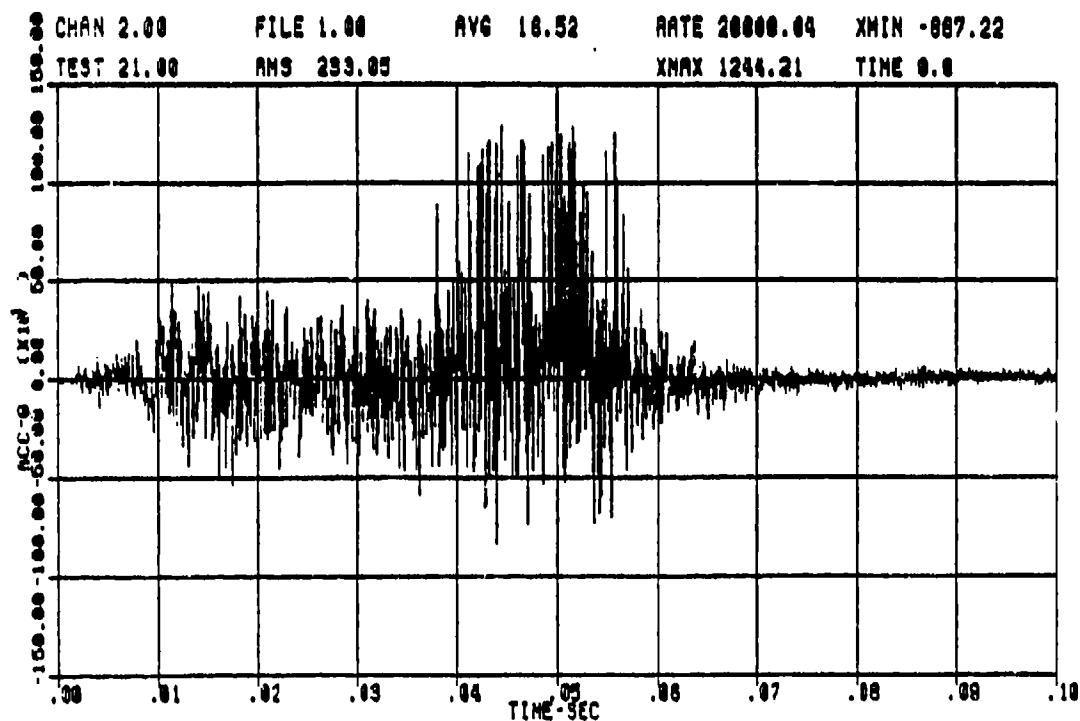
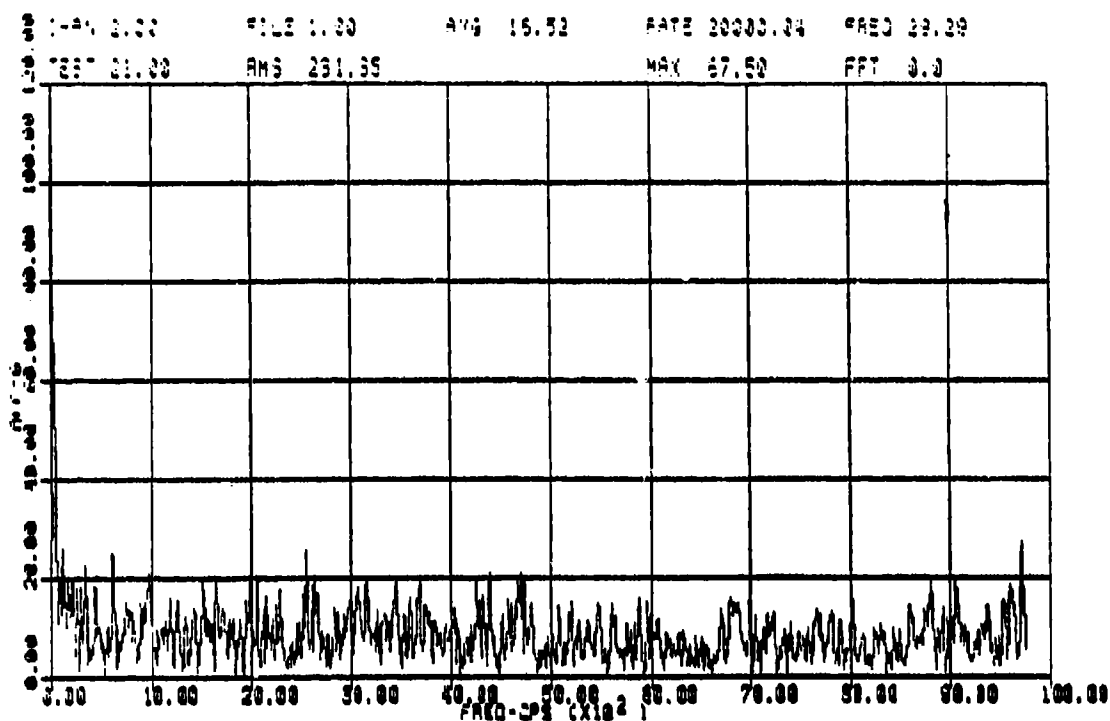
CH/2 3.0

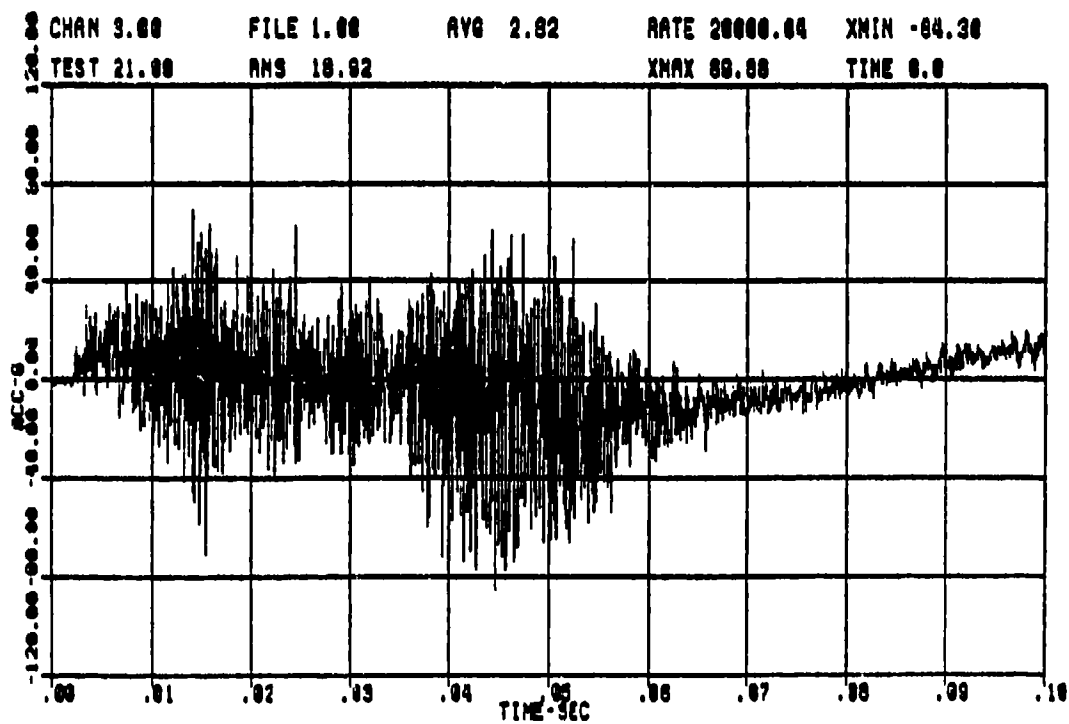
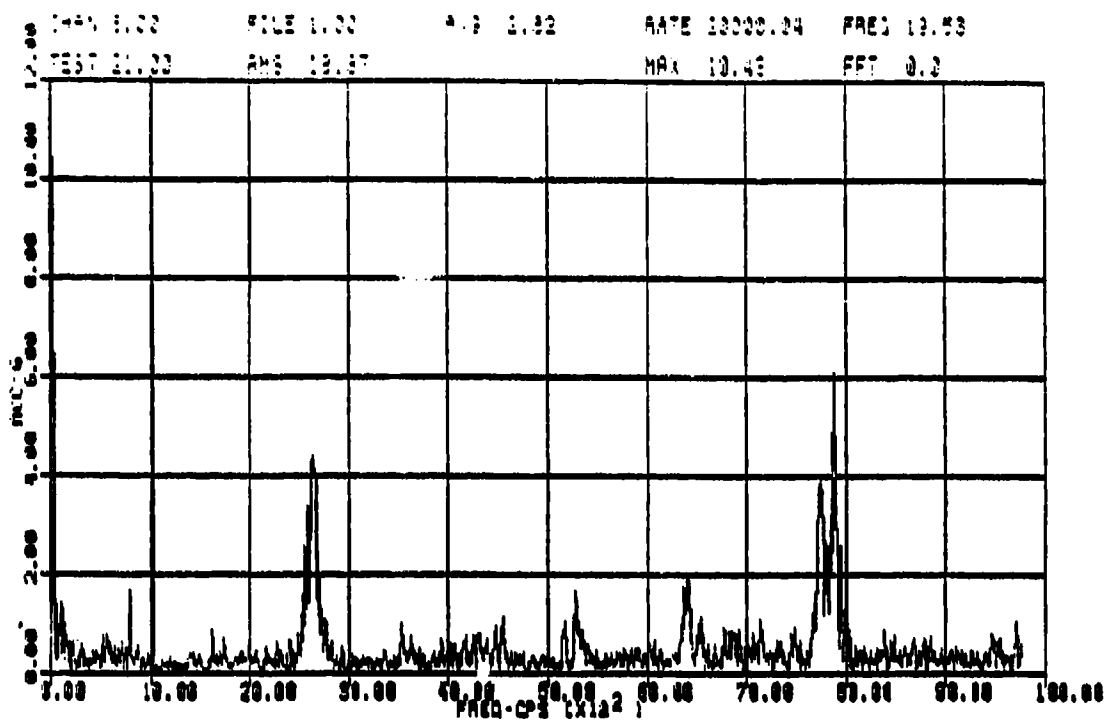
RATE - Digitizing rate, samples per second

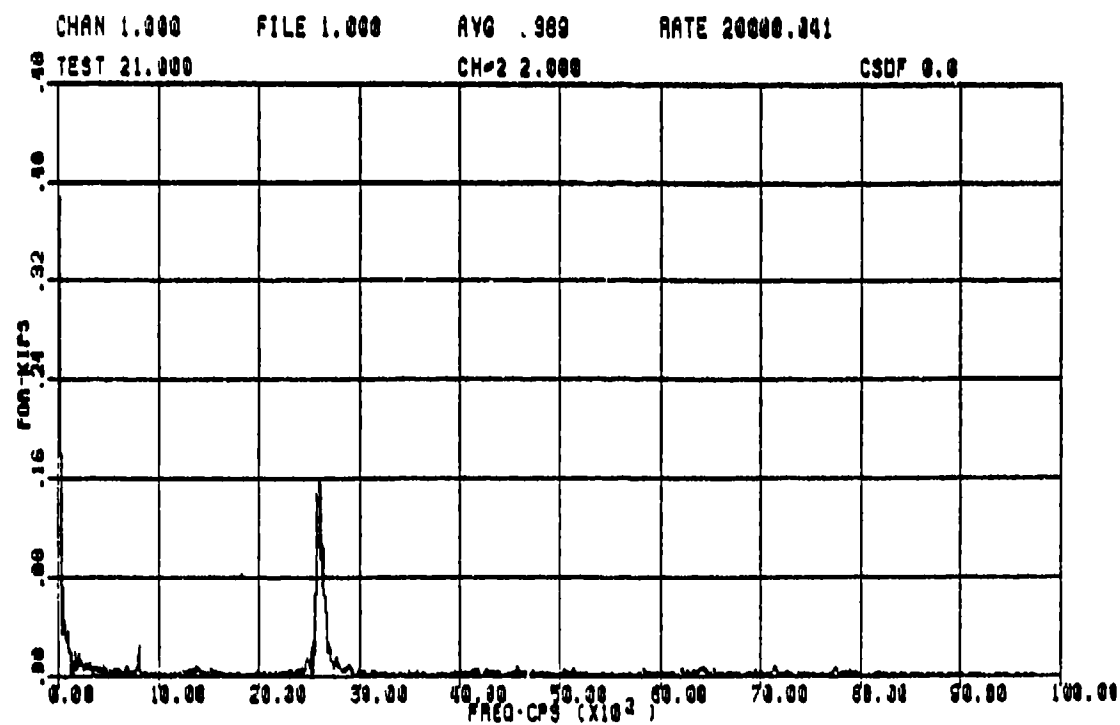
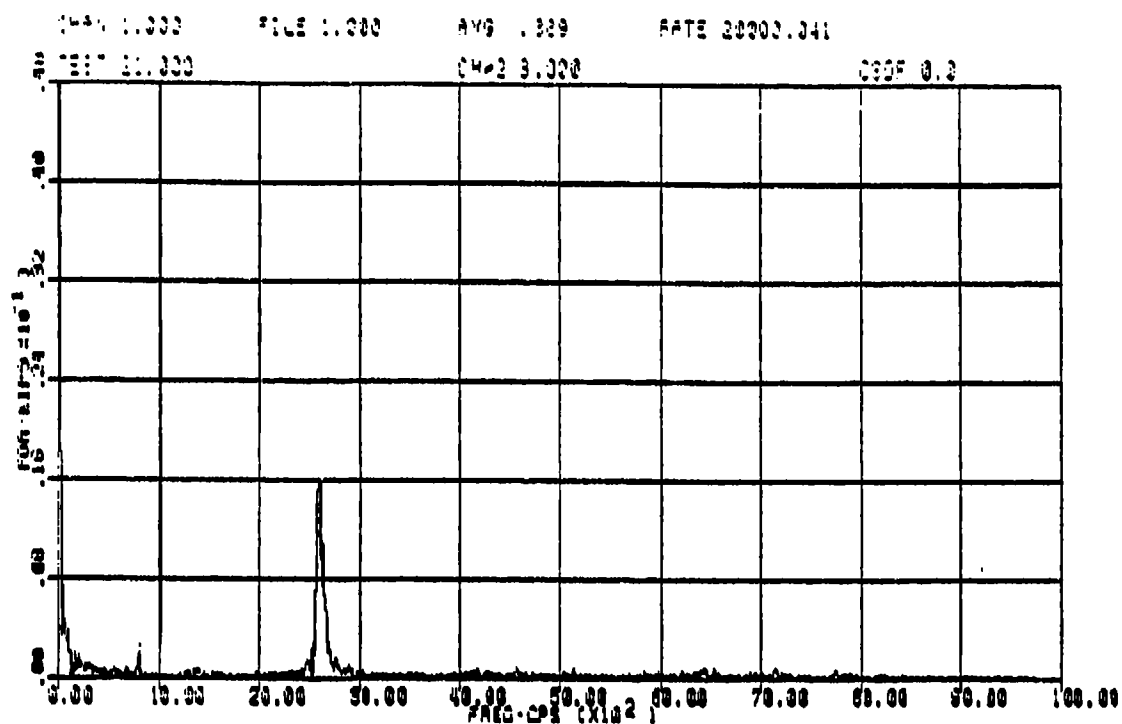


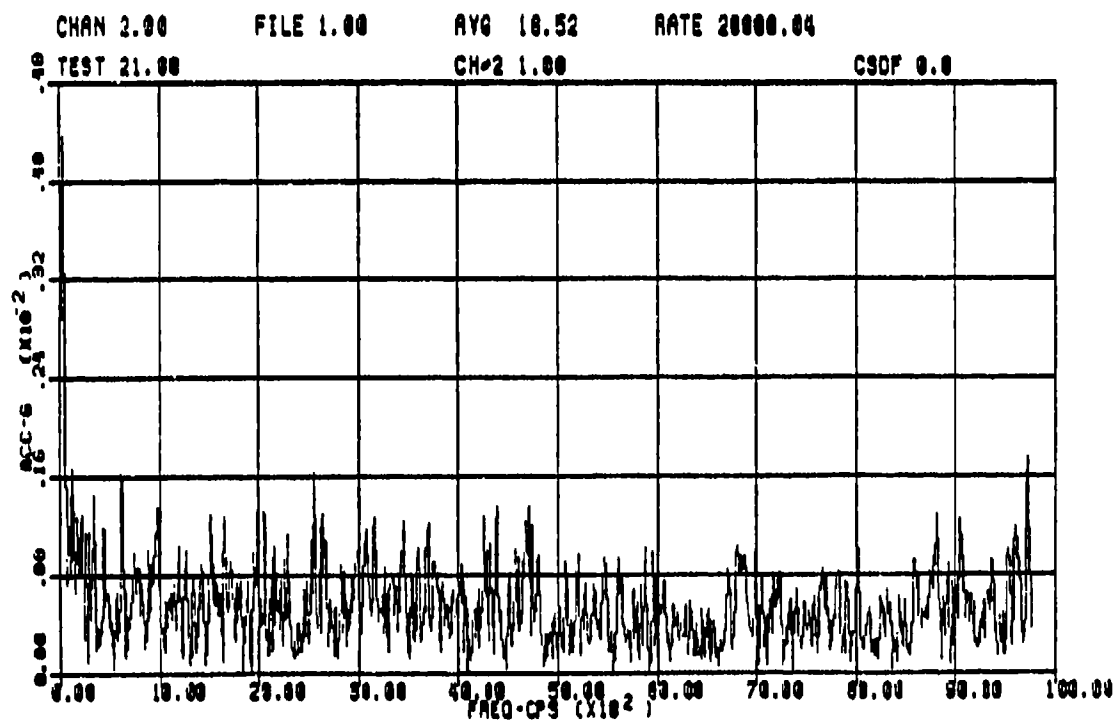
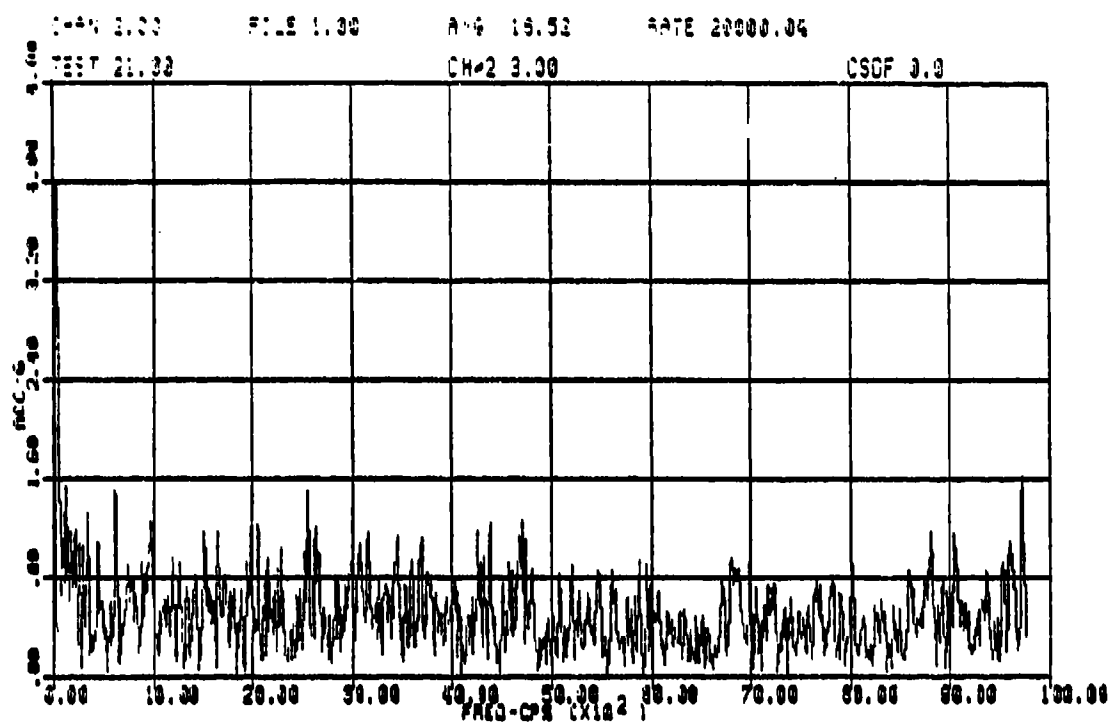
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #8%
AIR BAG PRESSURE = 50 PSI

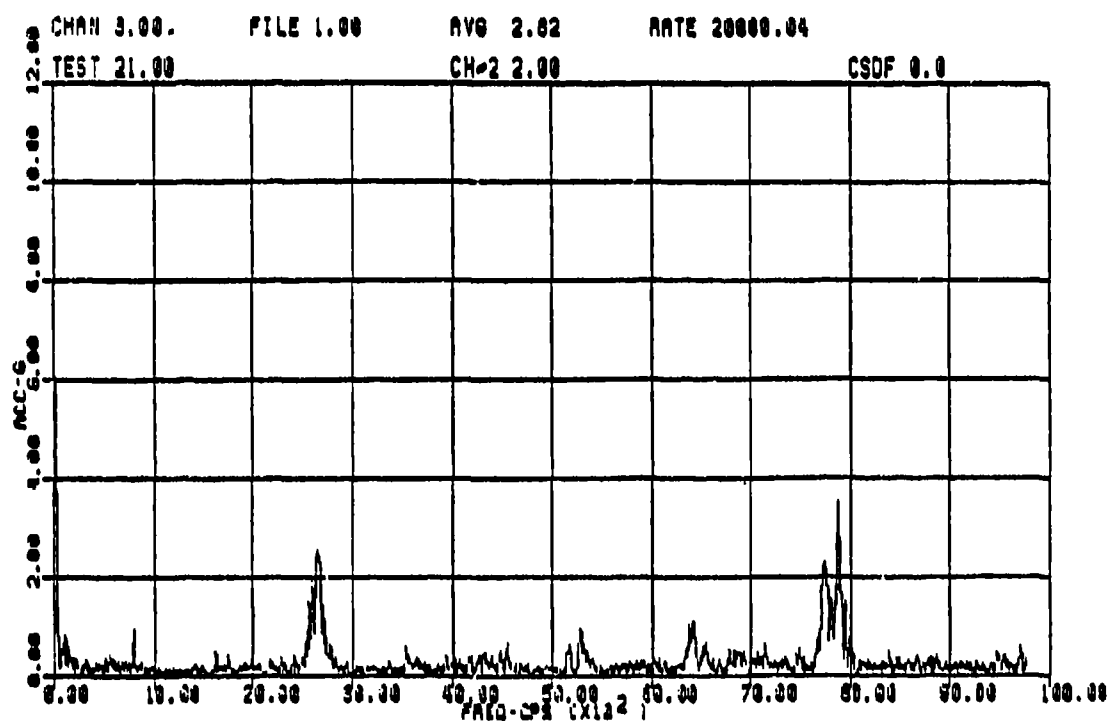
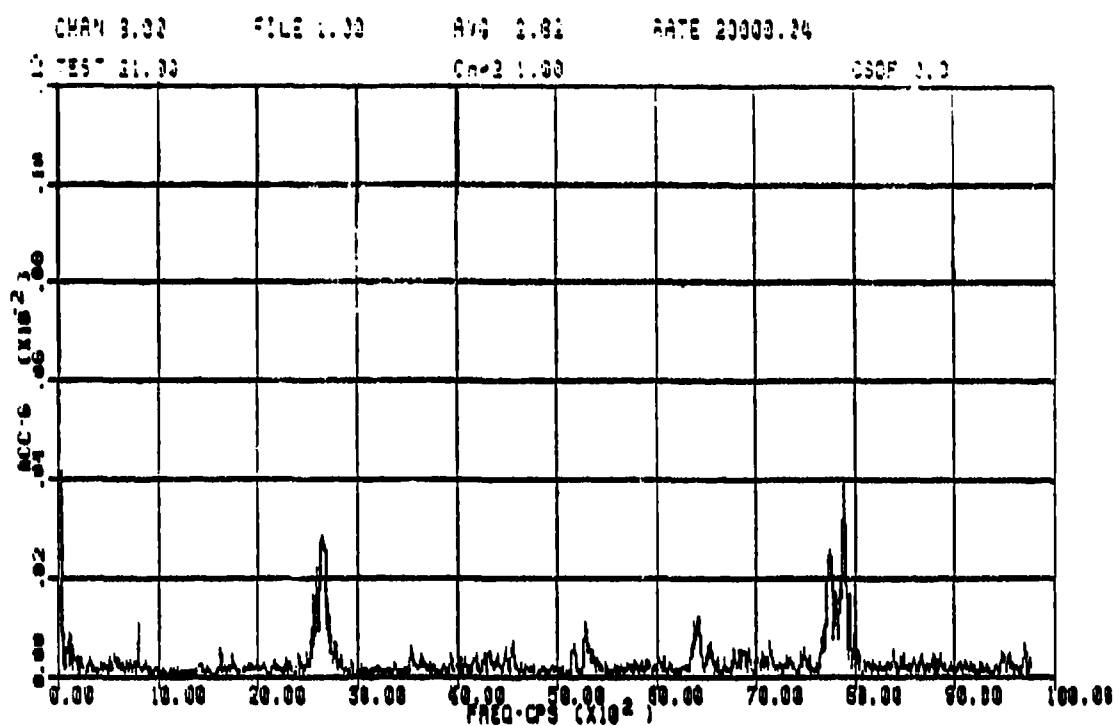


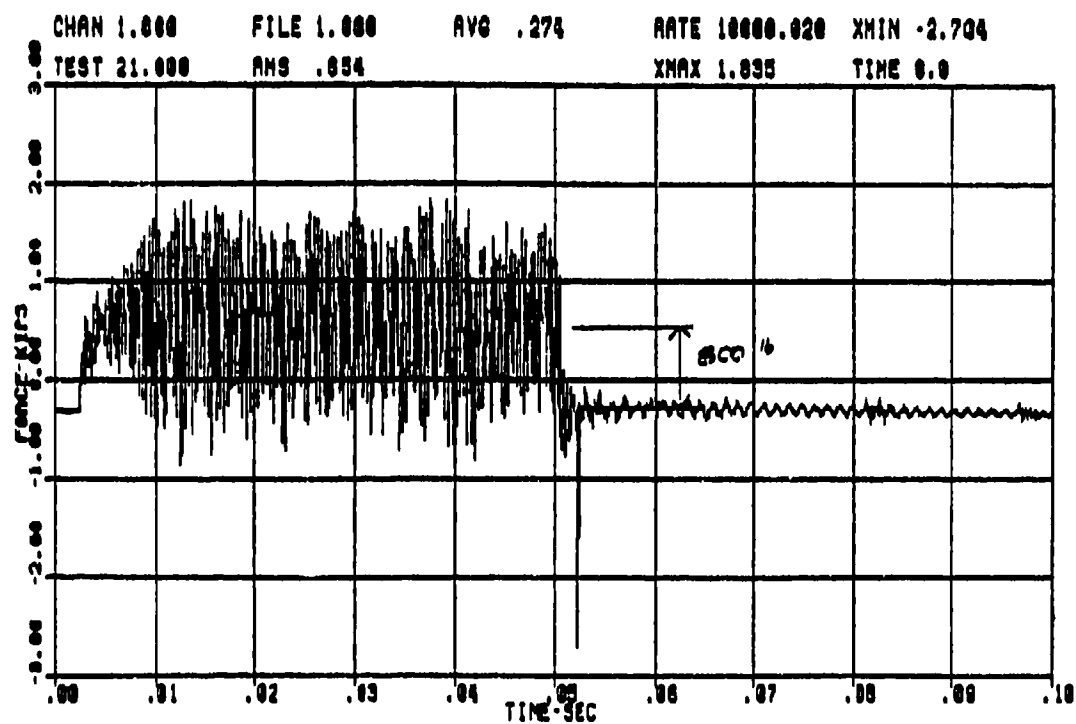
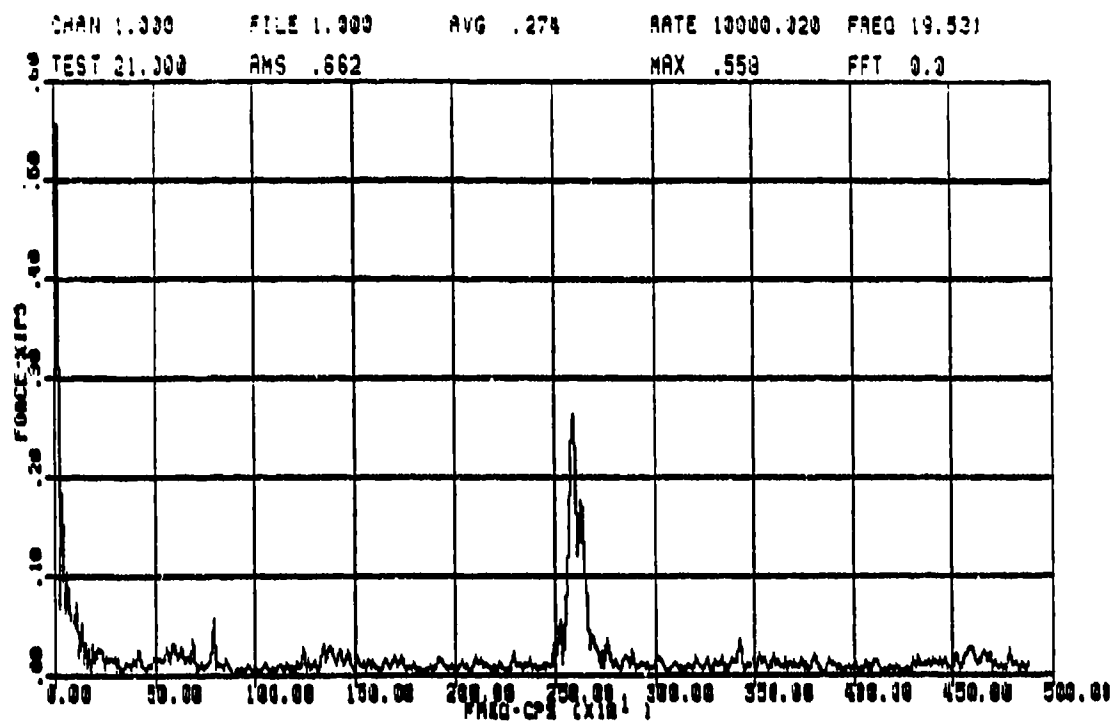


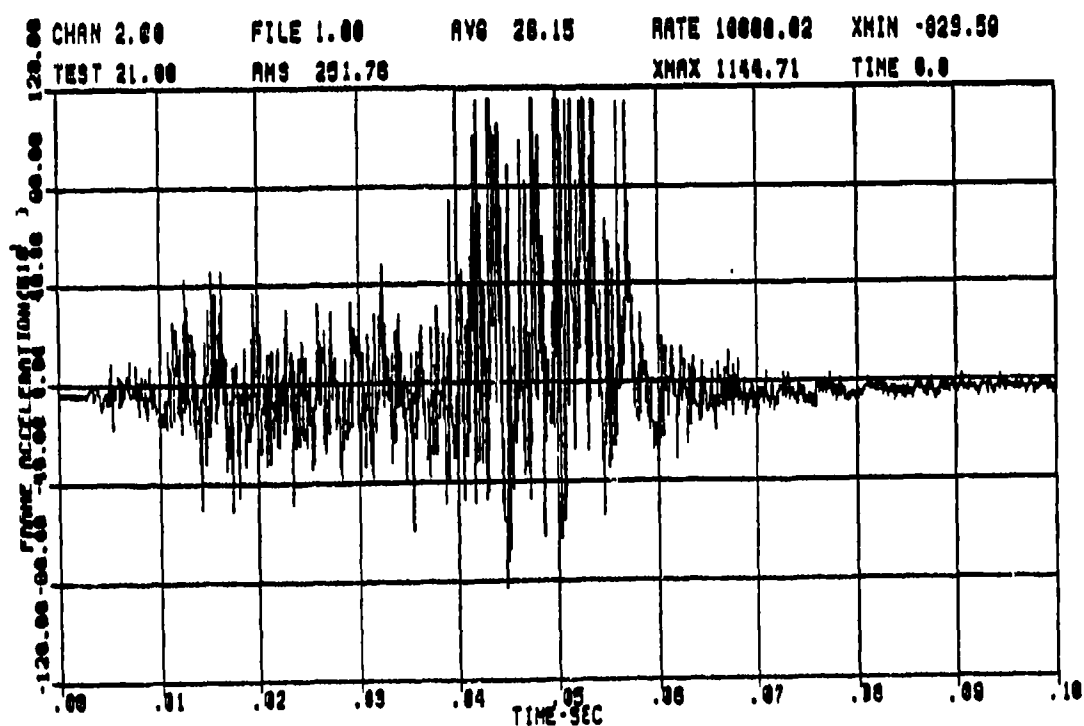
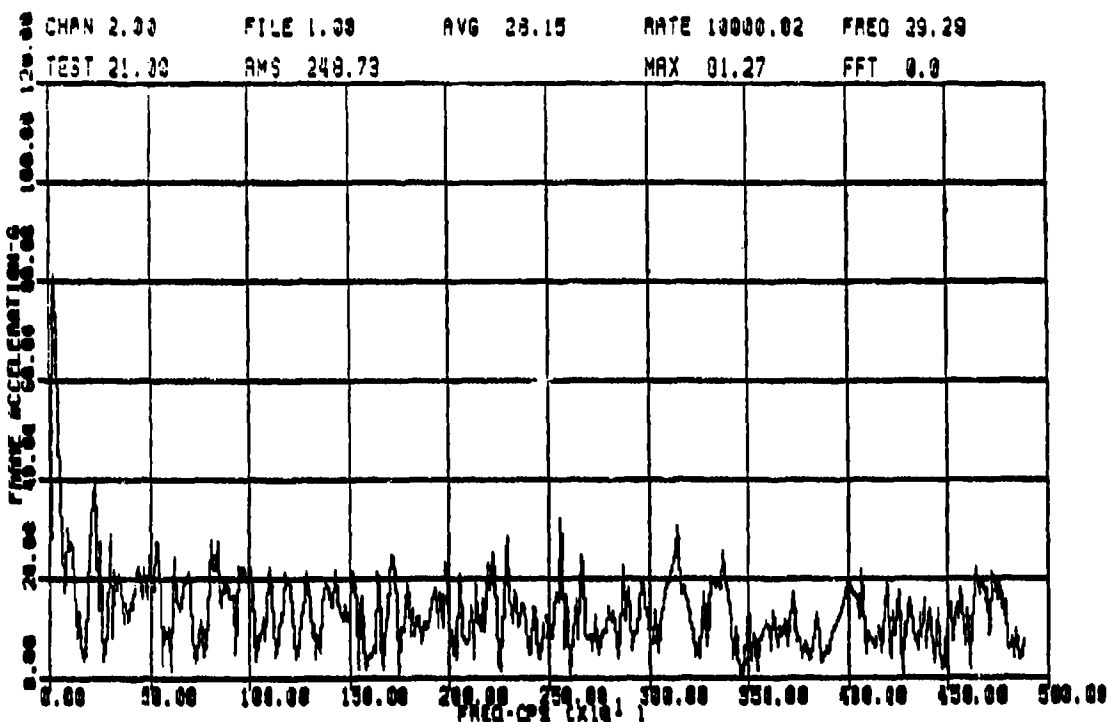


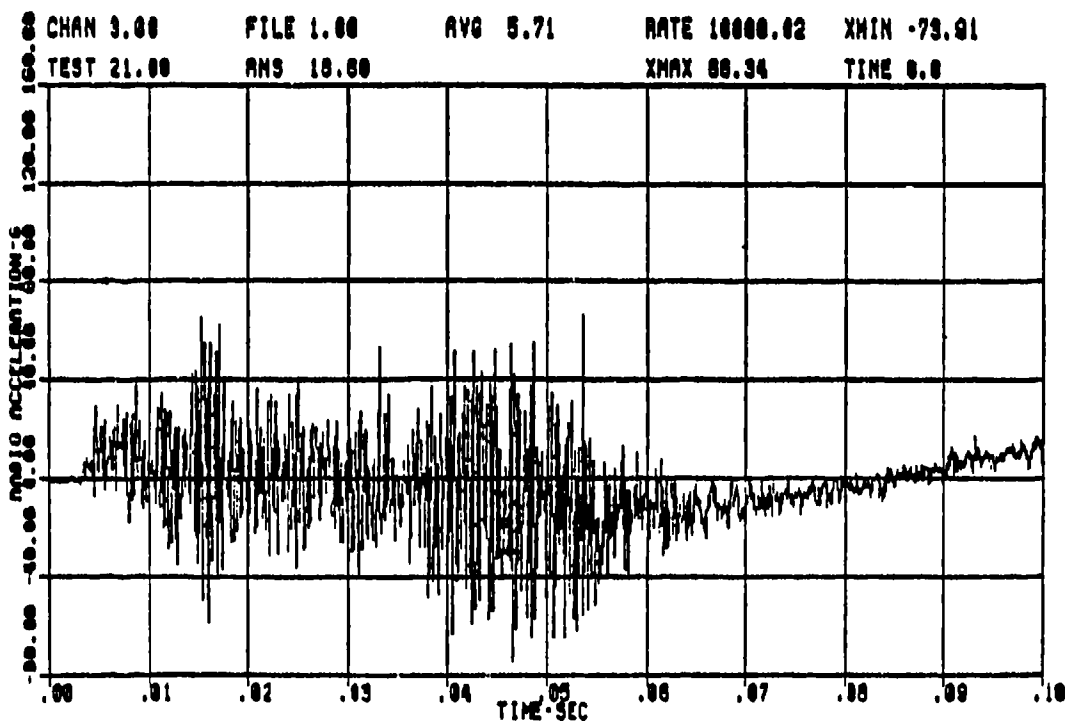
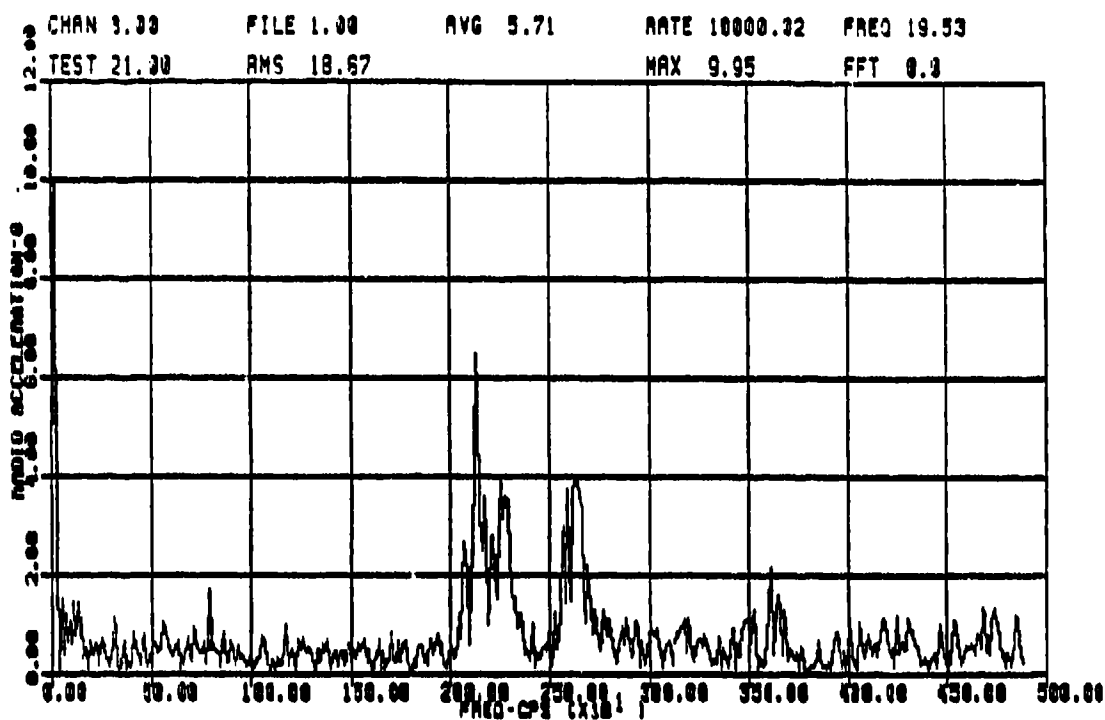


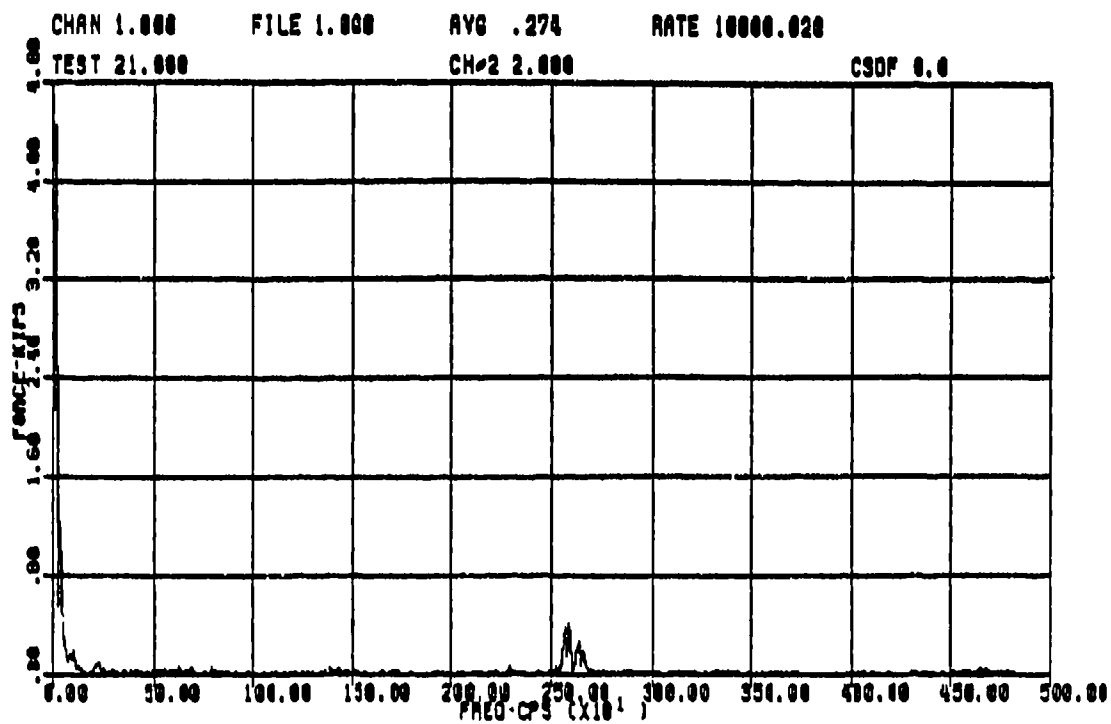
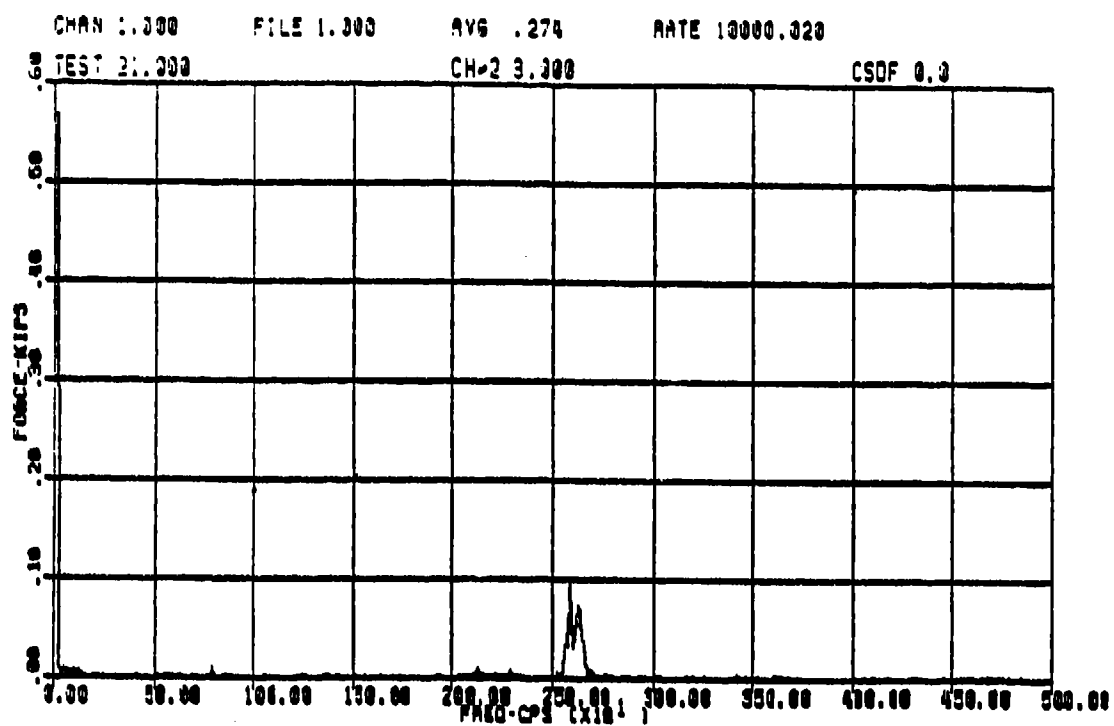


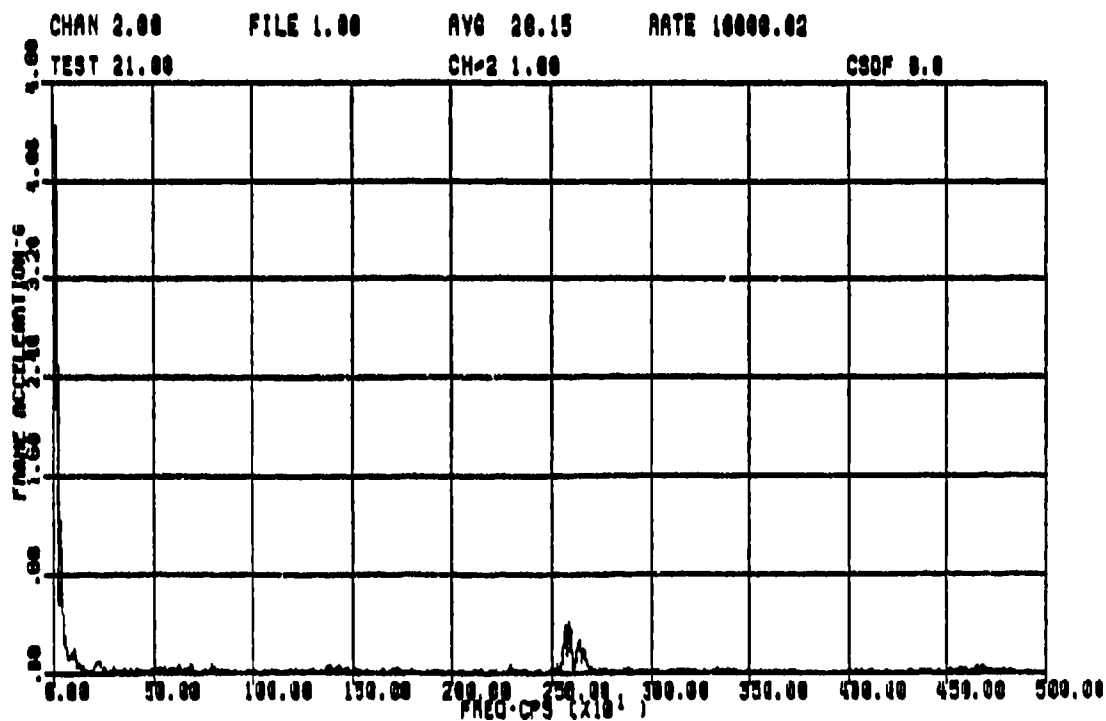
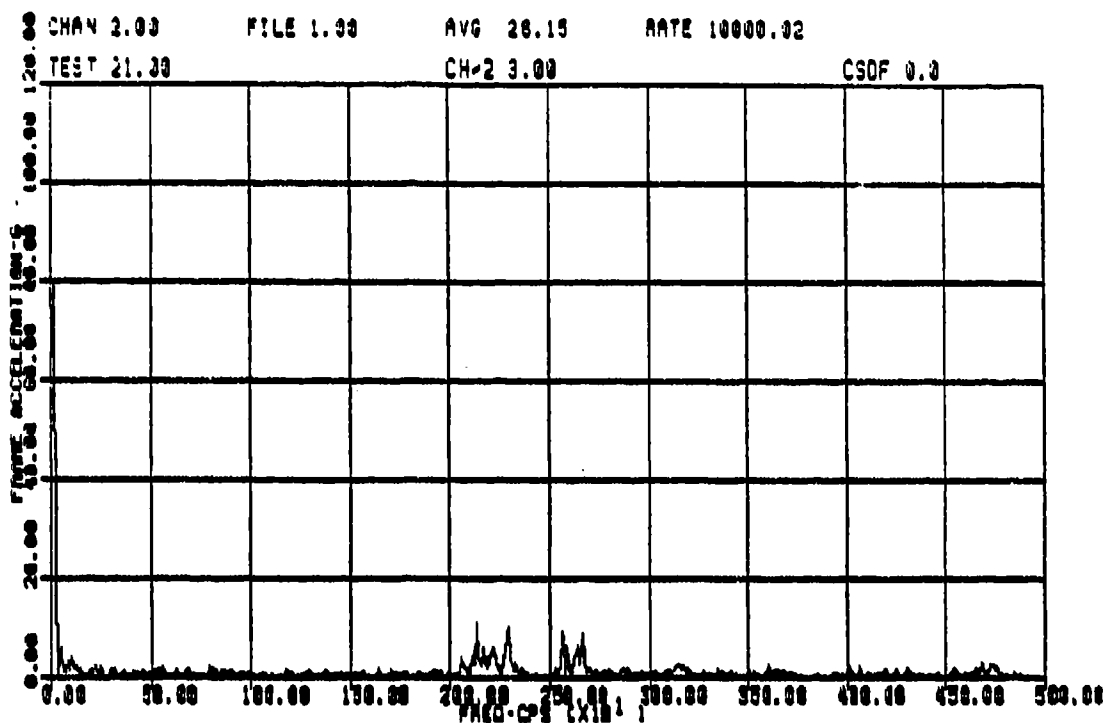


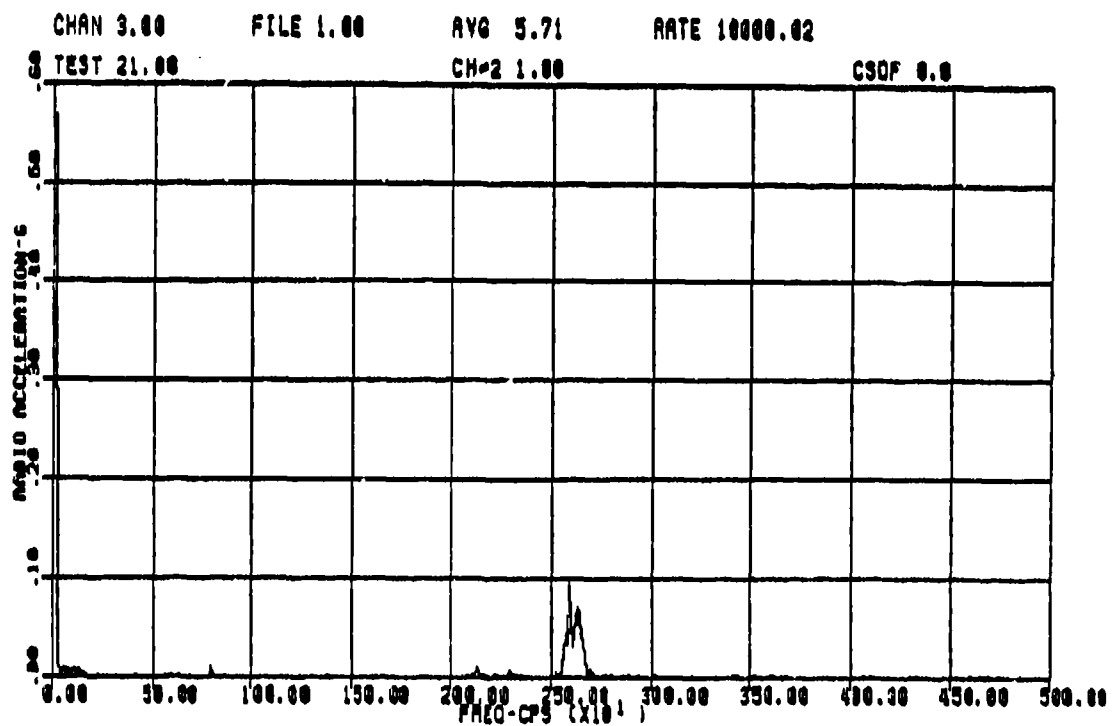
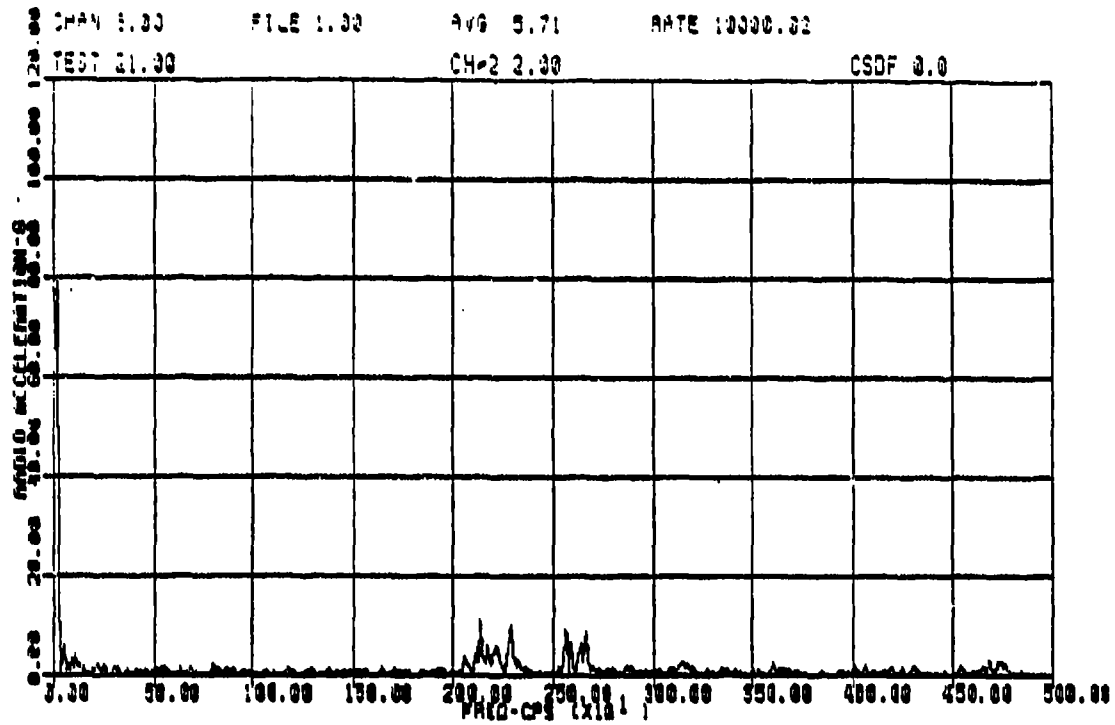




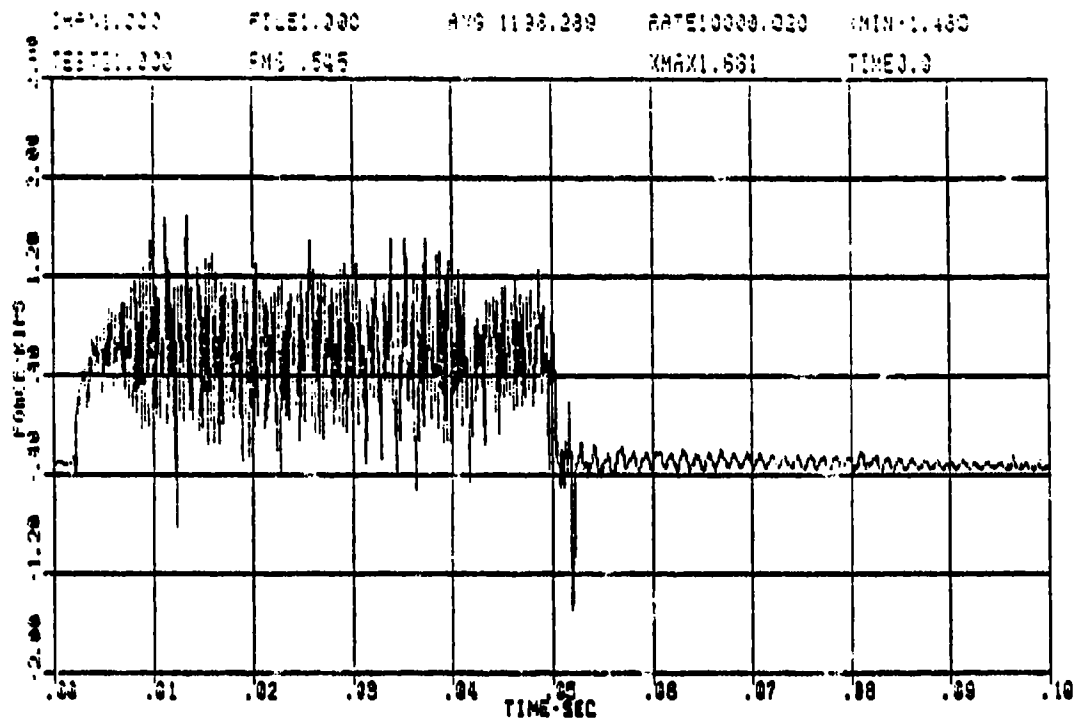




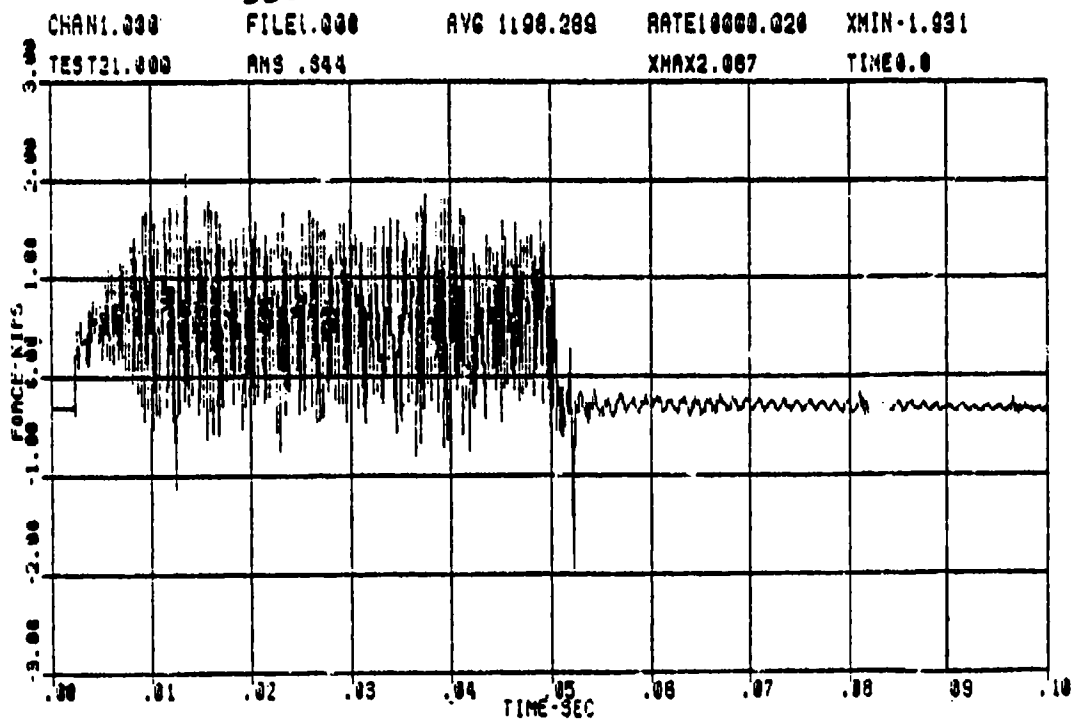




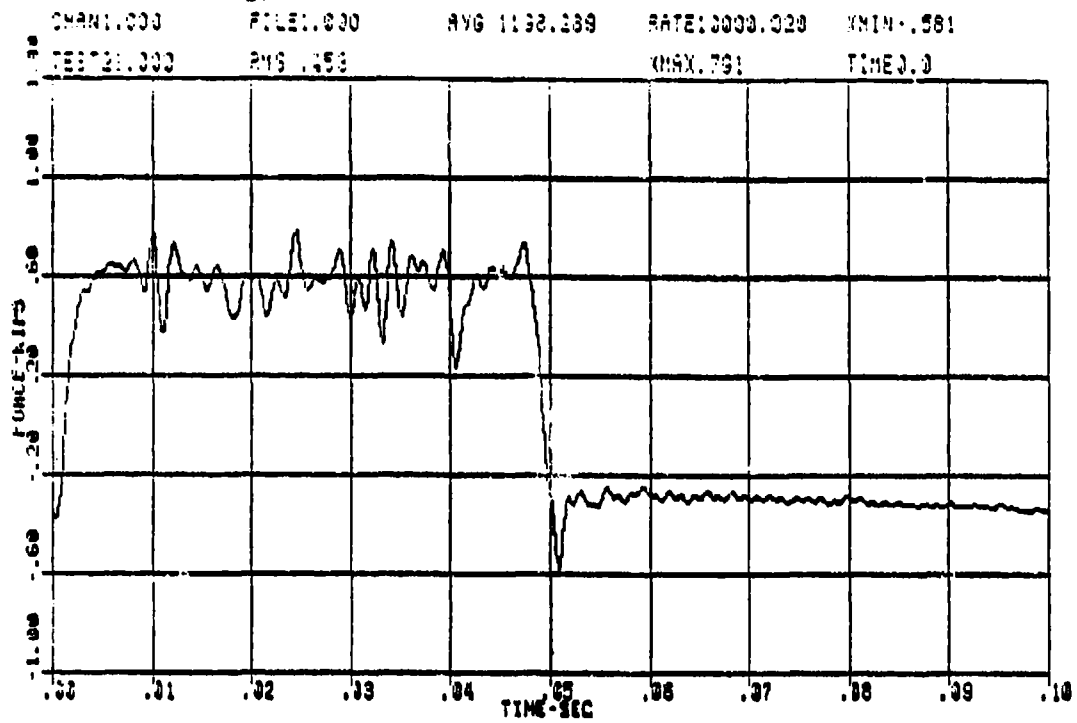
2500 Hz Low Pass Filter



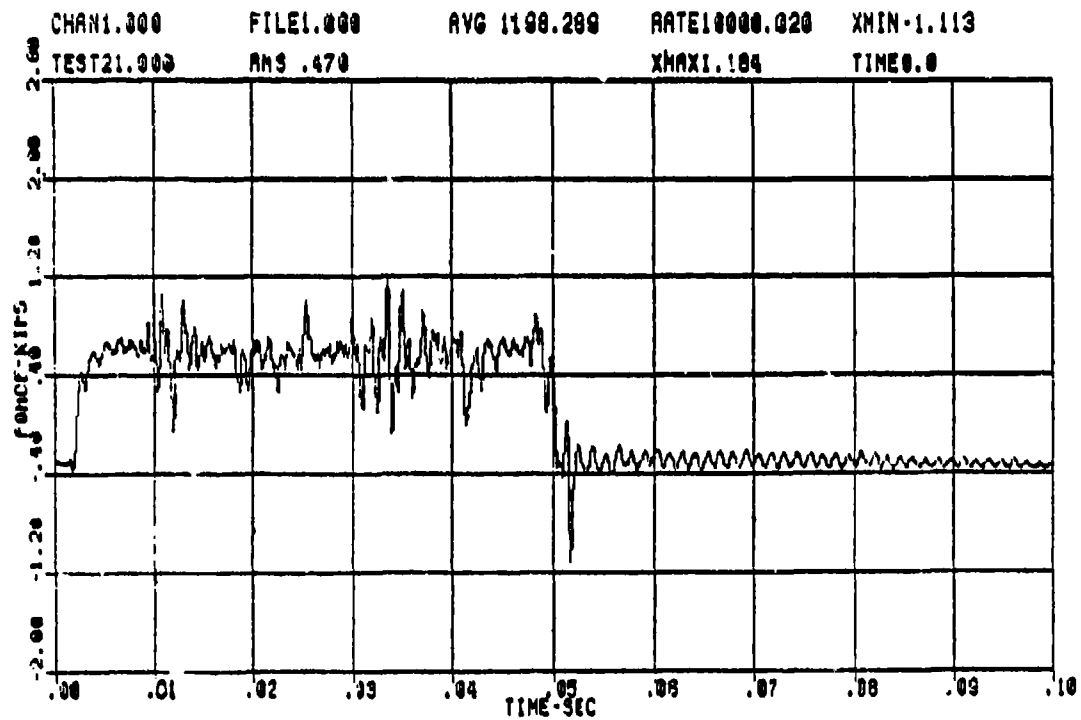
3500 Hz Low Pass Filter

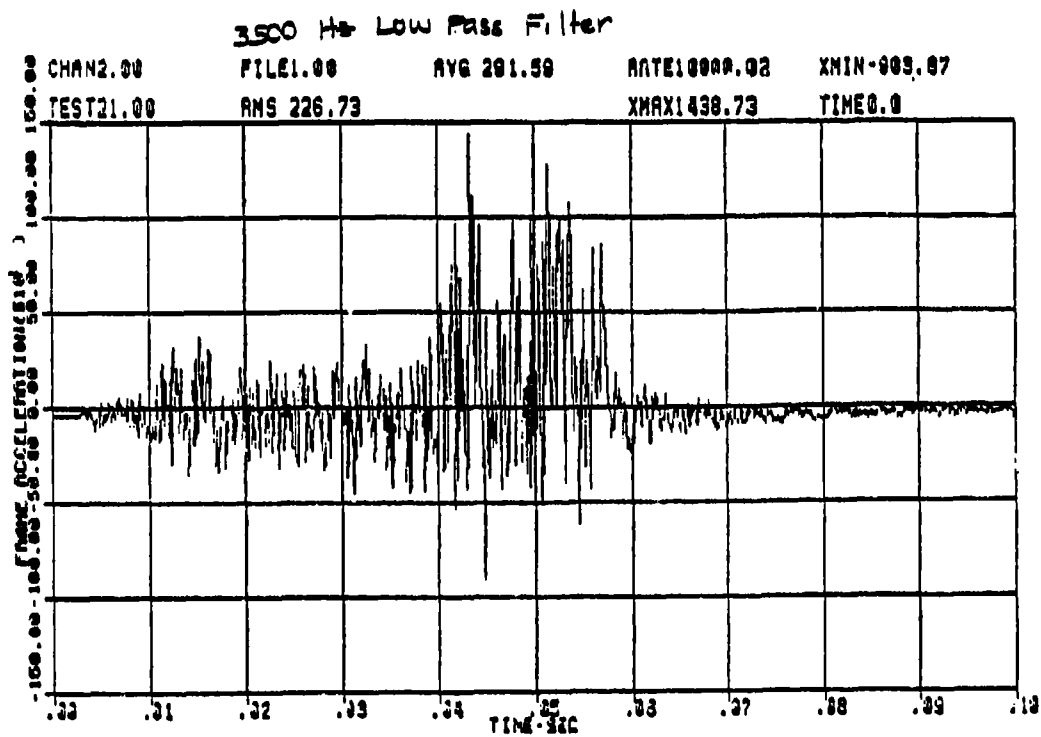
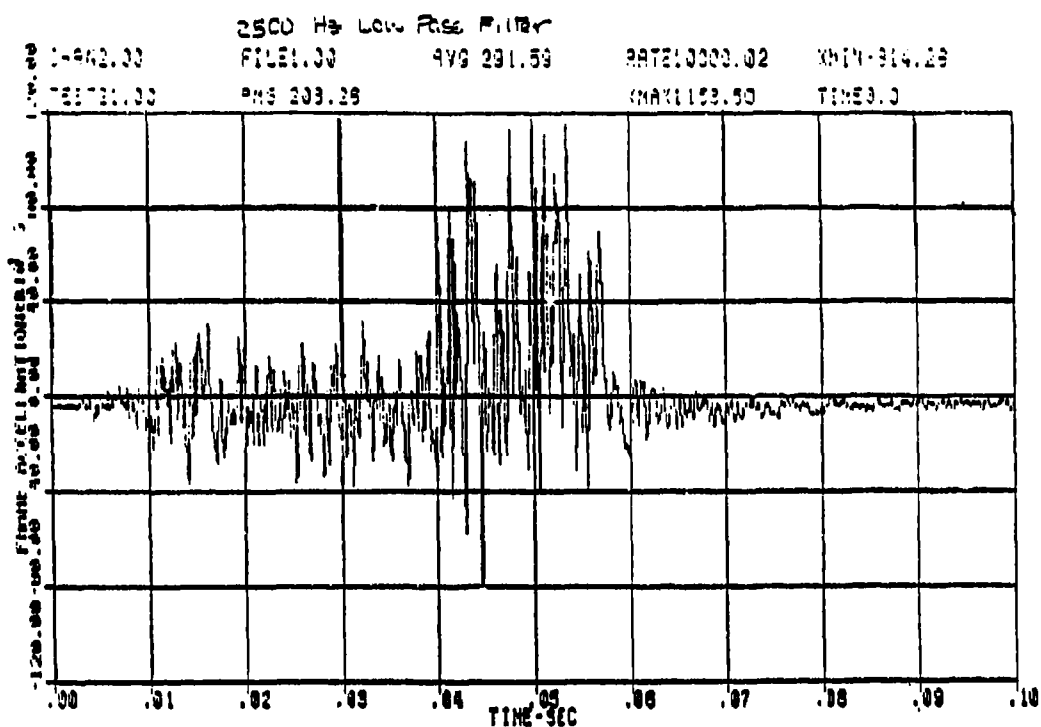


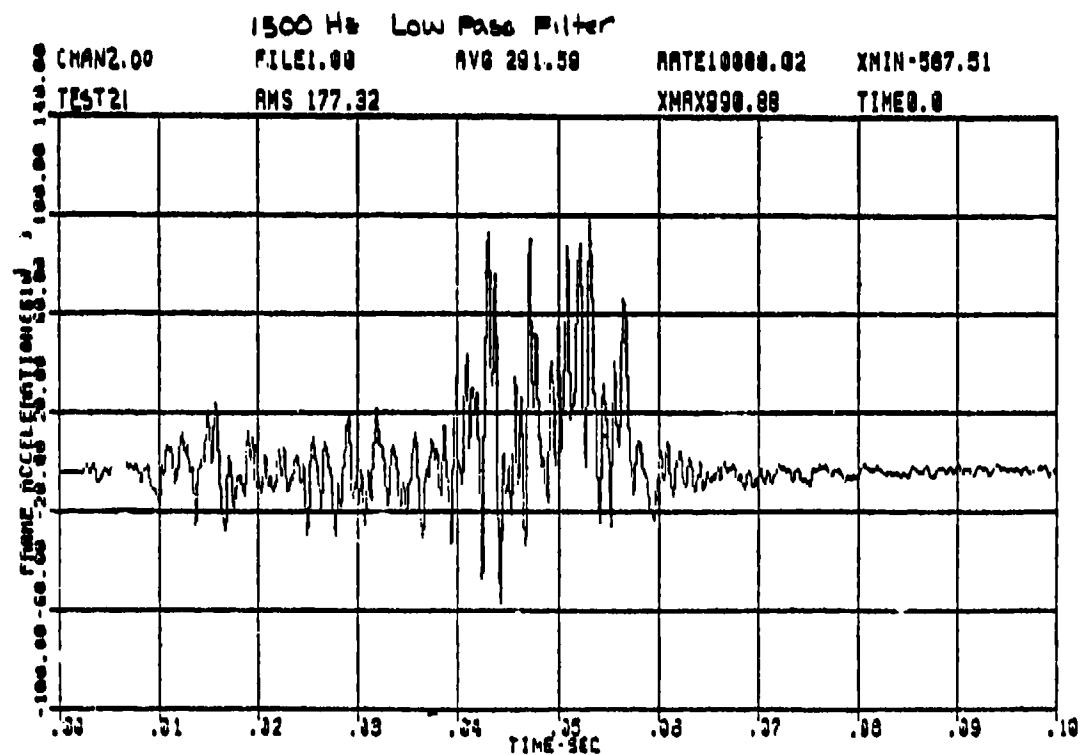
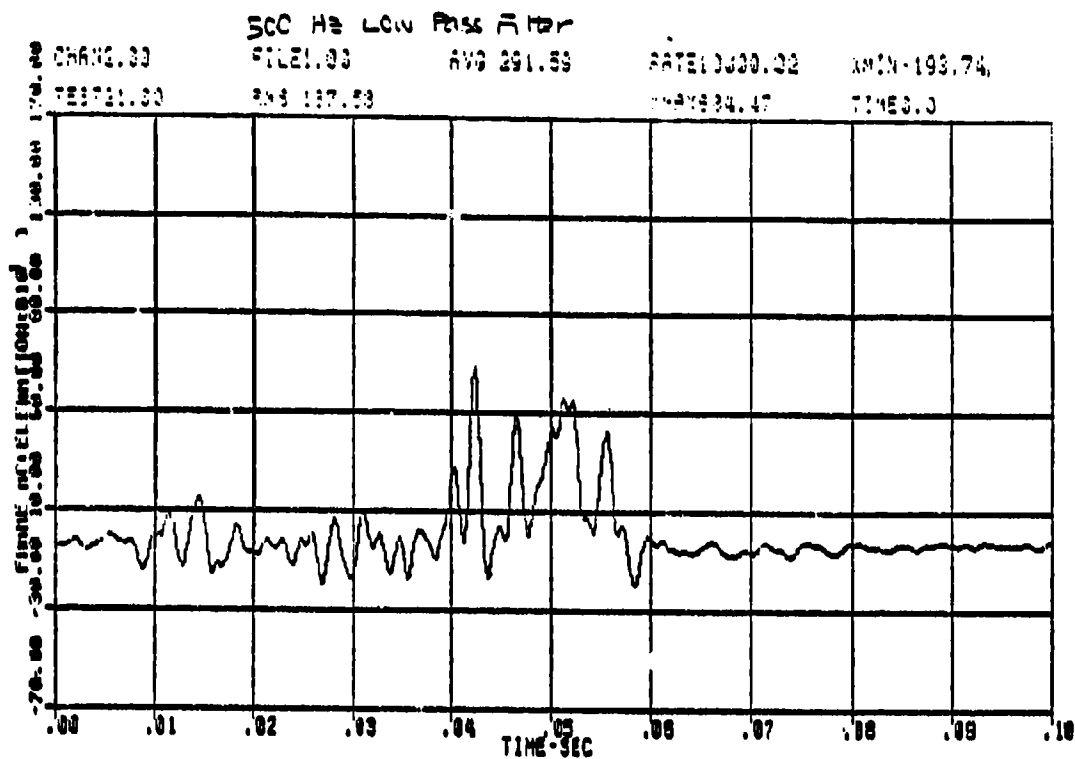
500 Hz Low Pass Filter

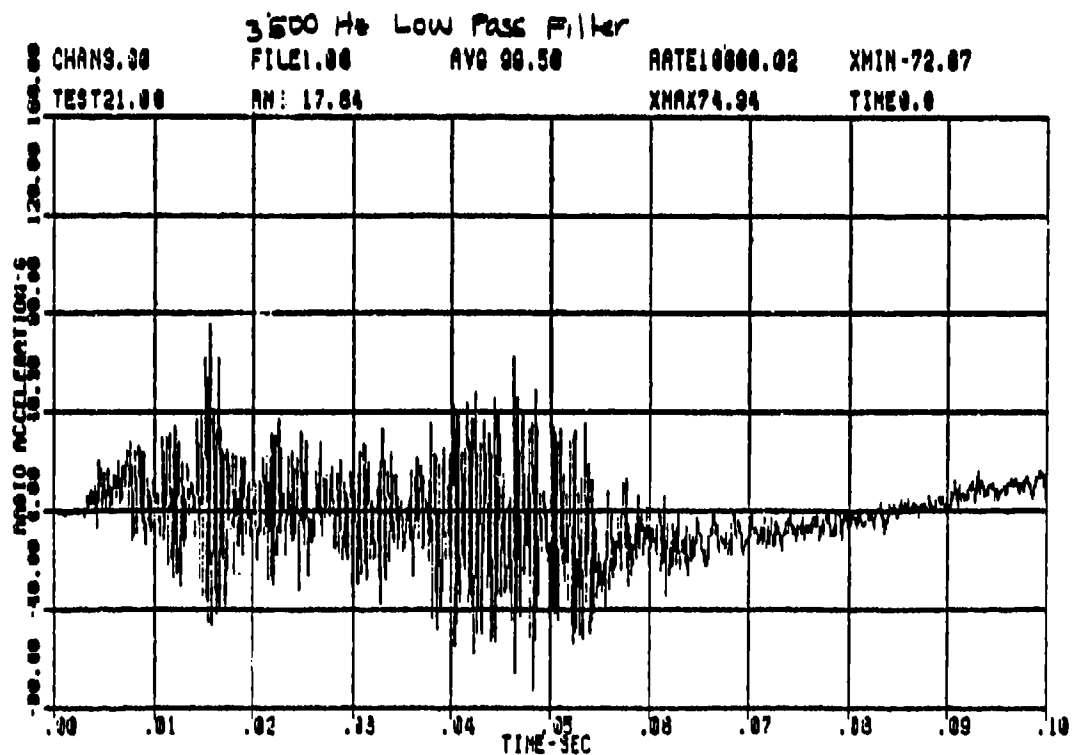
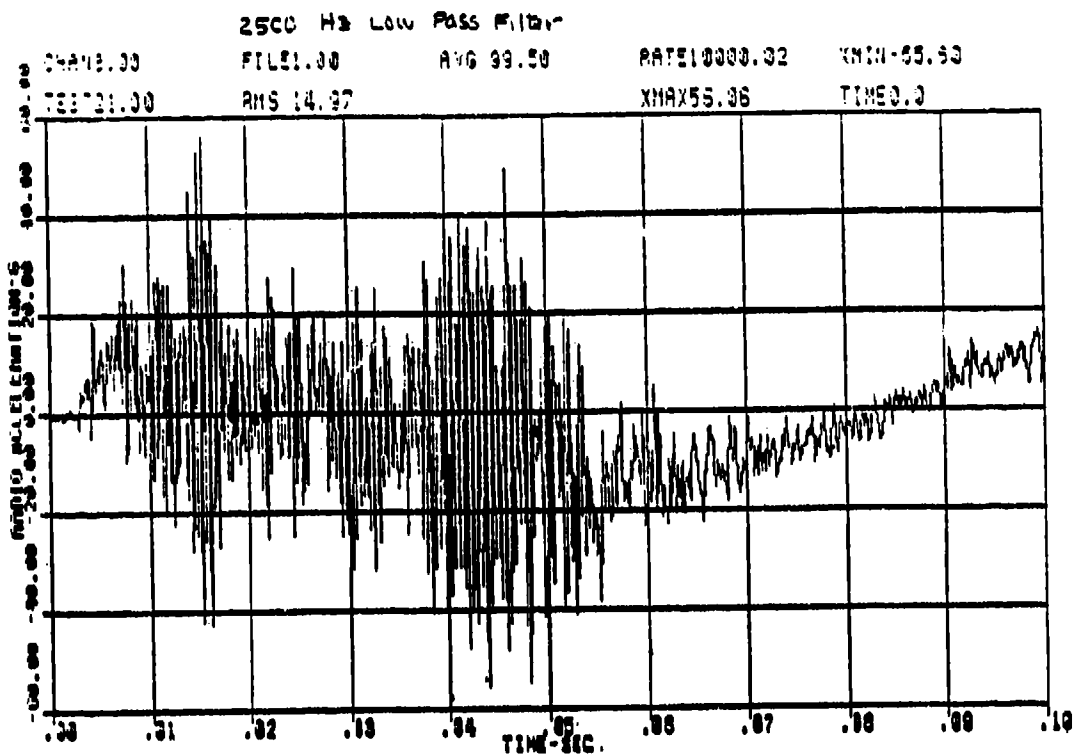


1500 Hz Low Pass Filter

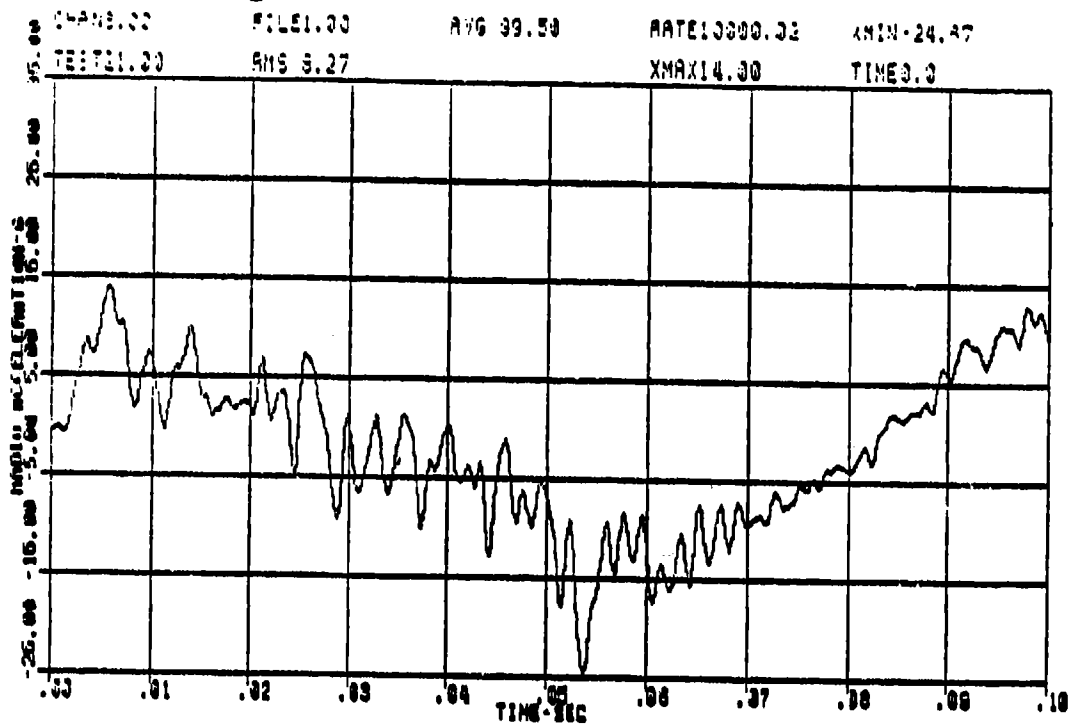




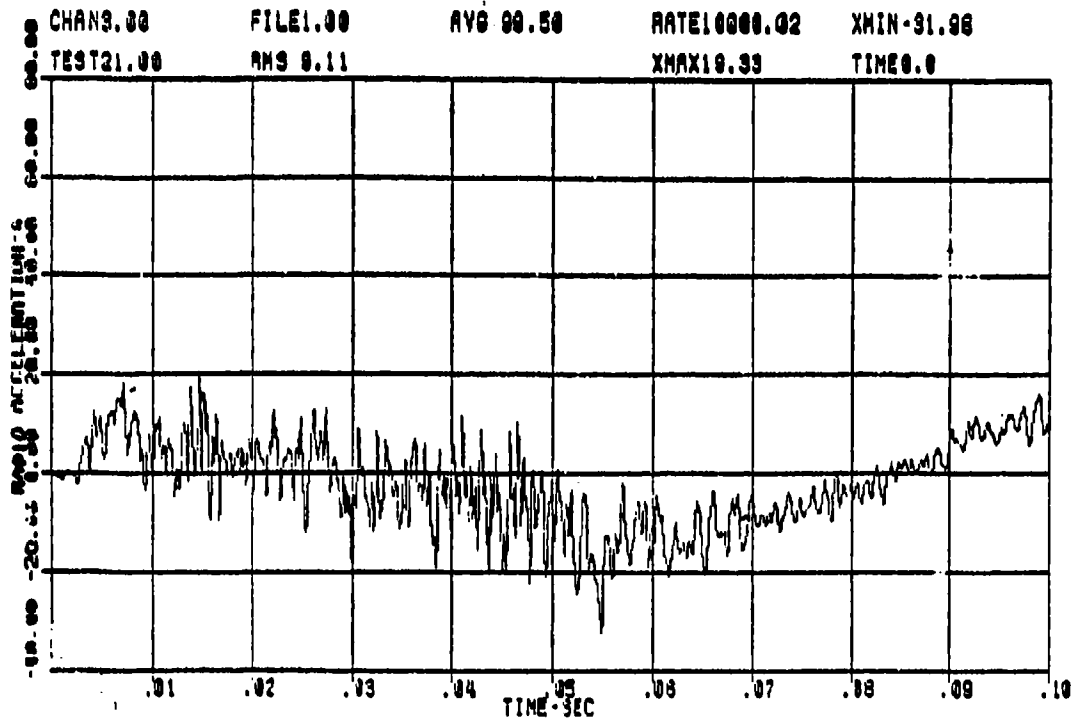




500 Hz Low Pass Filter

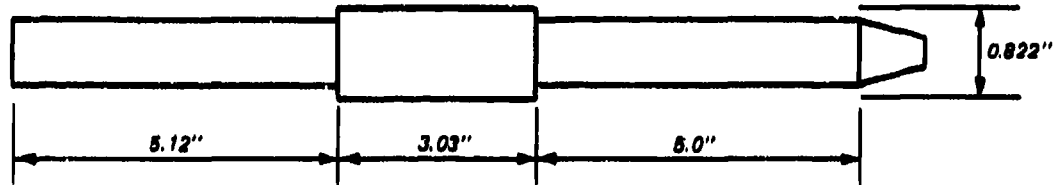


1500 Hz Low Pass Filter



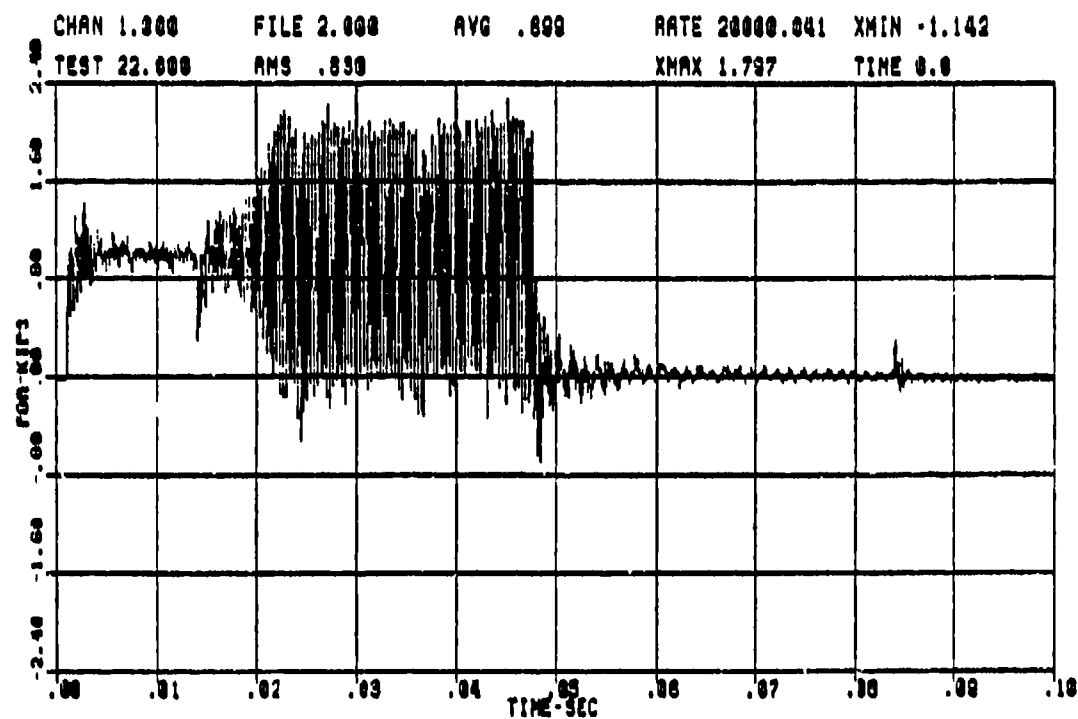
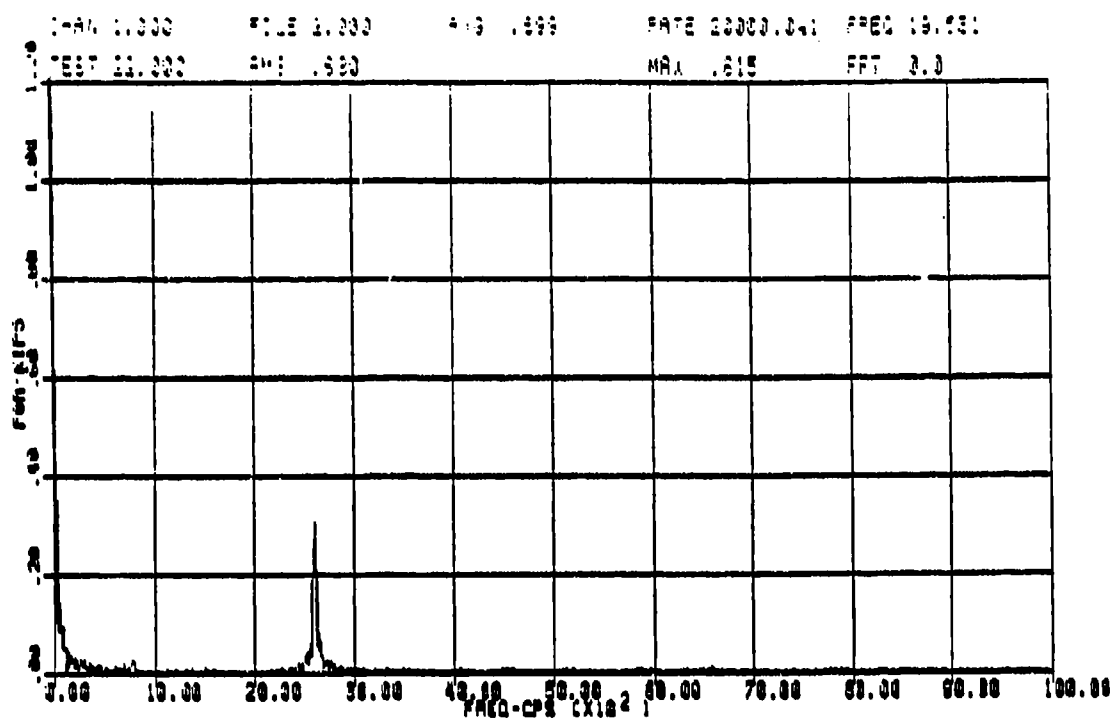
APPENDIX H: TEST 22 RESULTS

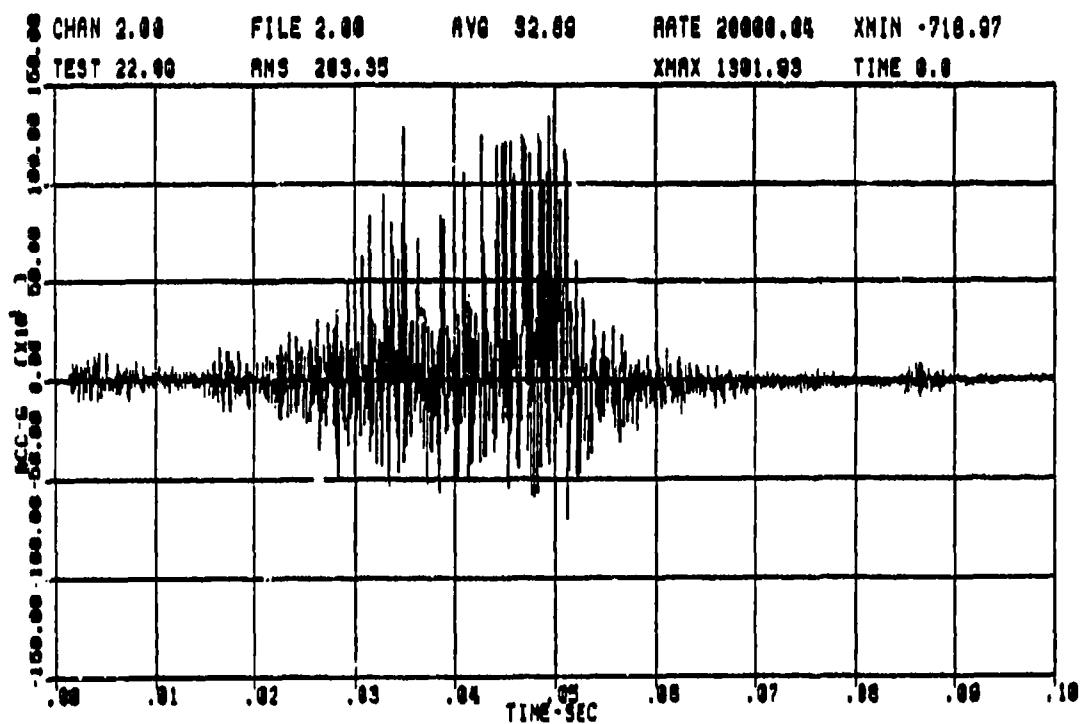
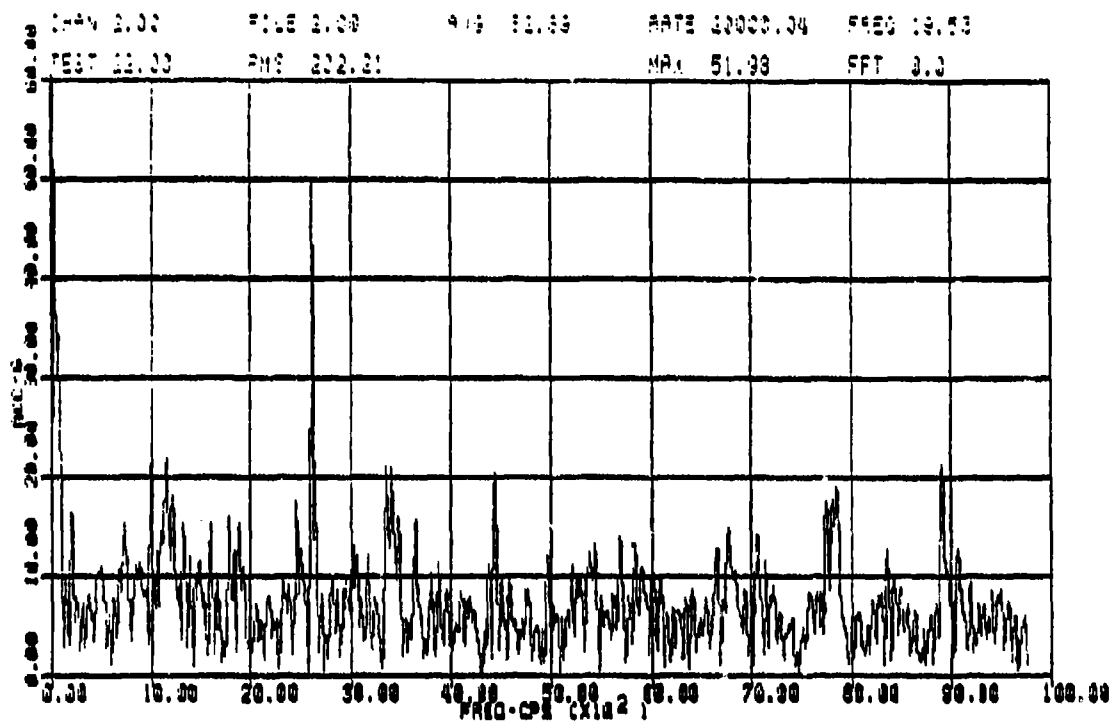
Test 22
Equipment Rack Soft-Mounted
AN/GRC-103 in Rack, Off-Line



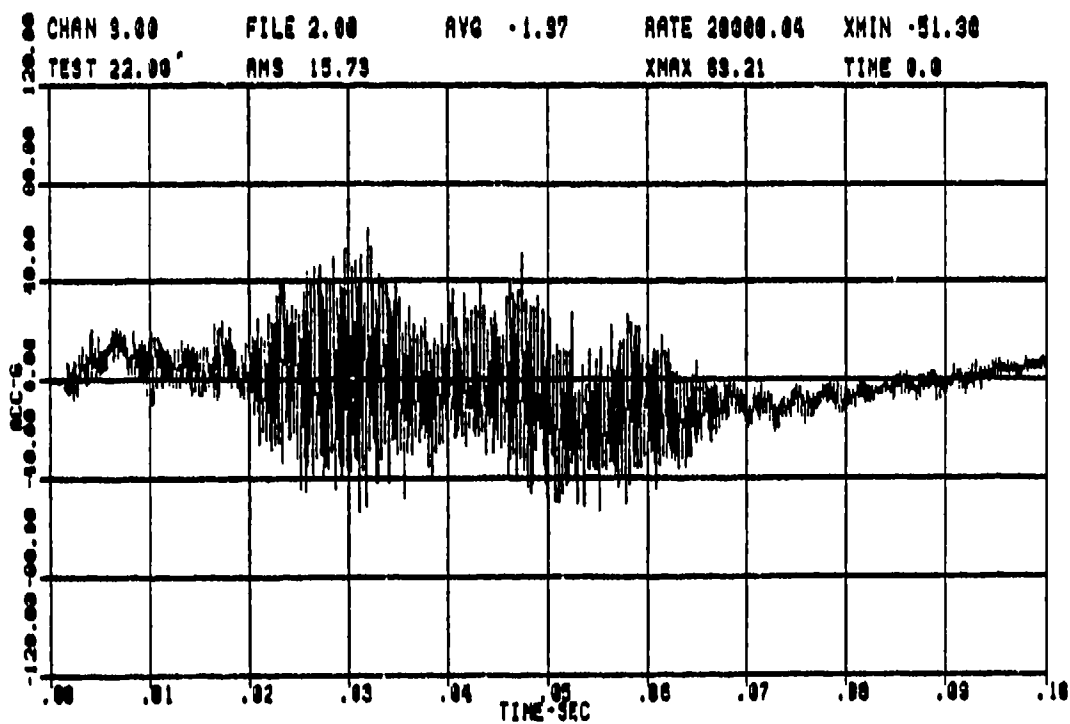
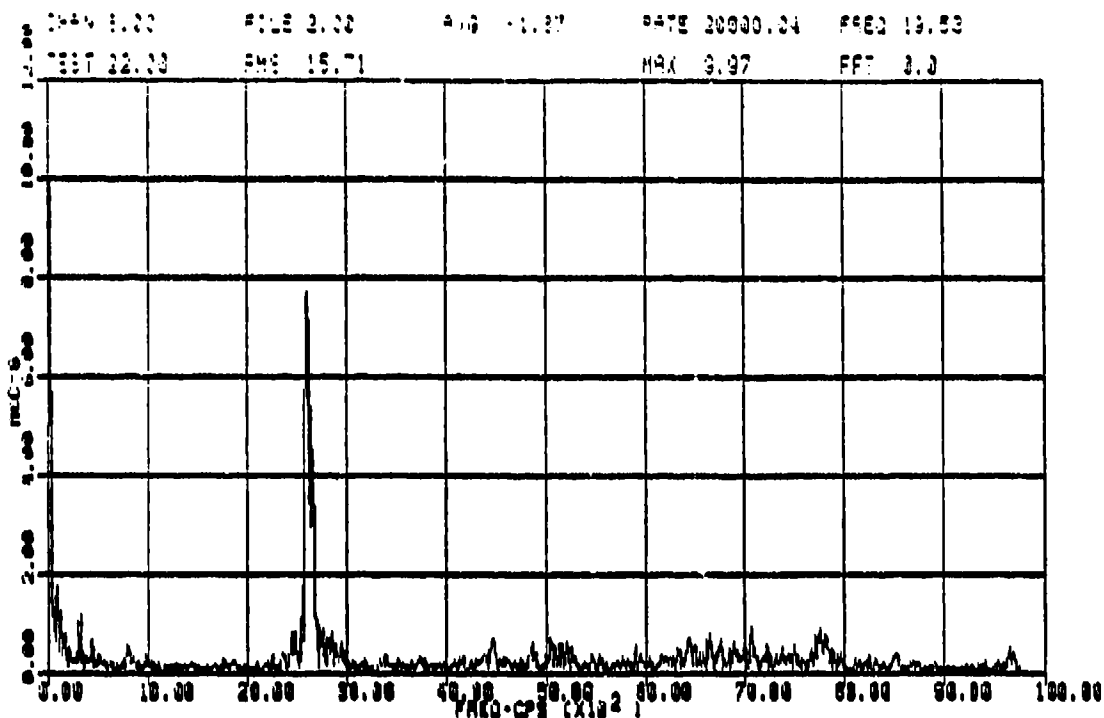
PULSE TRAIN - TEST 22

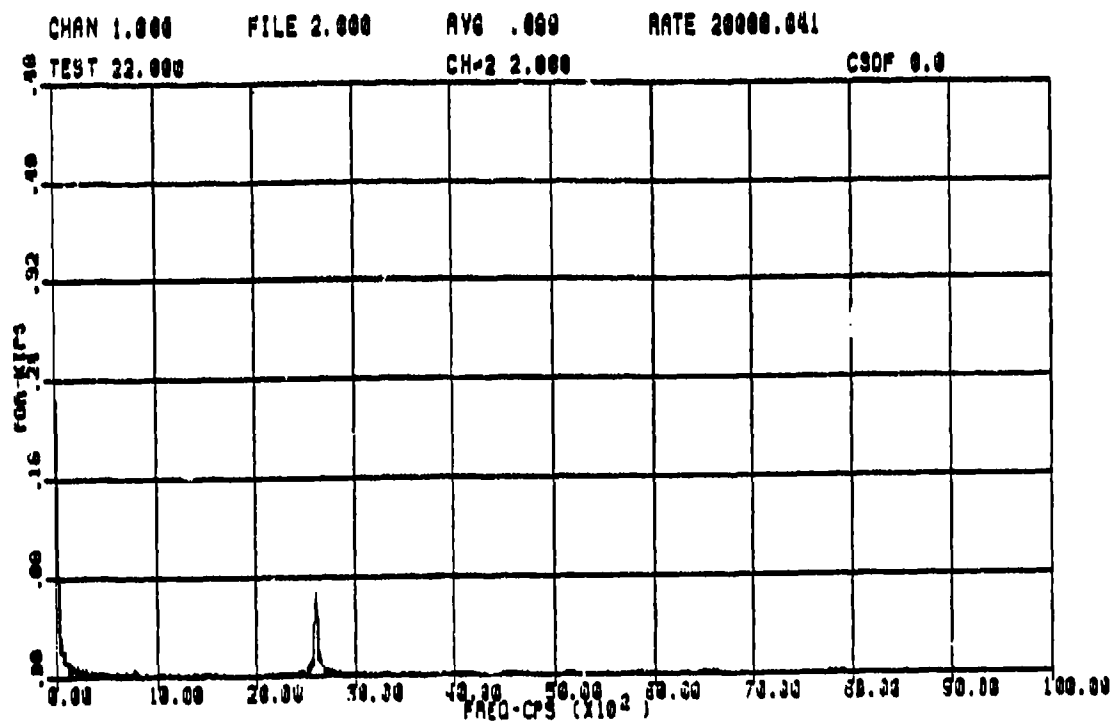
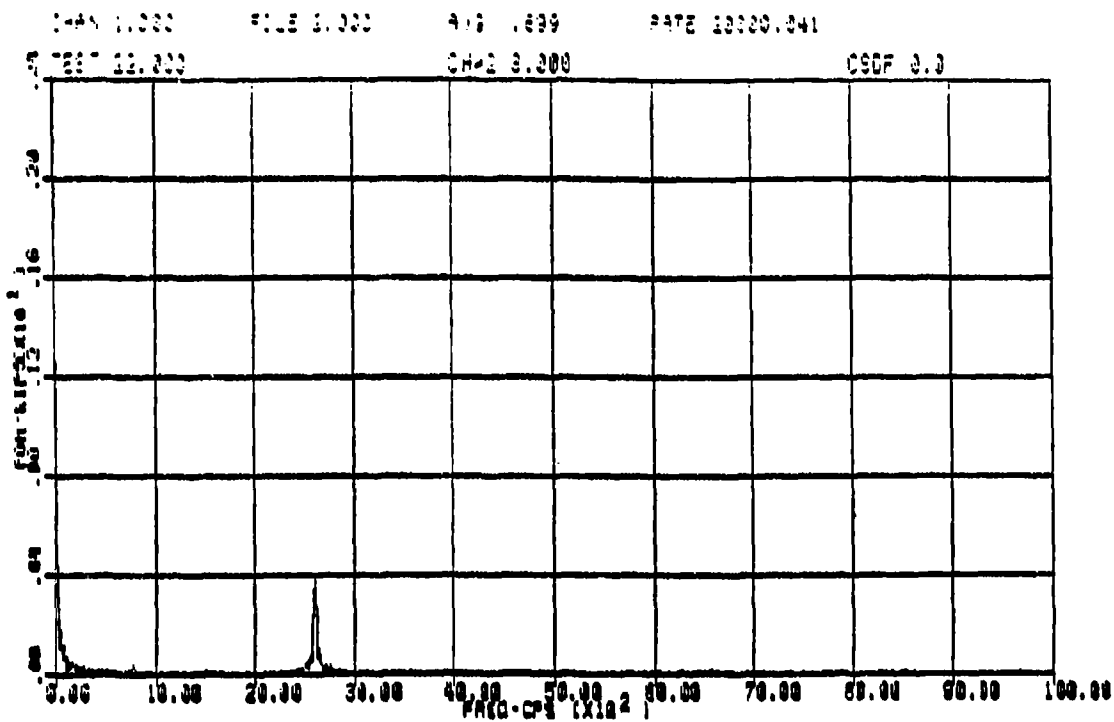
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #6½
AIR BAG PRESSURE = 30 PSI

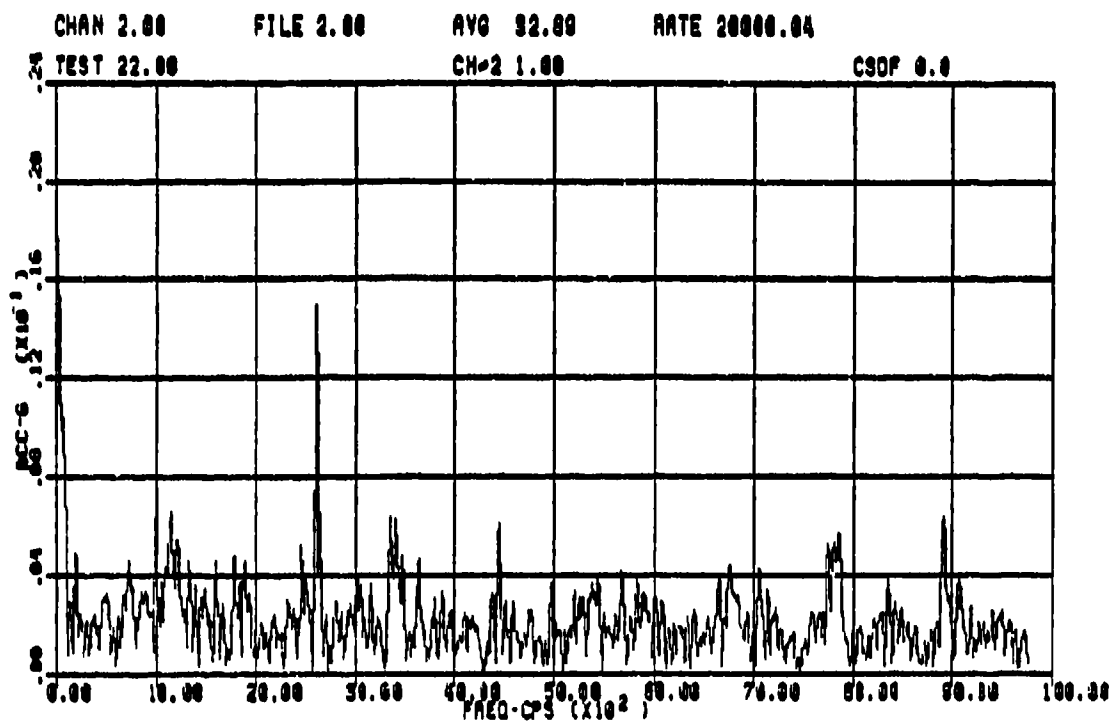
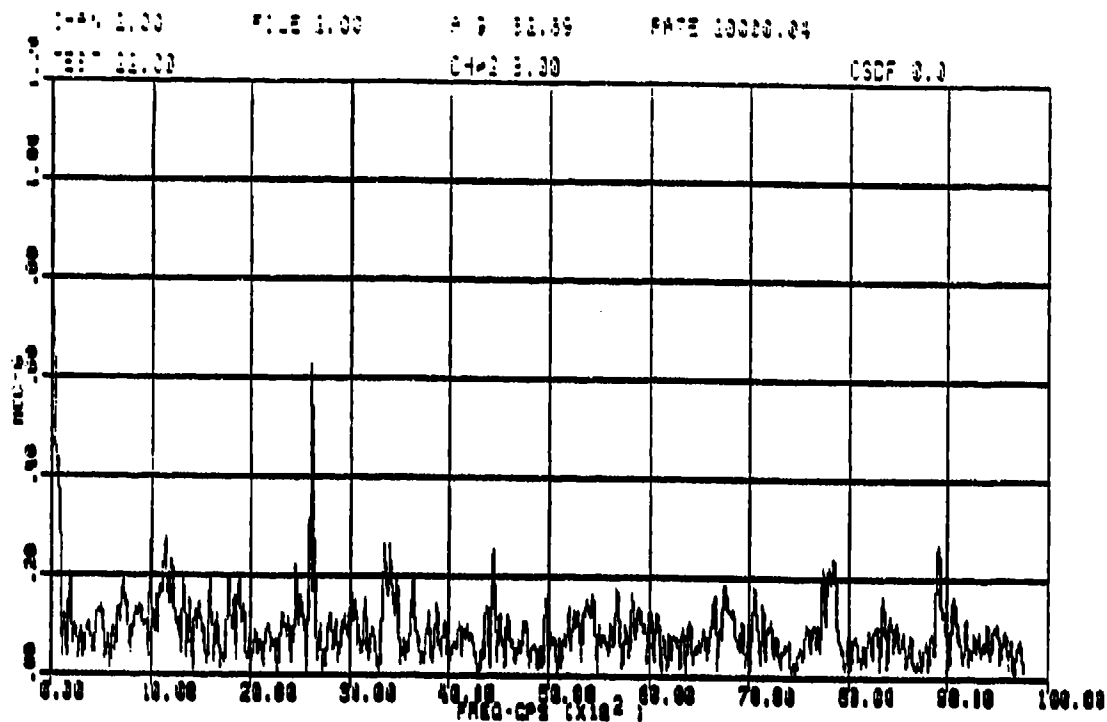


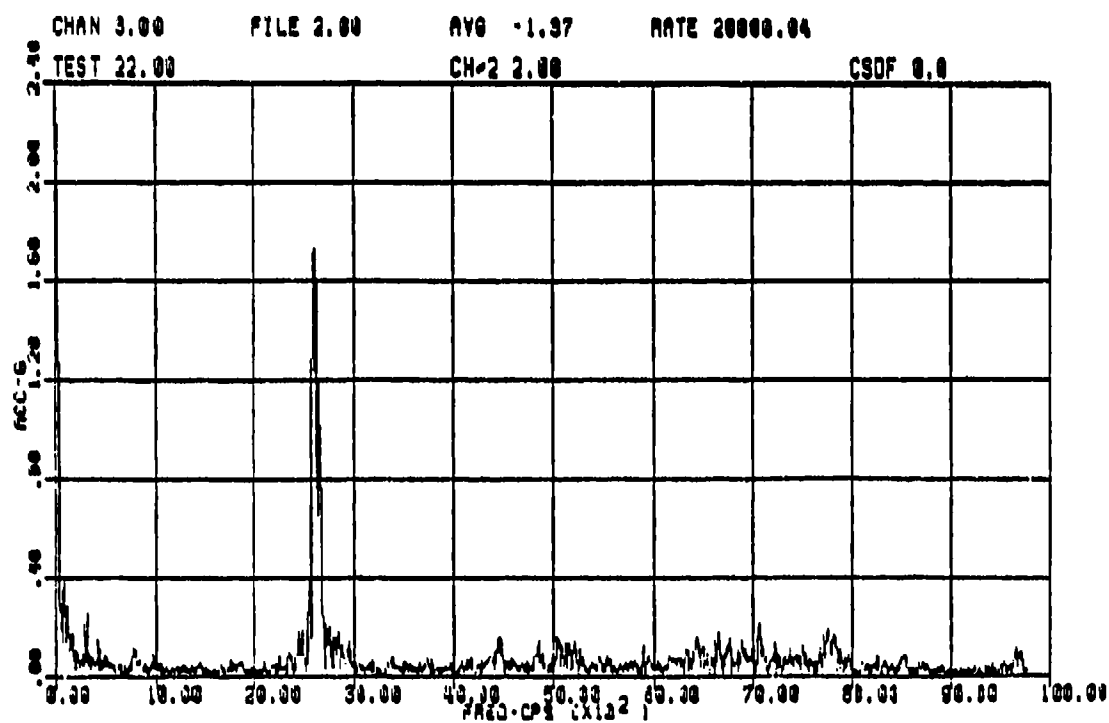
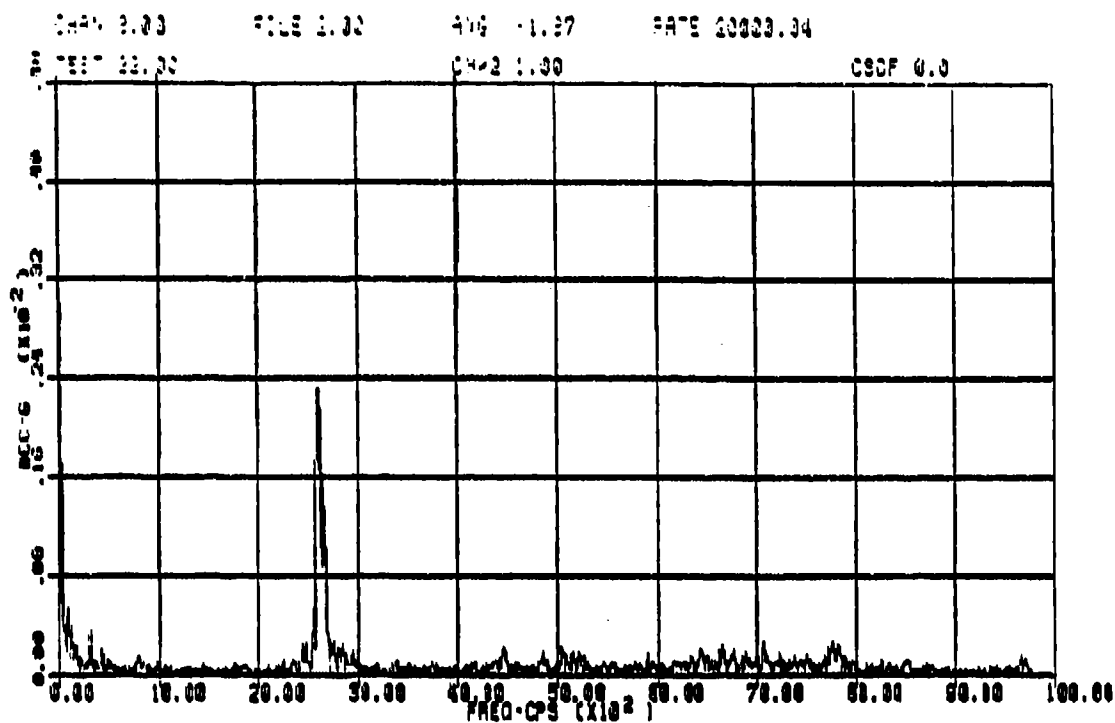


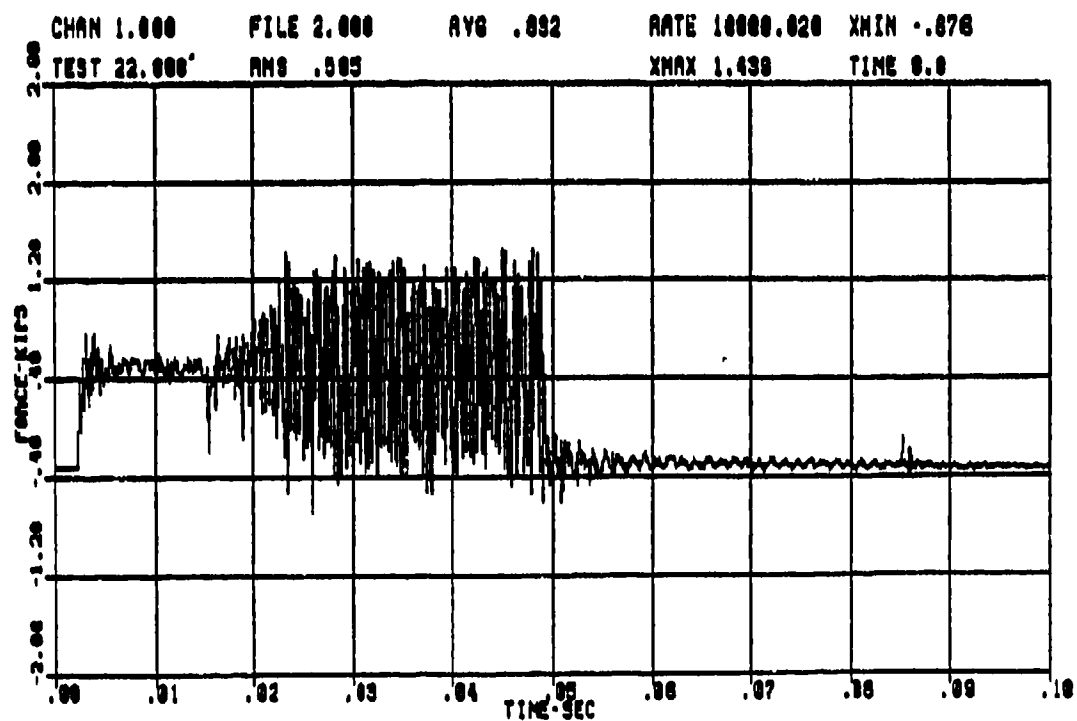
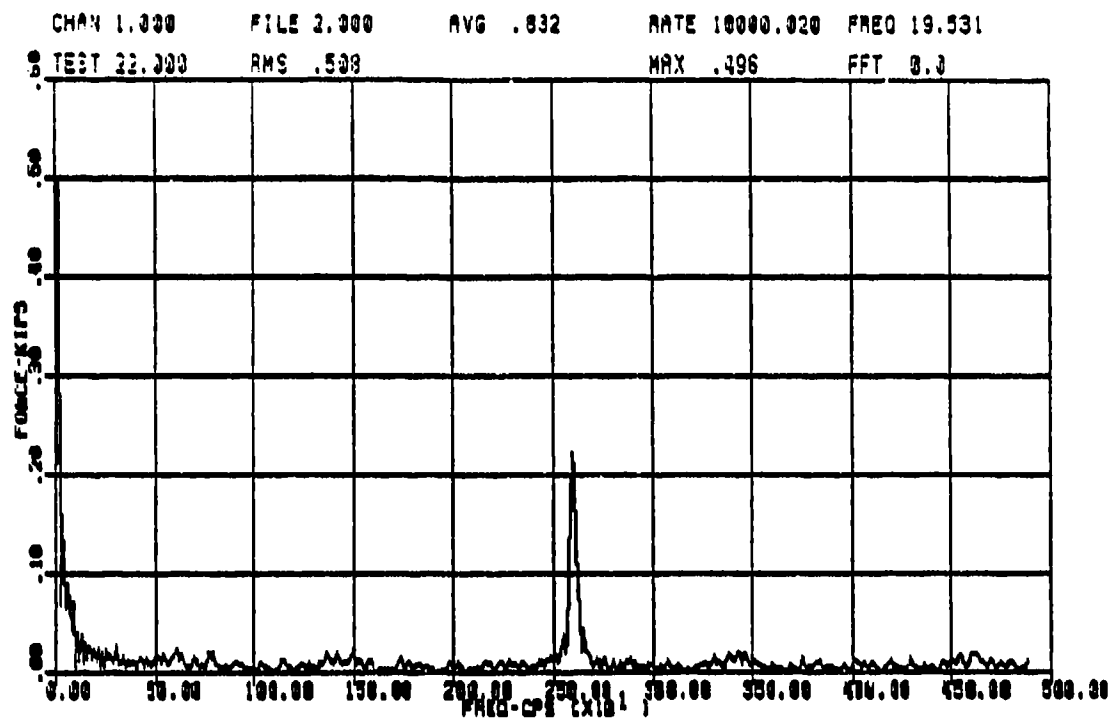
H3

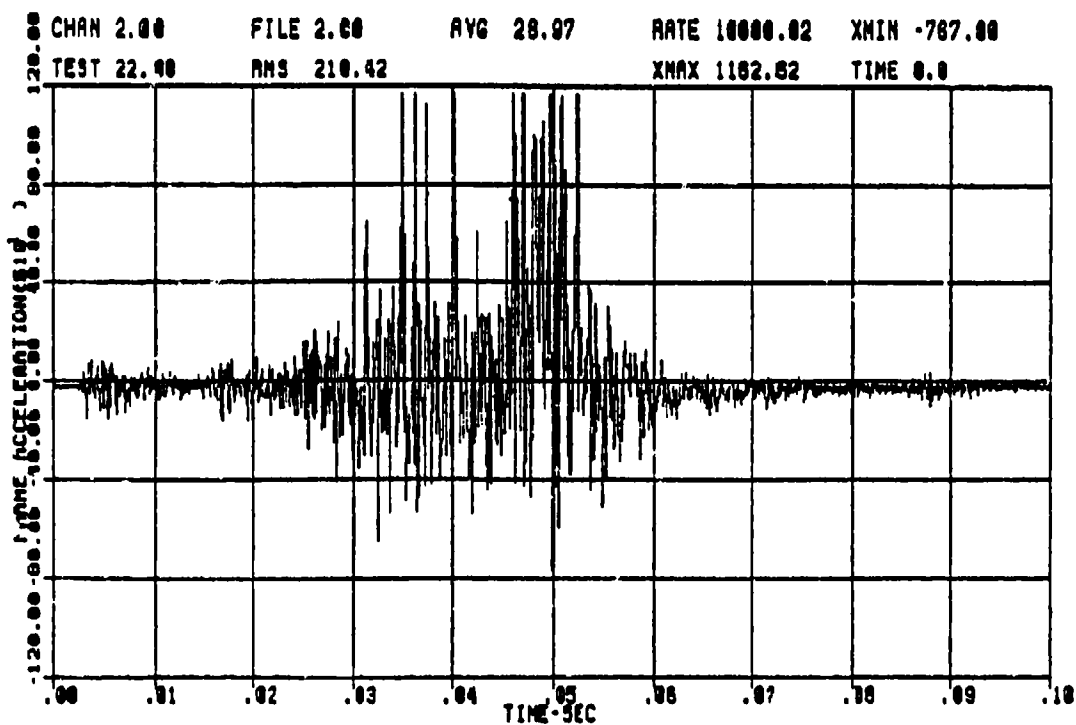
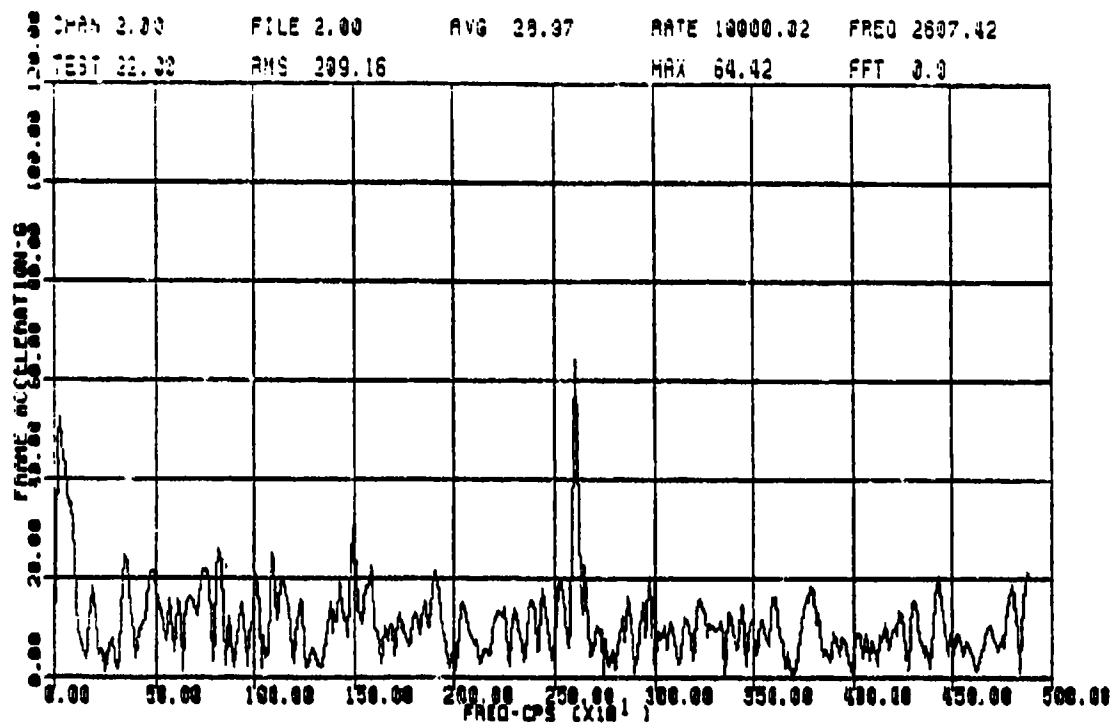


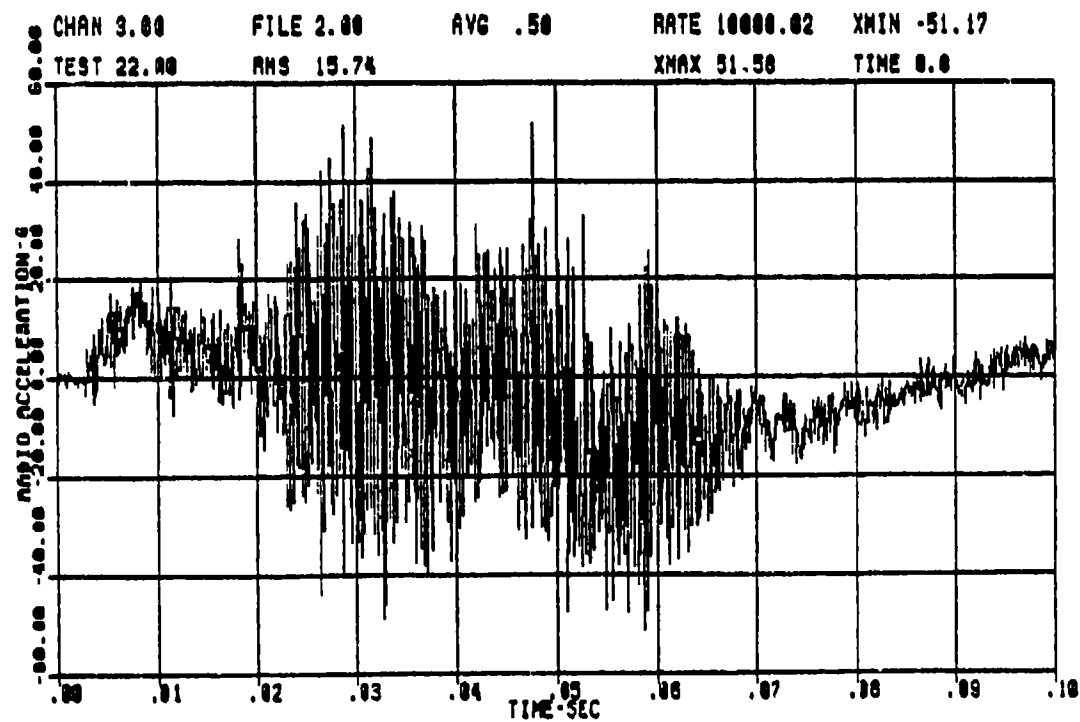
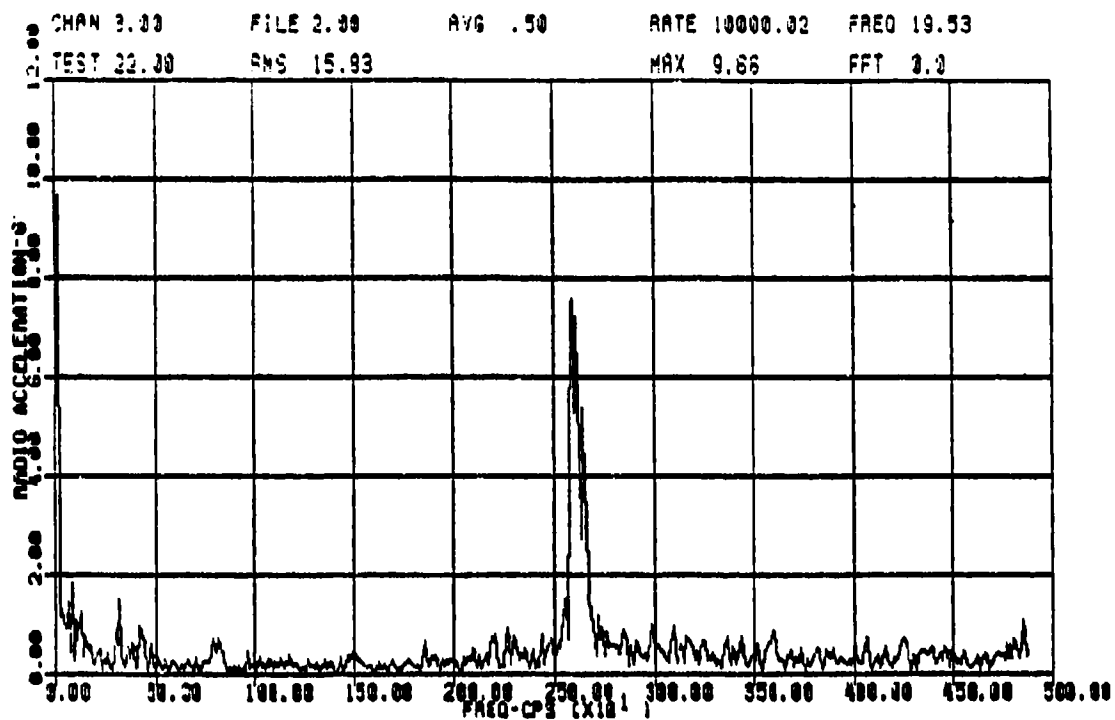


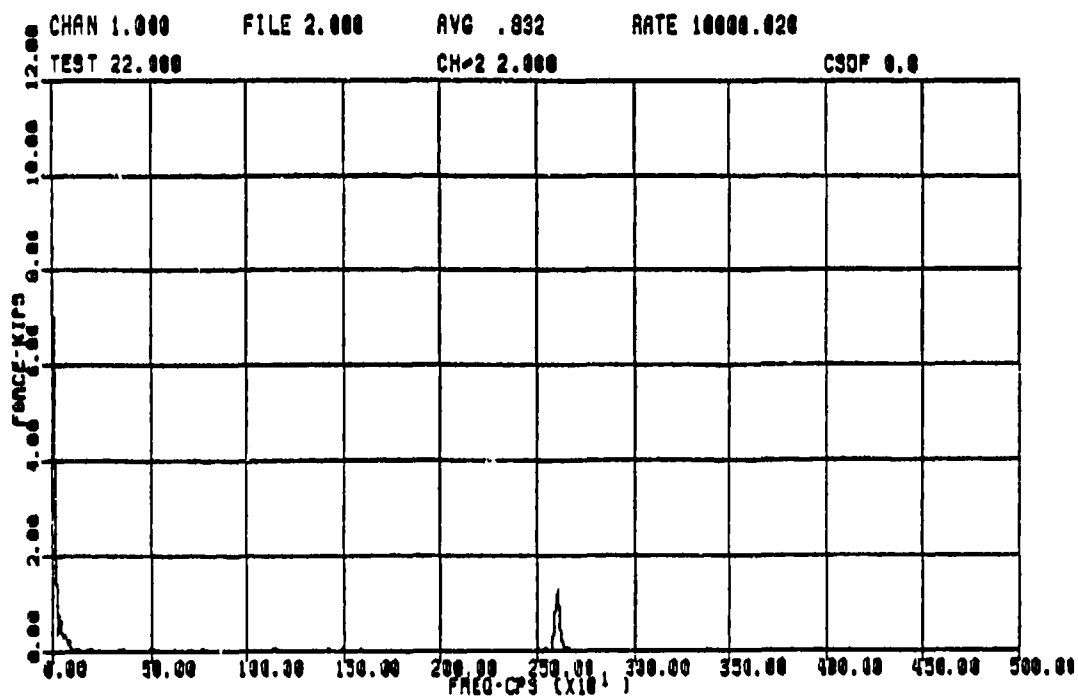
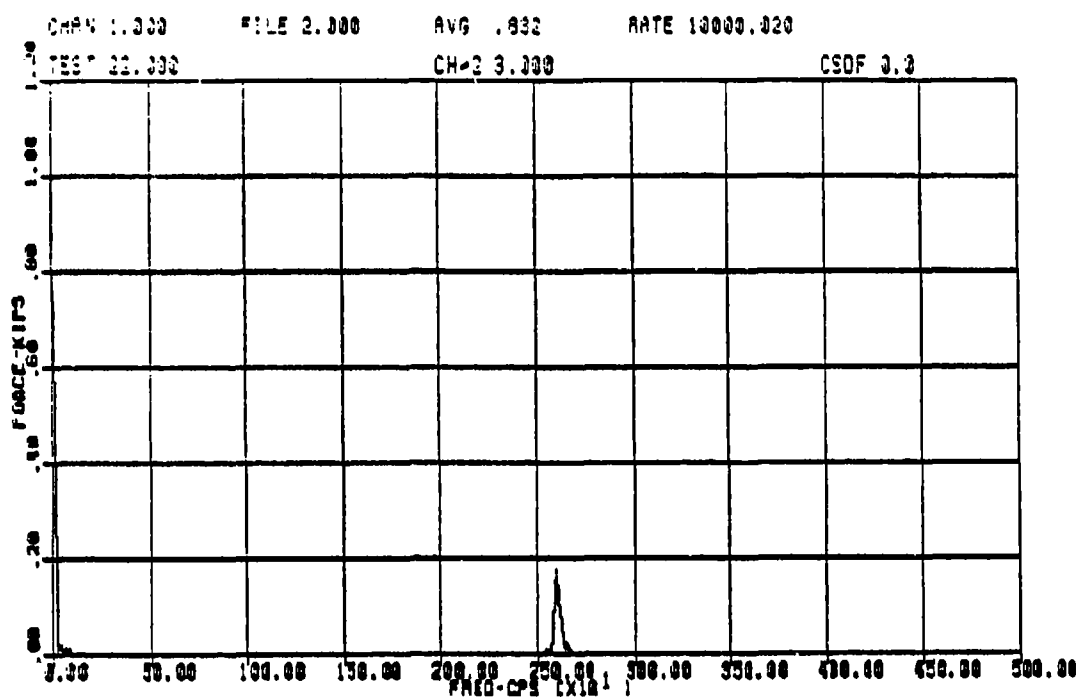


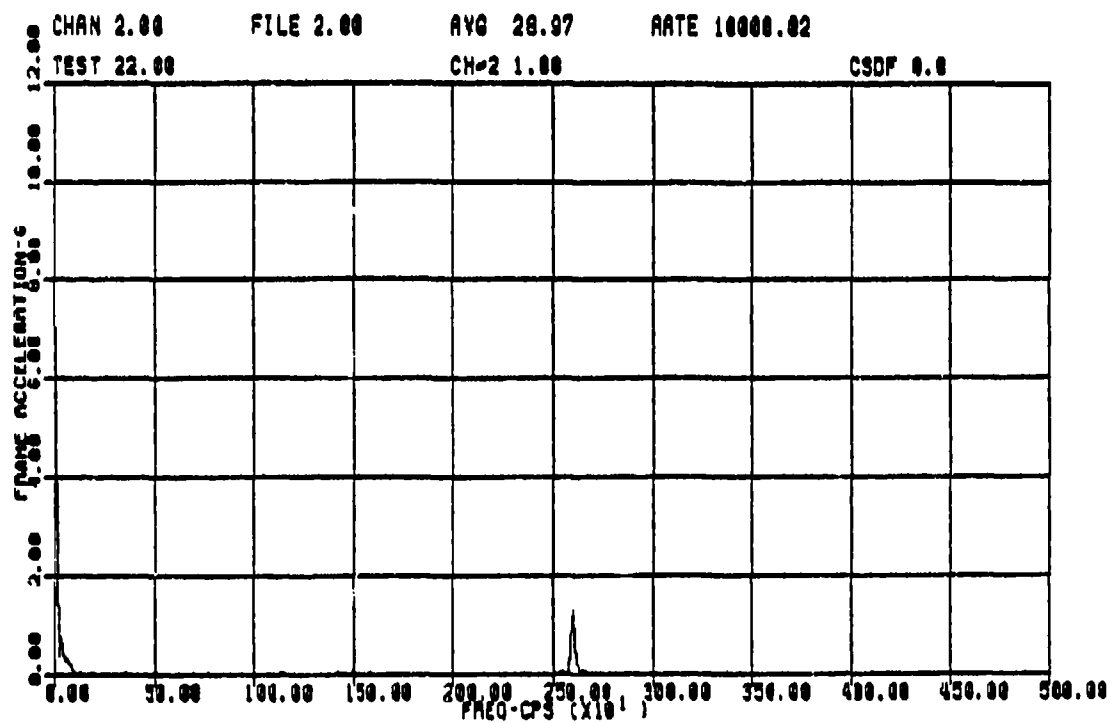
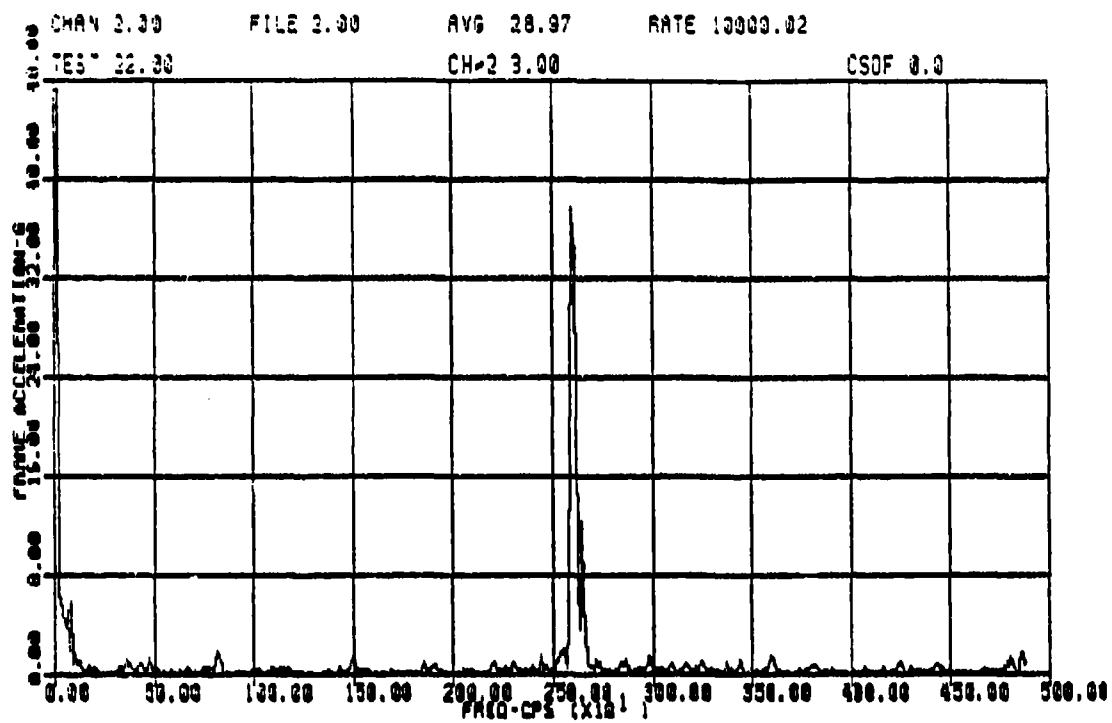


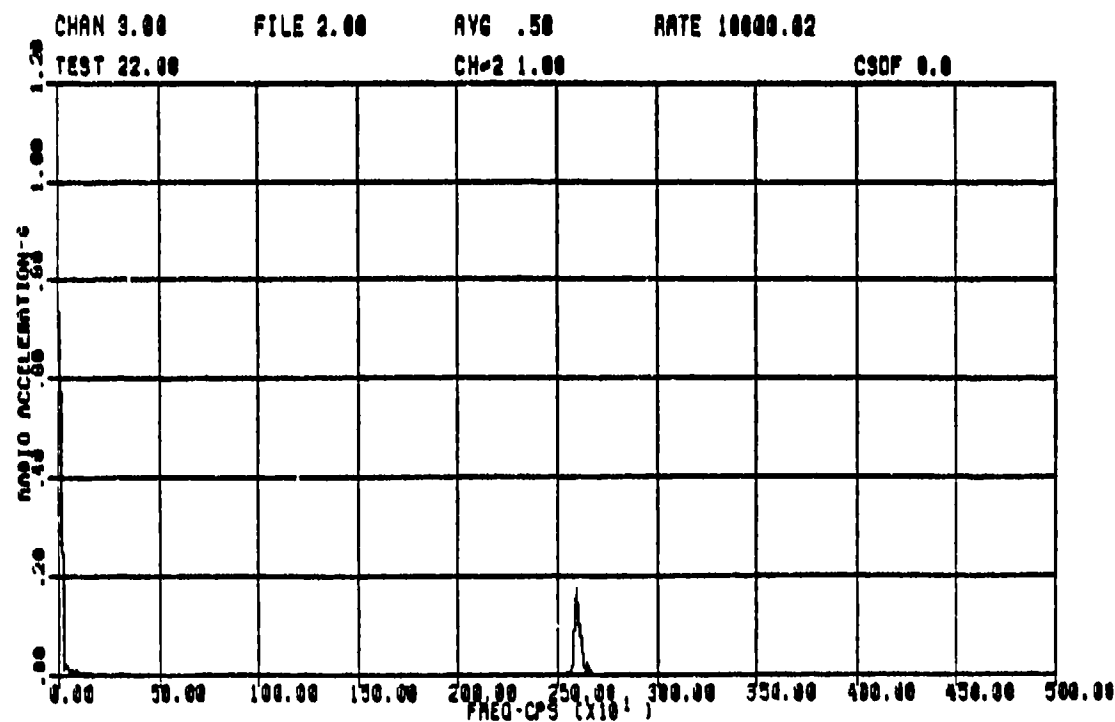
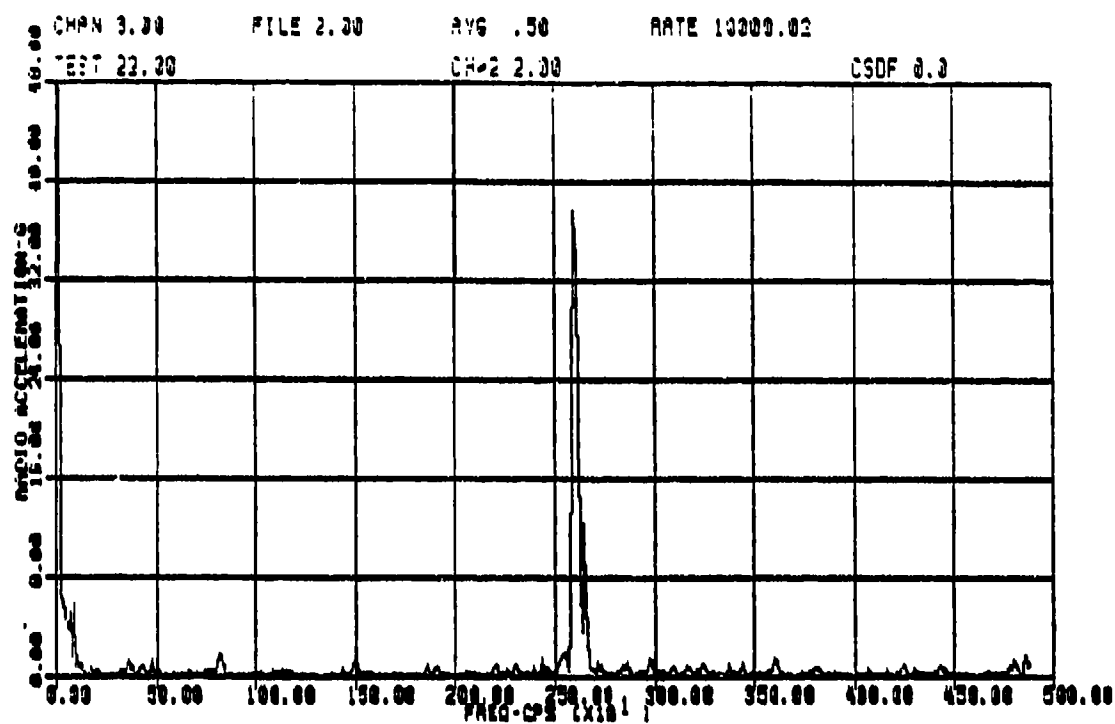


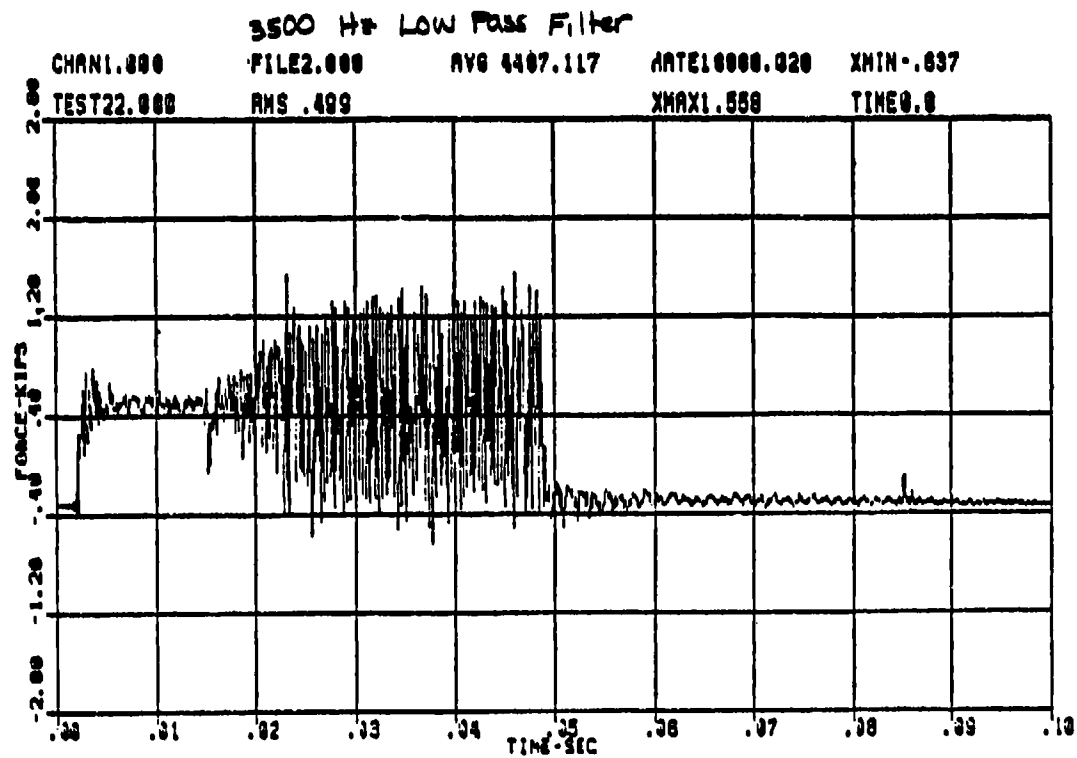
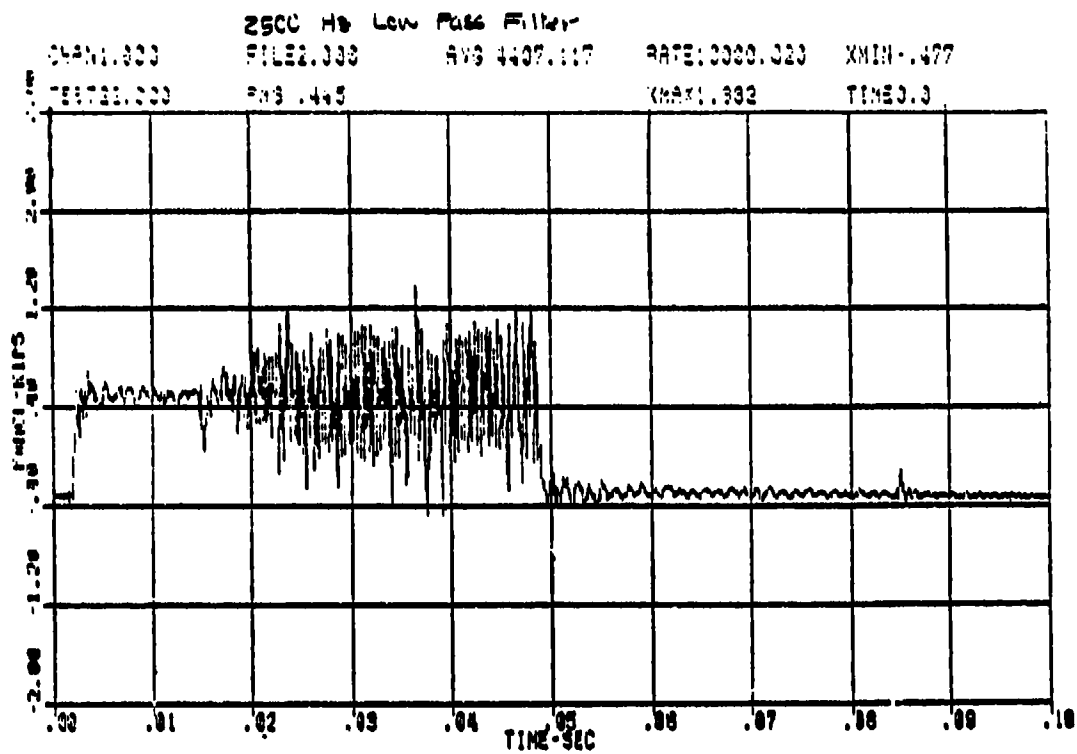




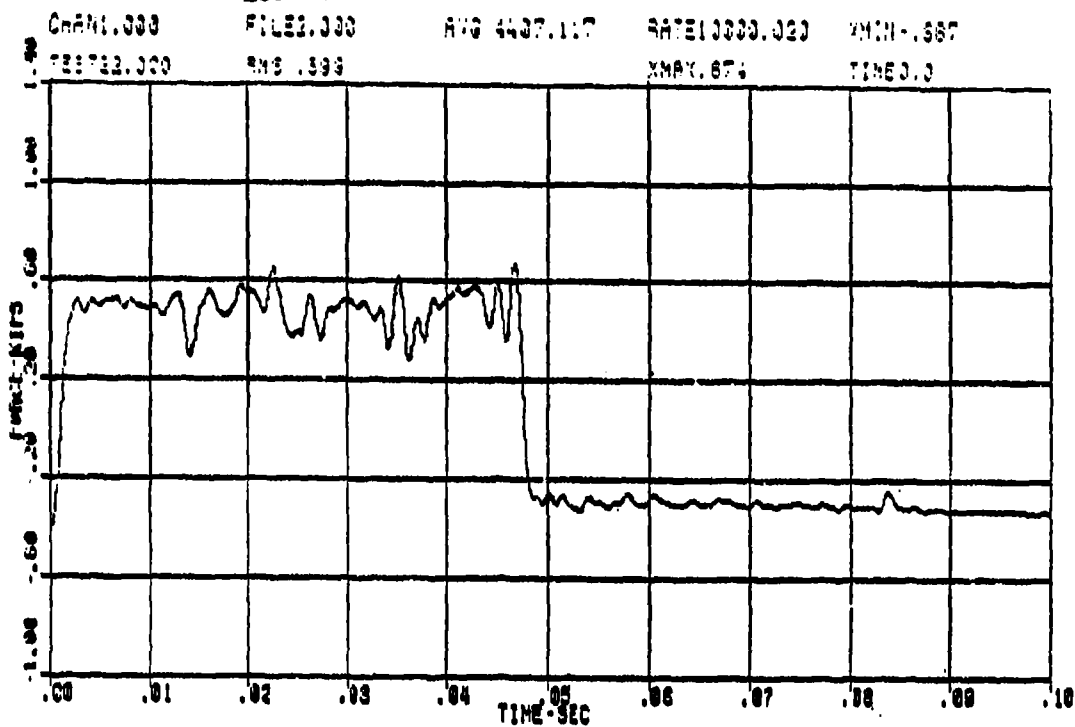




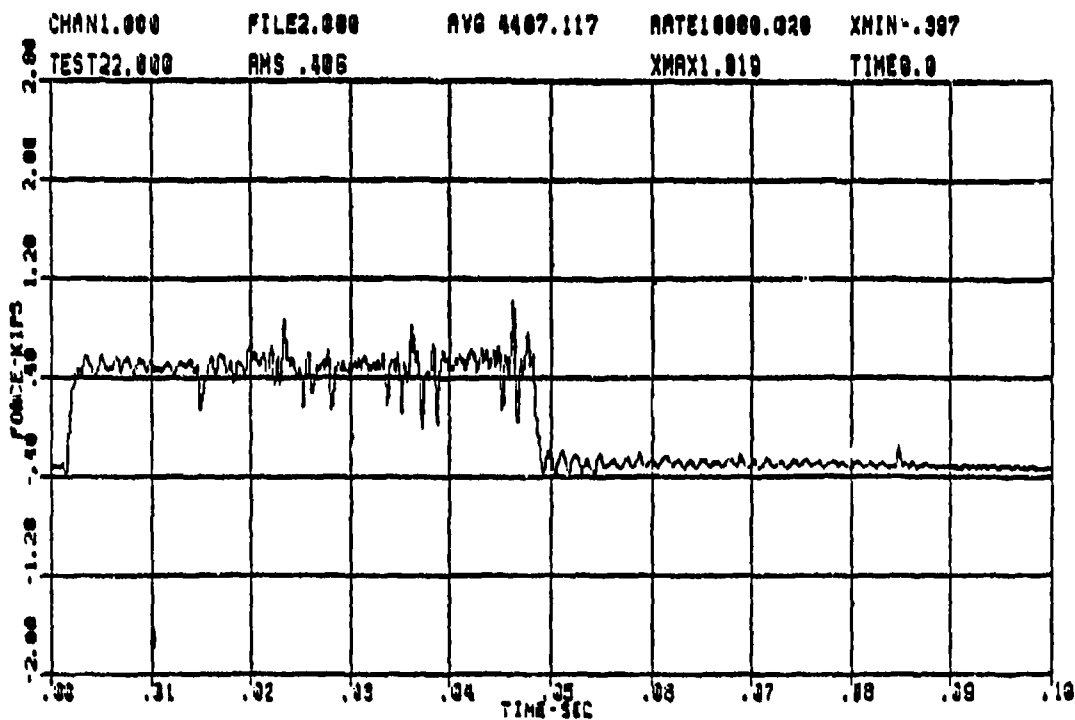


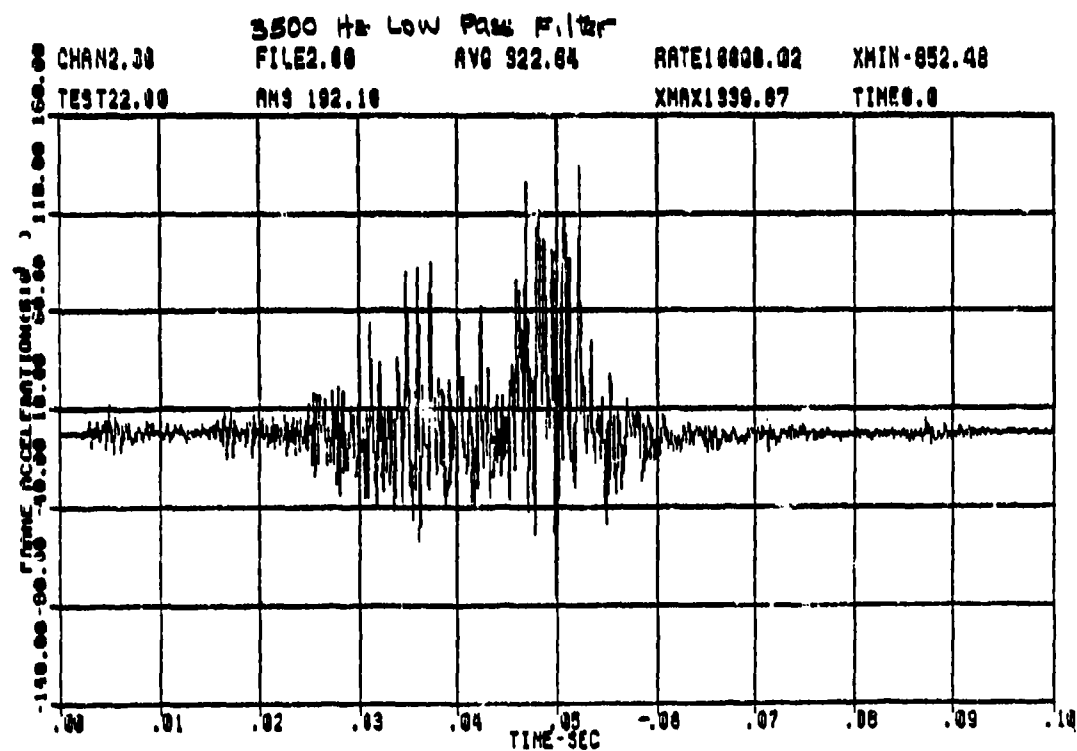
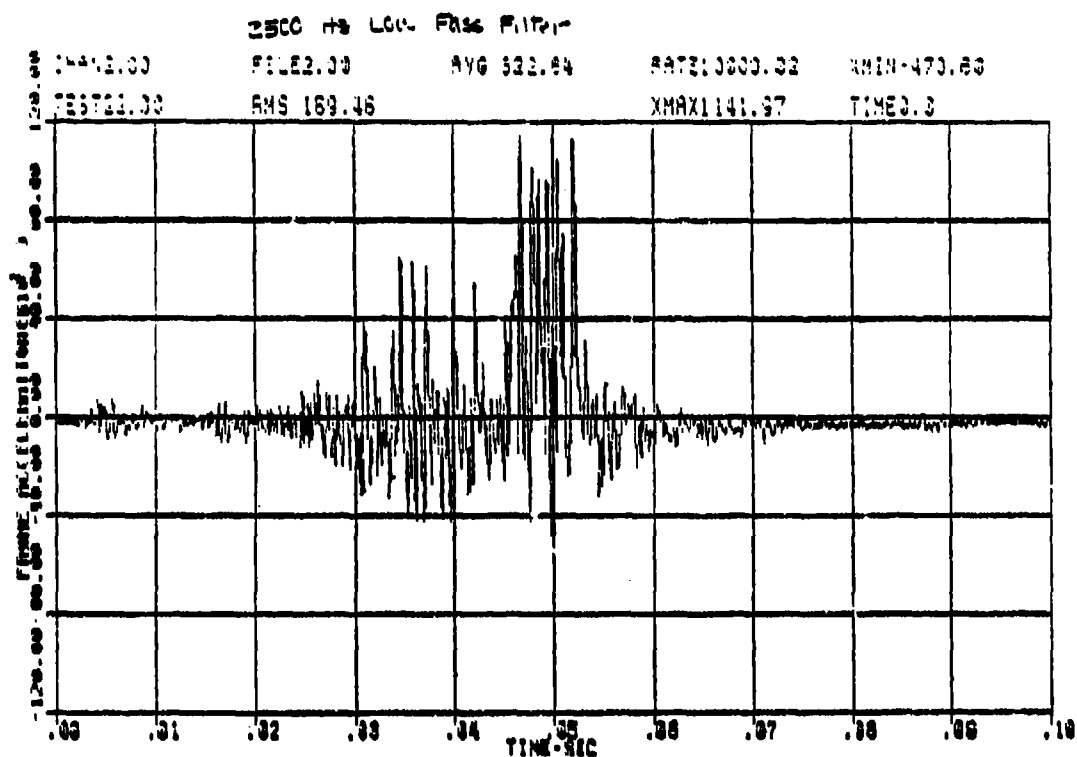


500 Hz Low Pass Filter

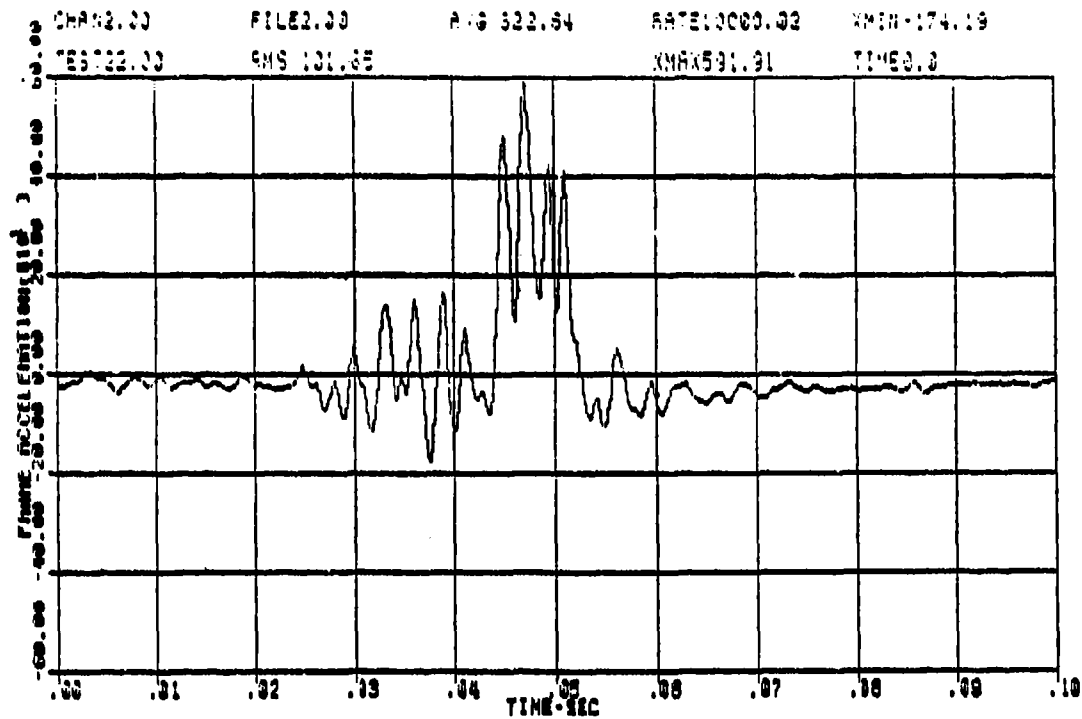


1500 Hz Low-Pass Filter

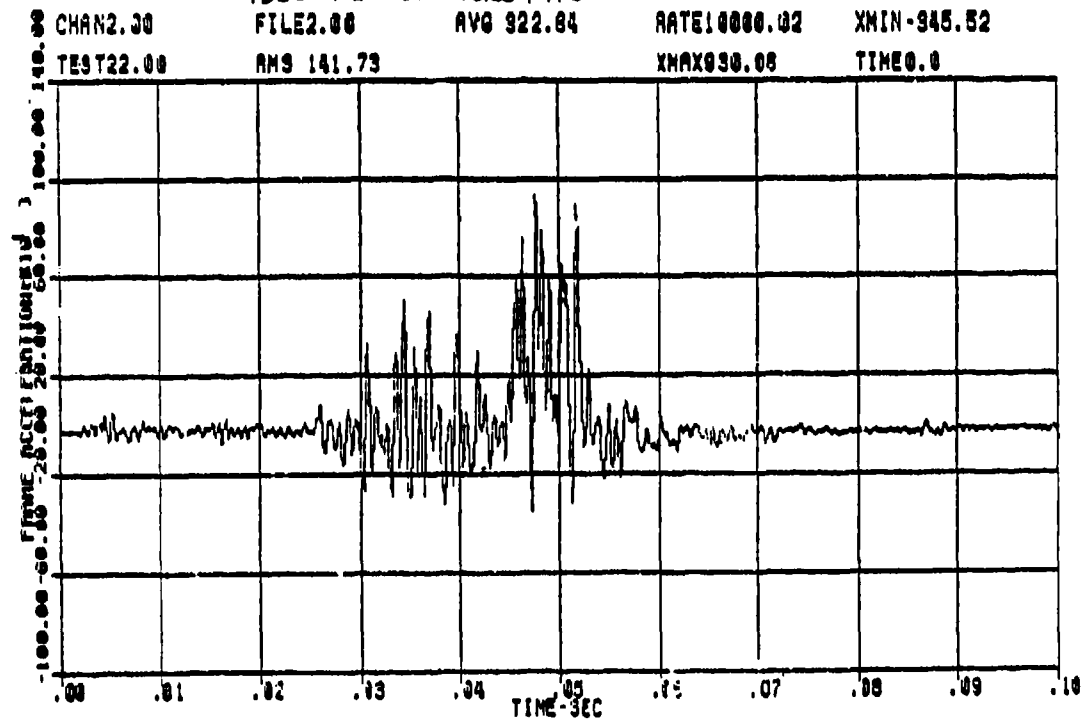


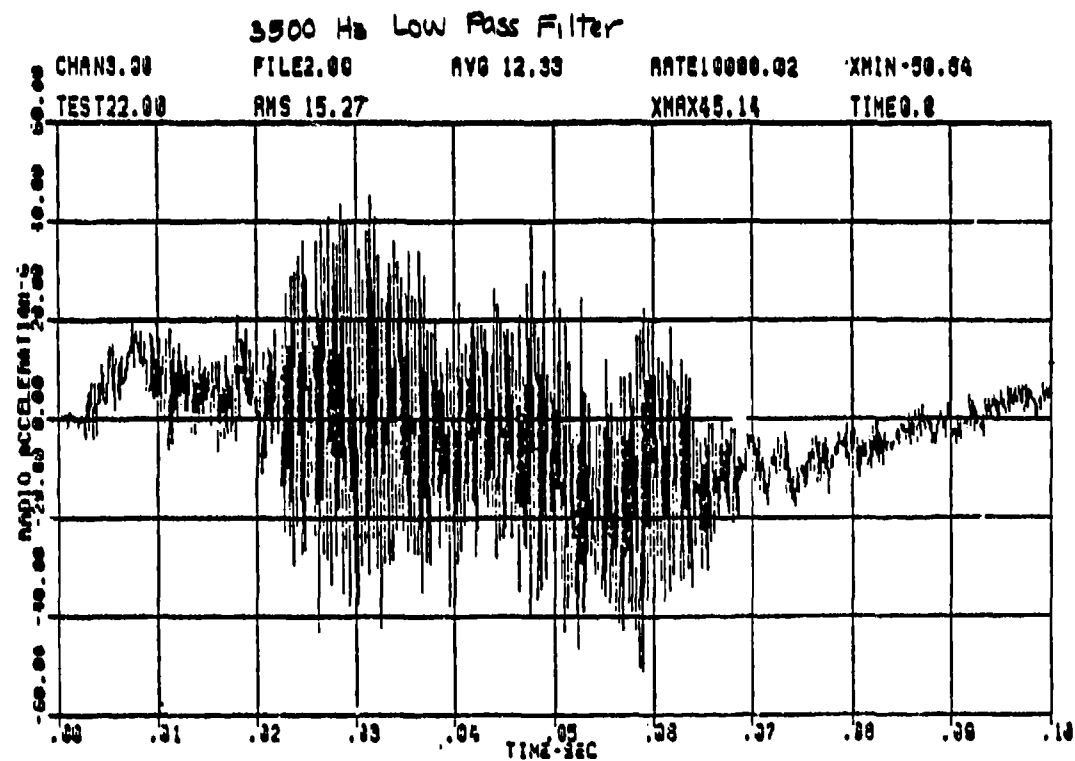
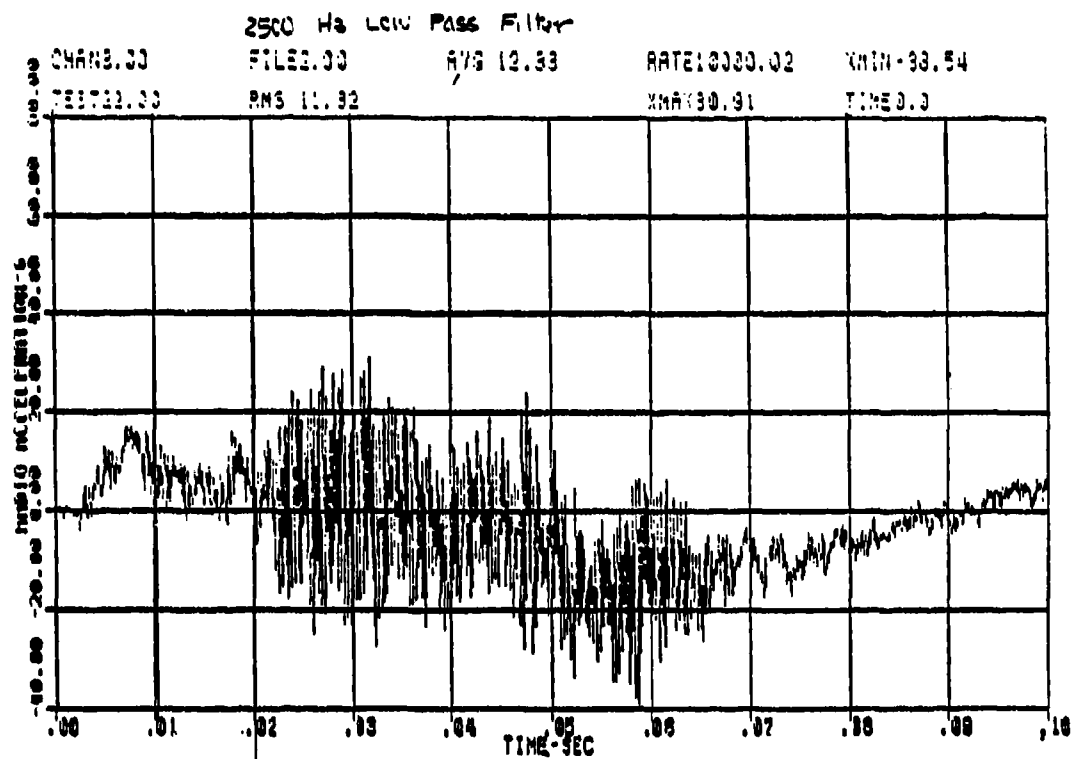


500 Hz Low Pass Filter

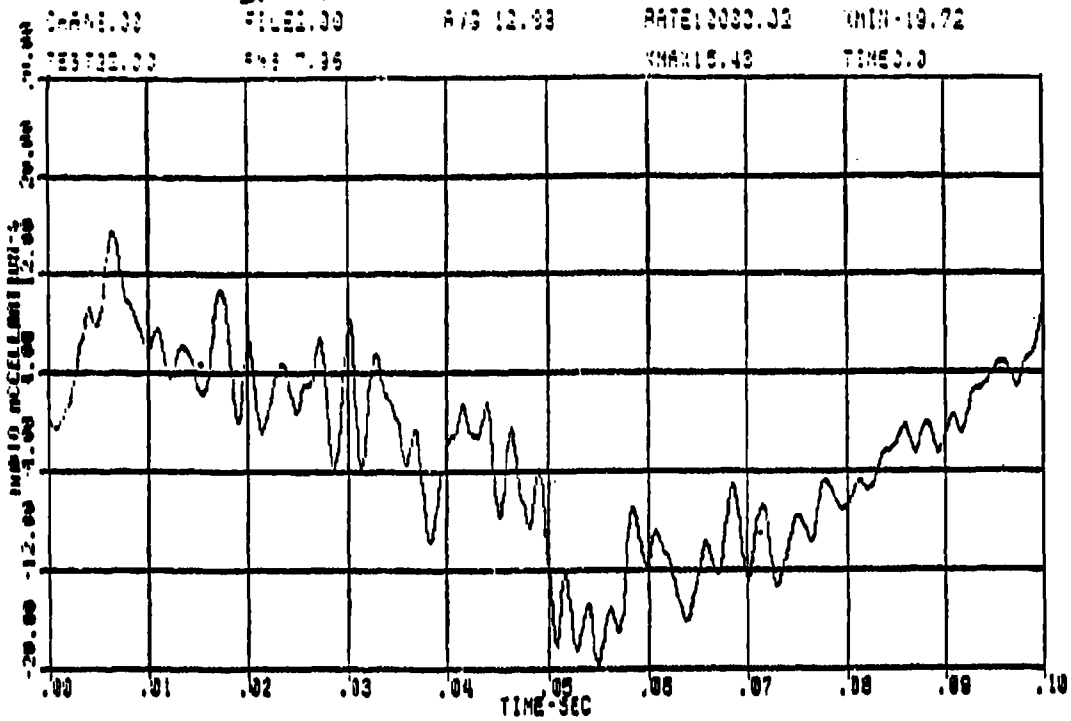


1500 Hz Low - Pass Filter

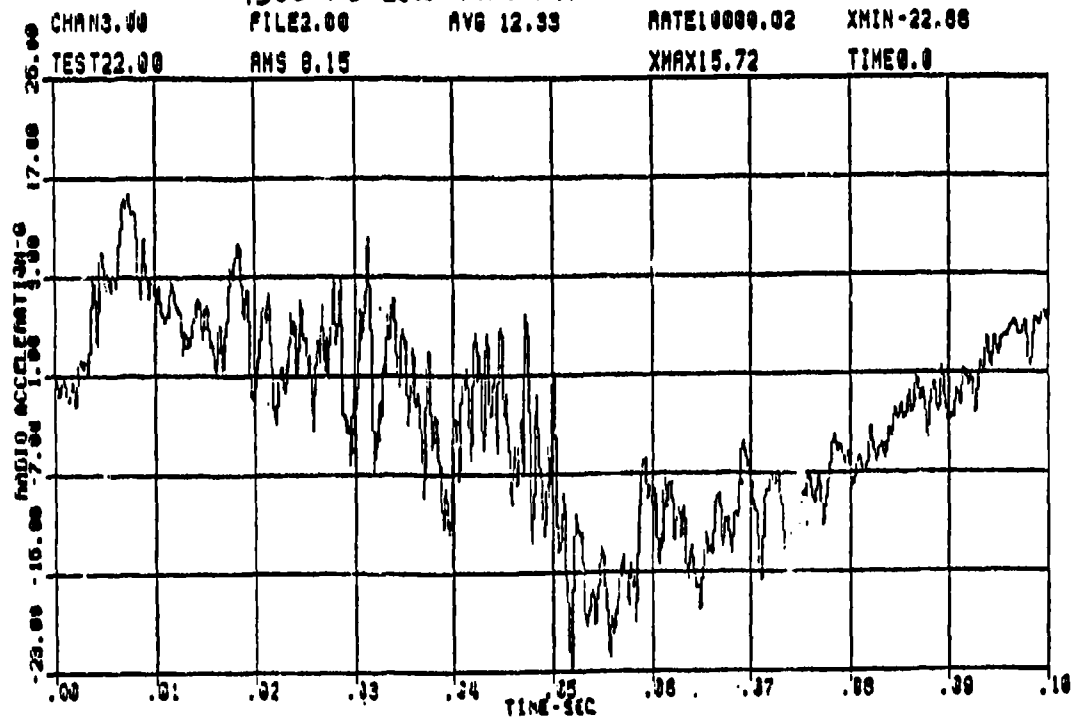




500 Hz Low Pass Filter

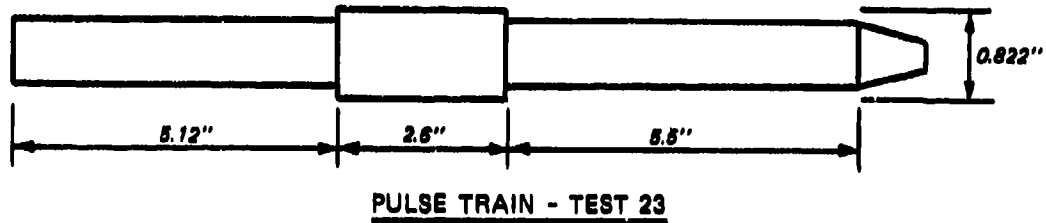


1500 Hz Low-Pass Filter

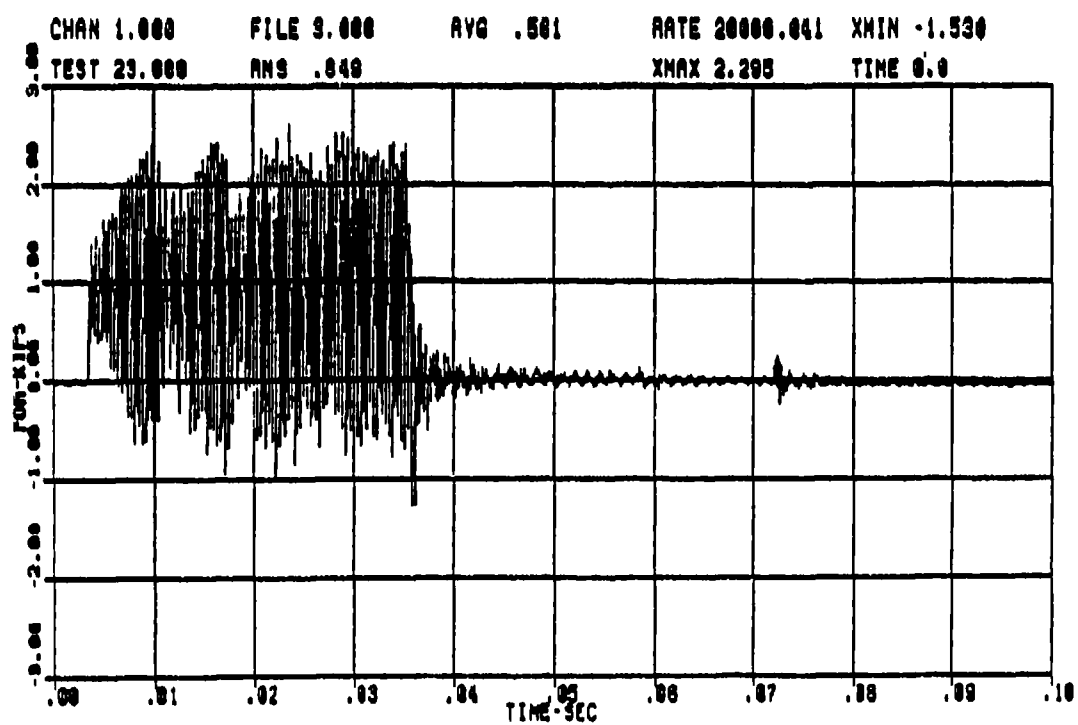
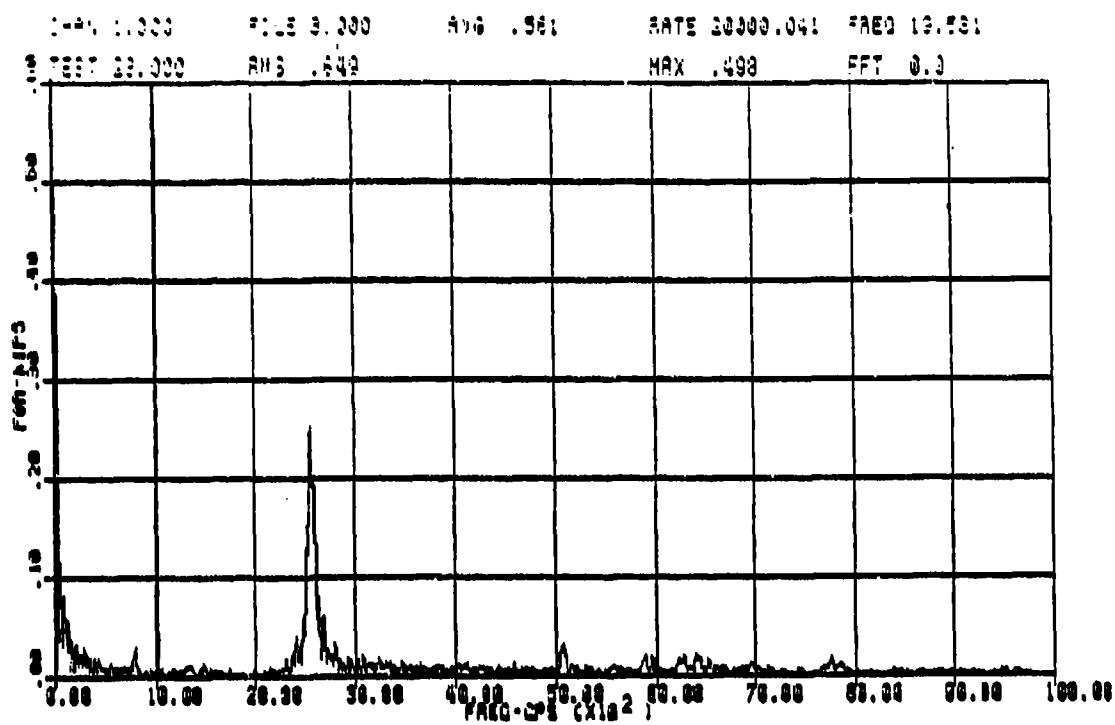


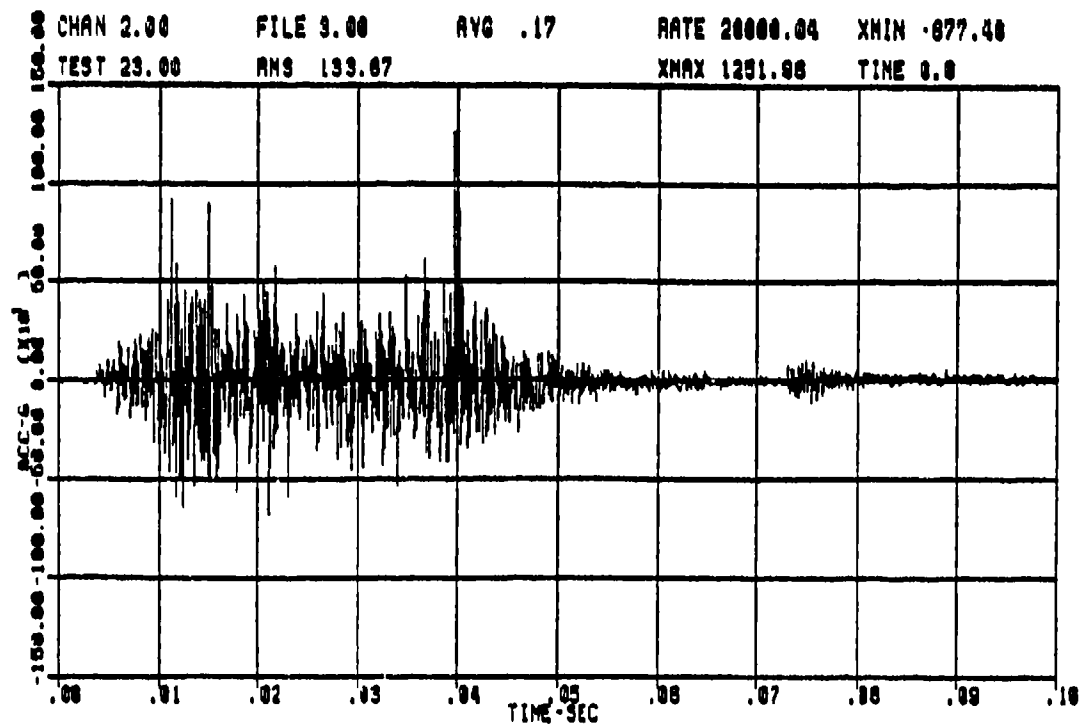
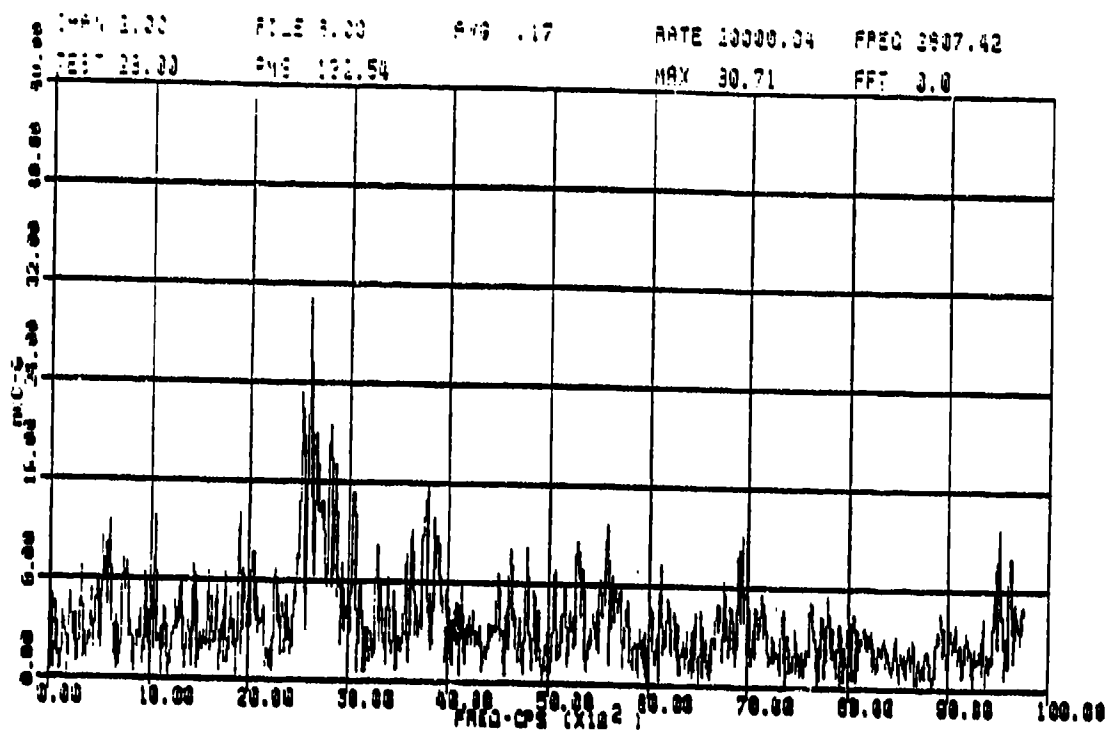
APPENDIX I: TEST 23 RESULTS

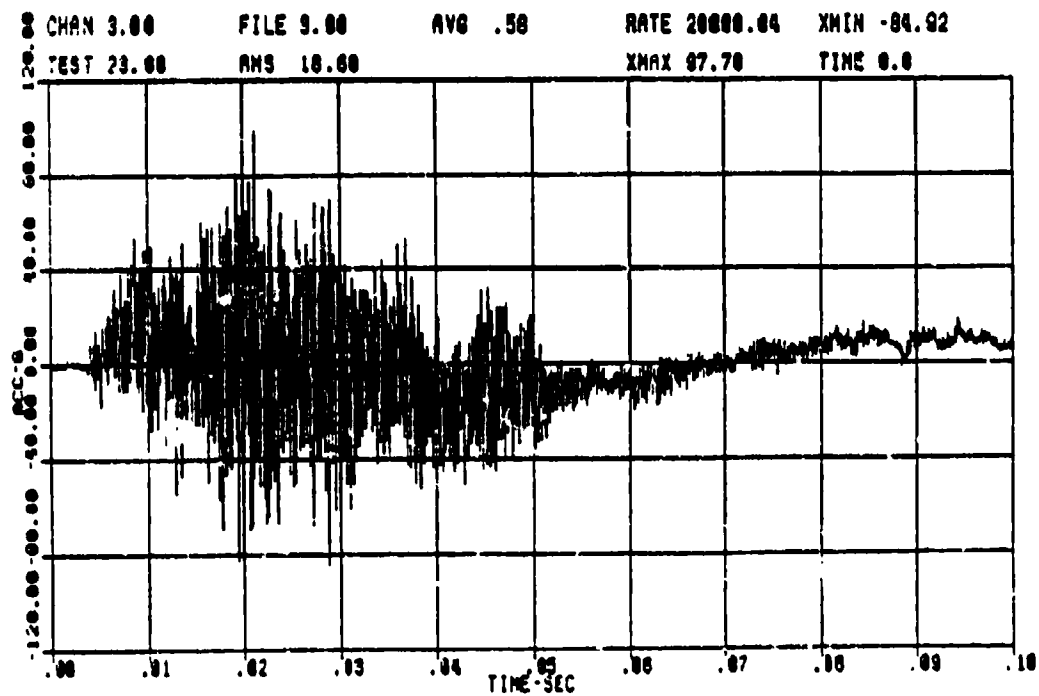
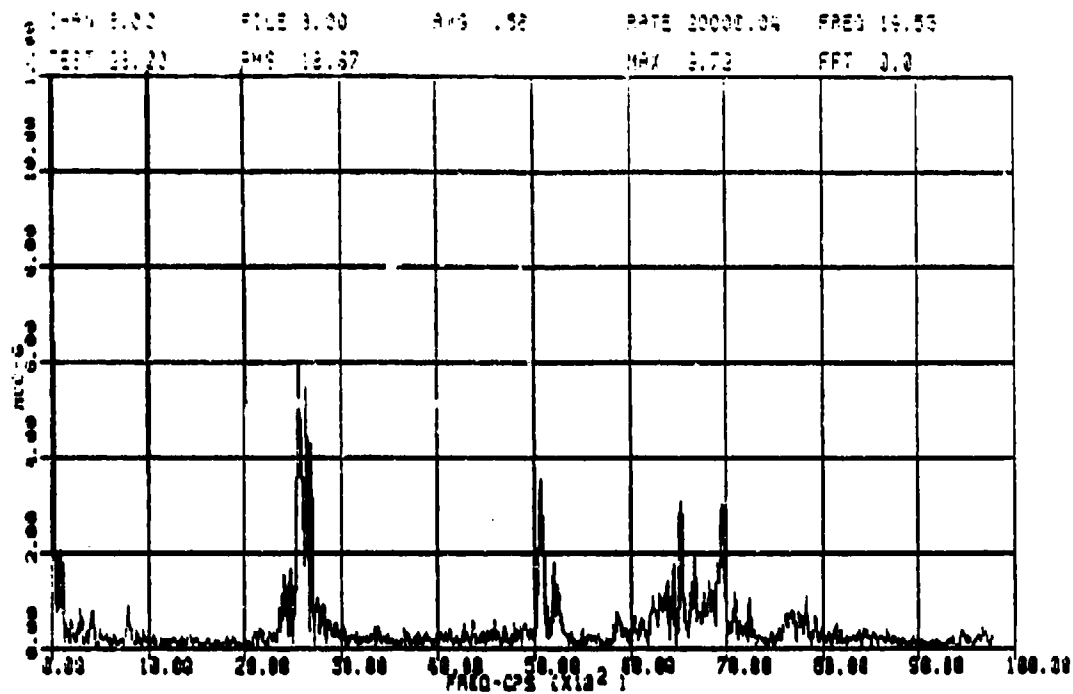
Test 23
Equipment Rack Soft-Mounted
AN/GRC-103 in Rack, Off-Line

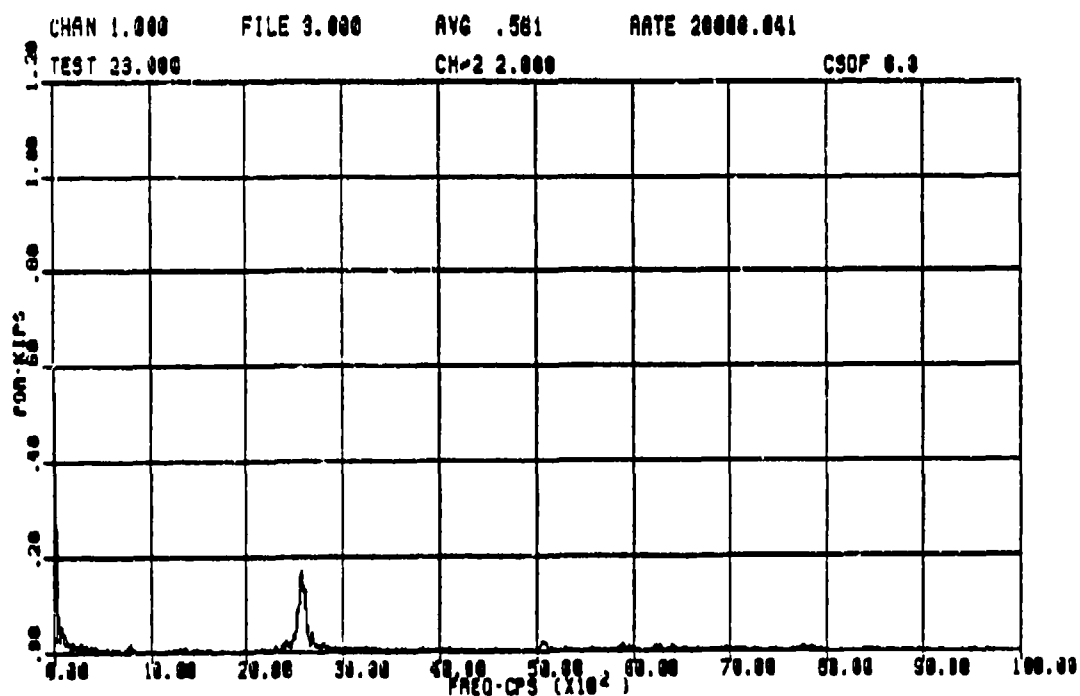
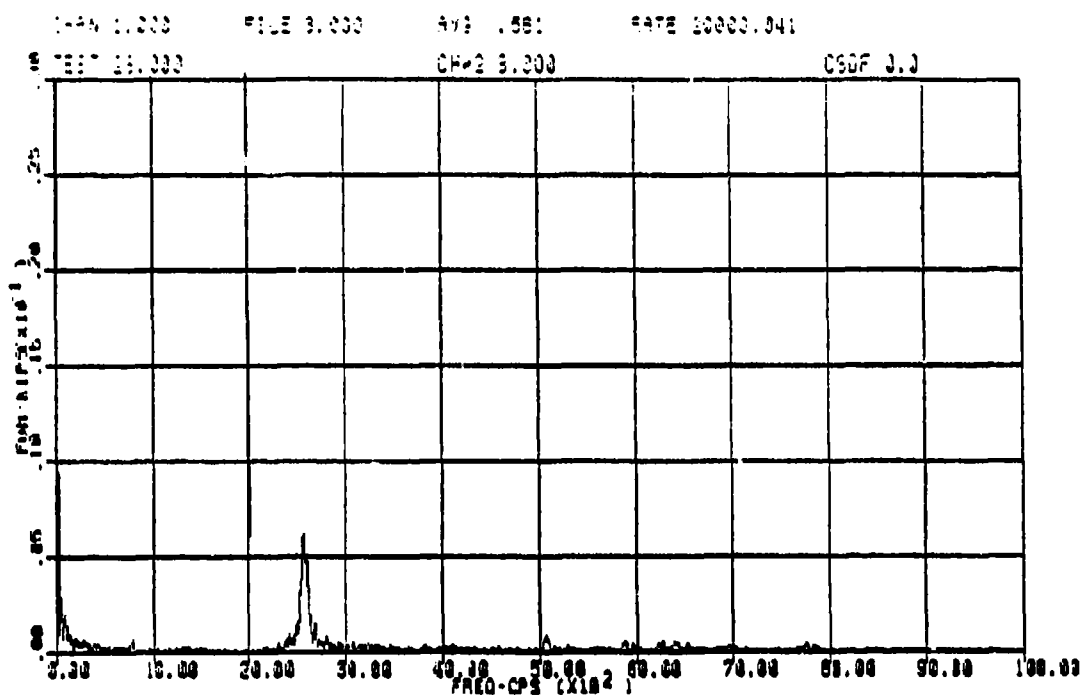


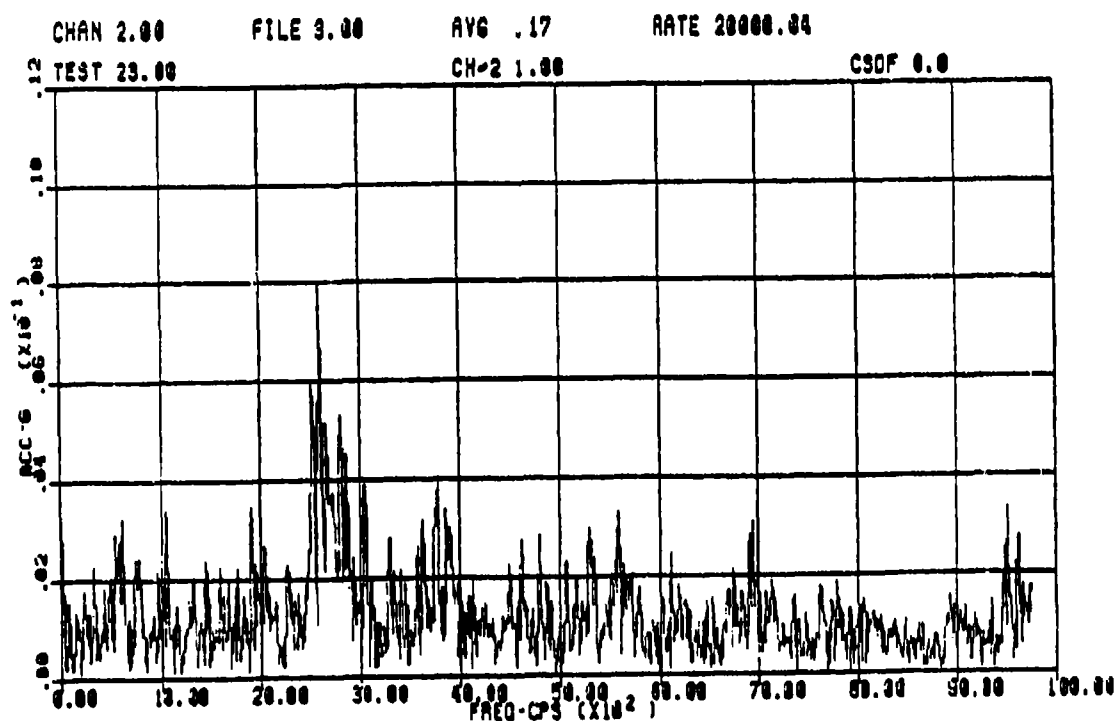
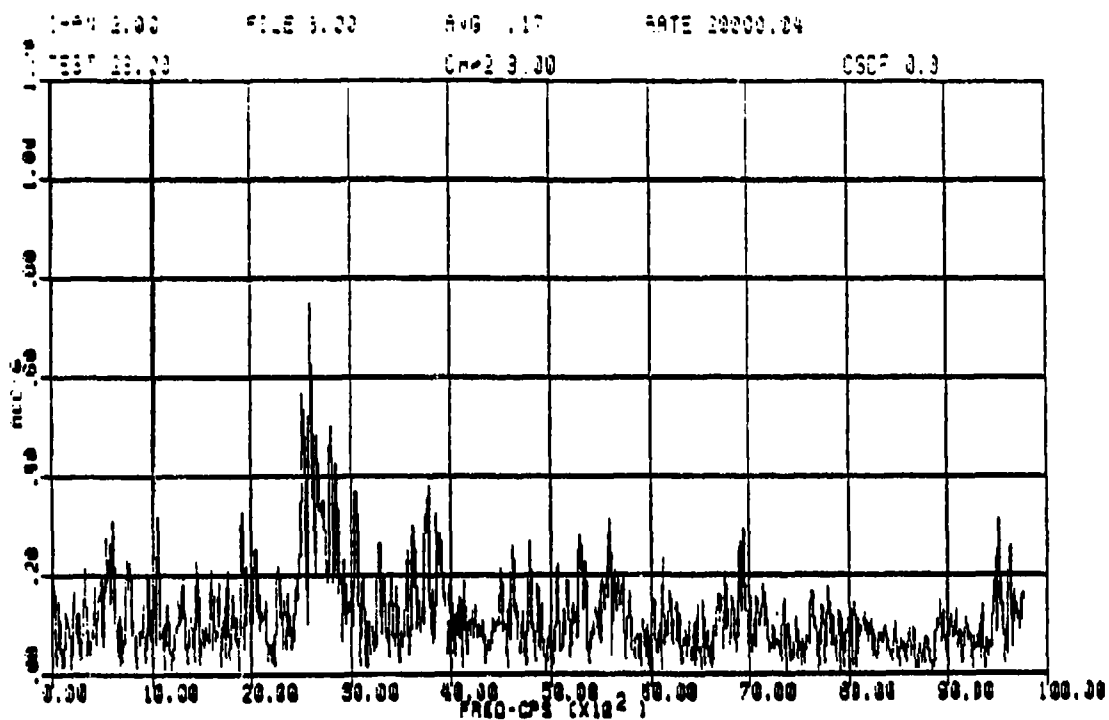
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #64
AIR BAG PRESSURE = 70 PSI

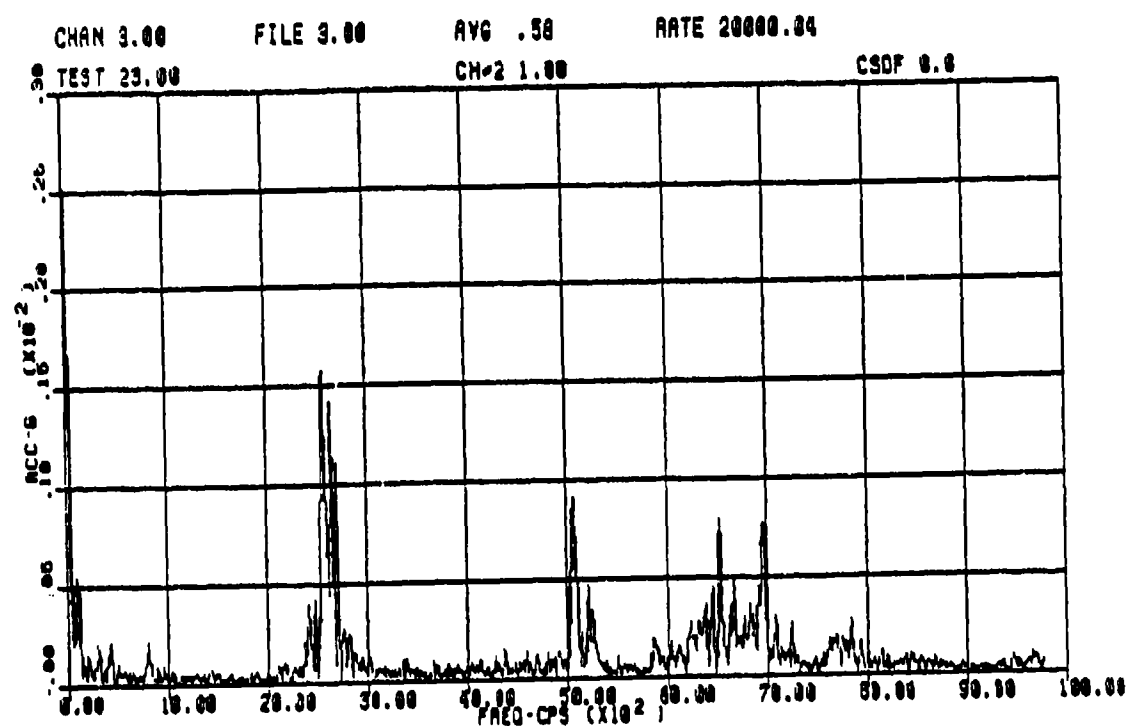
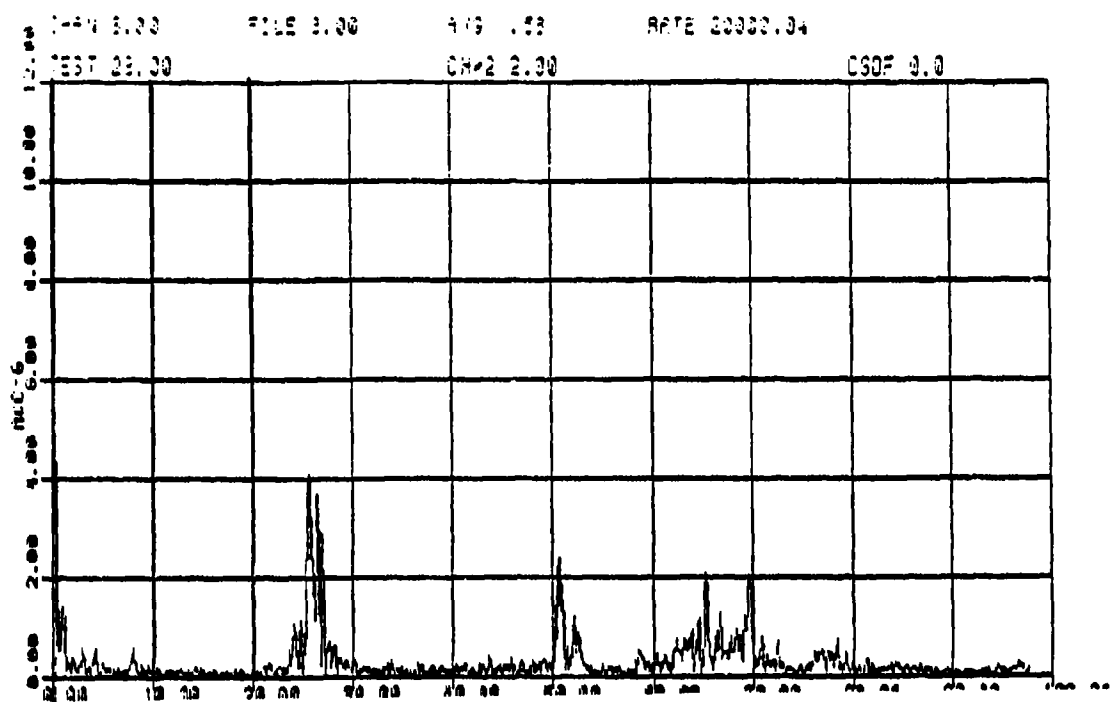


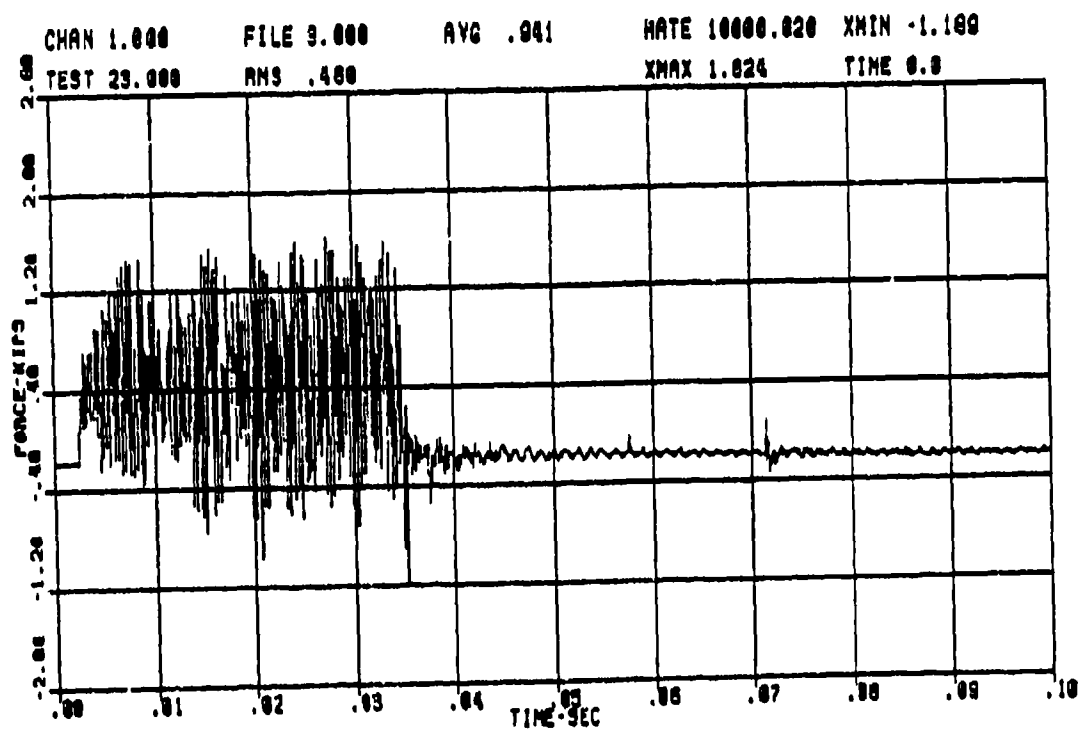
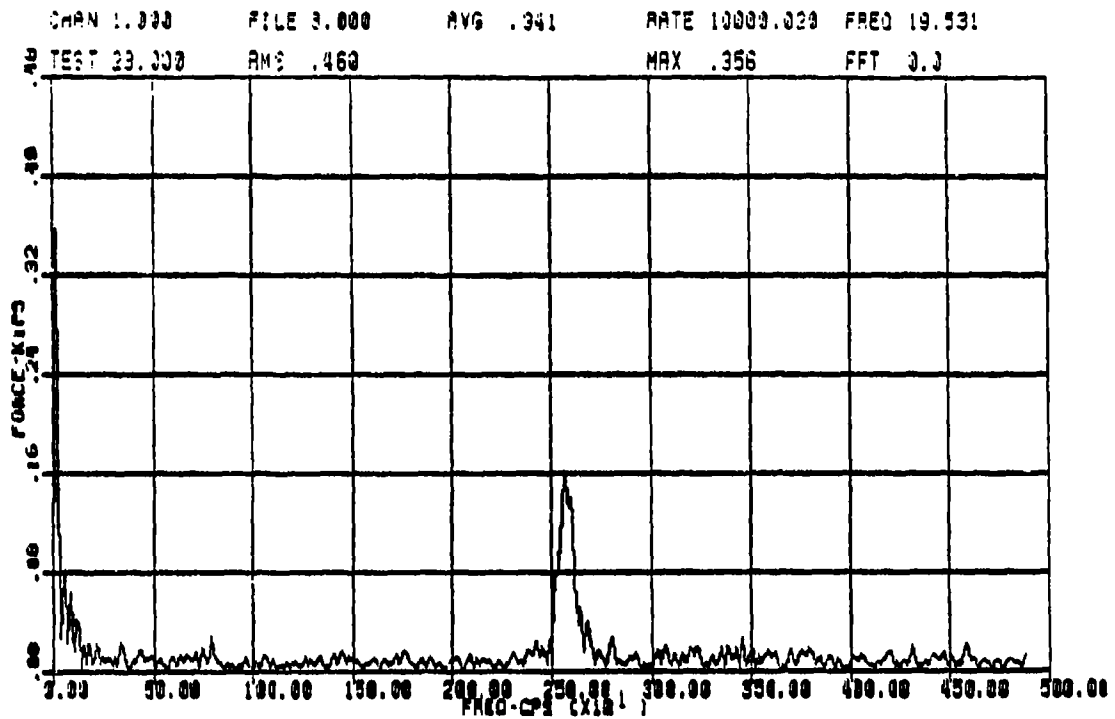


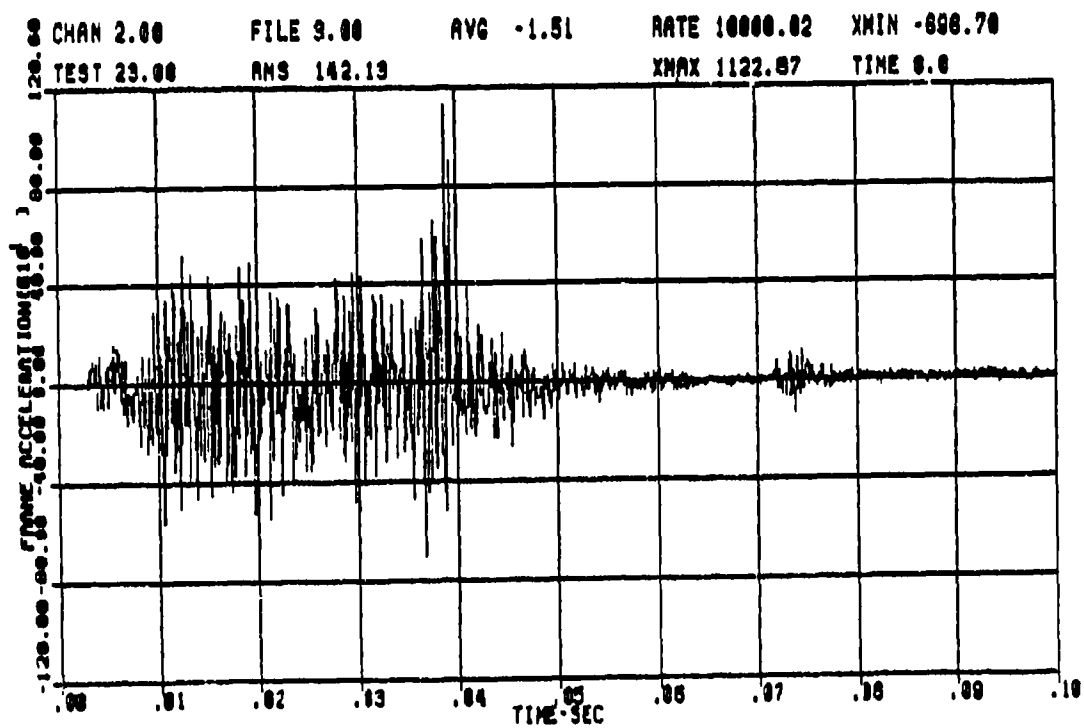
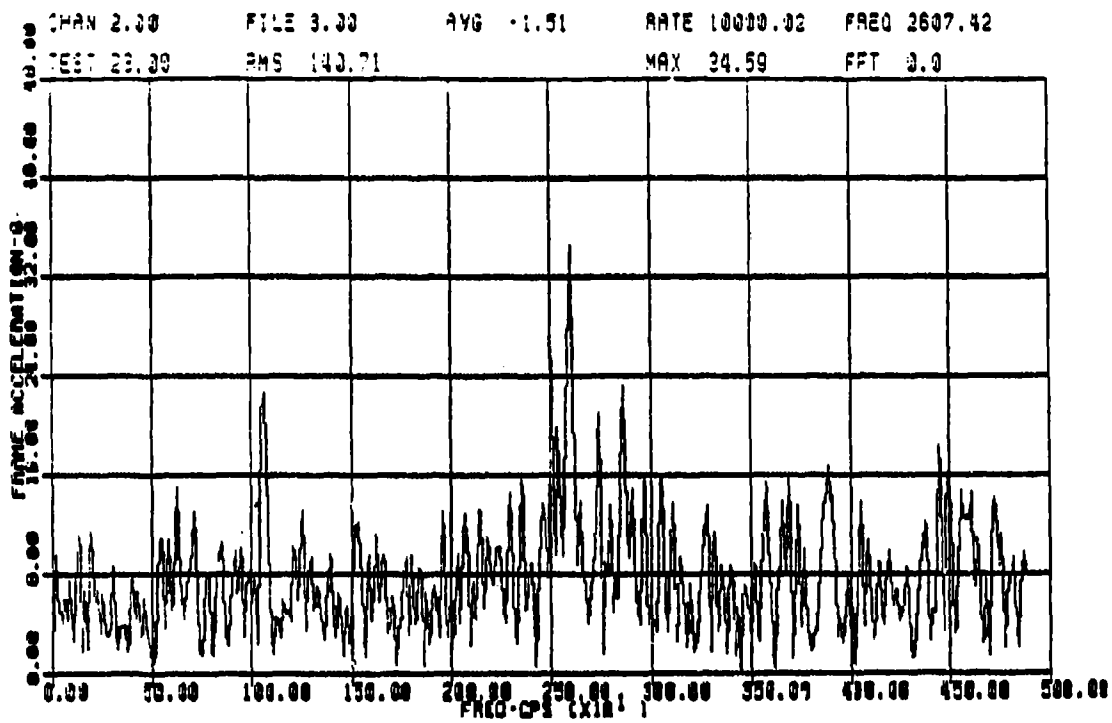


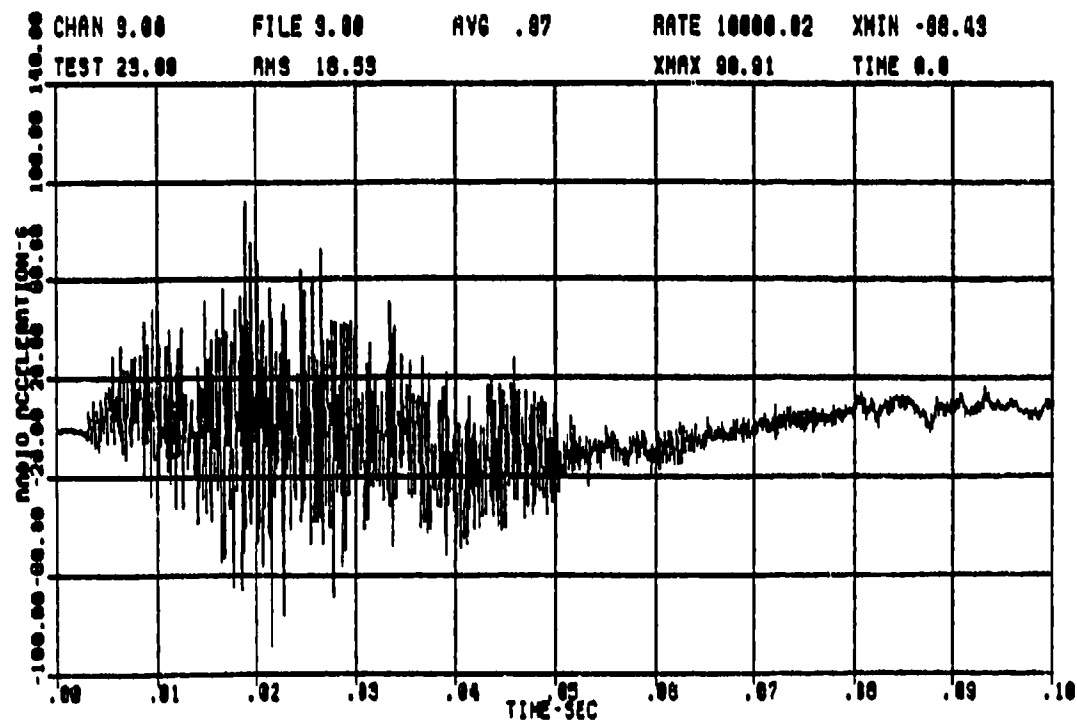
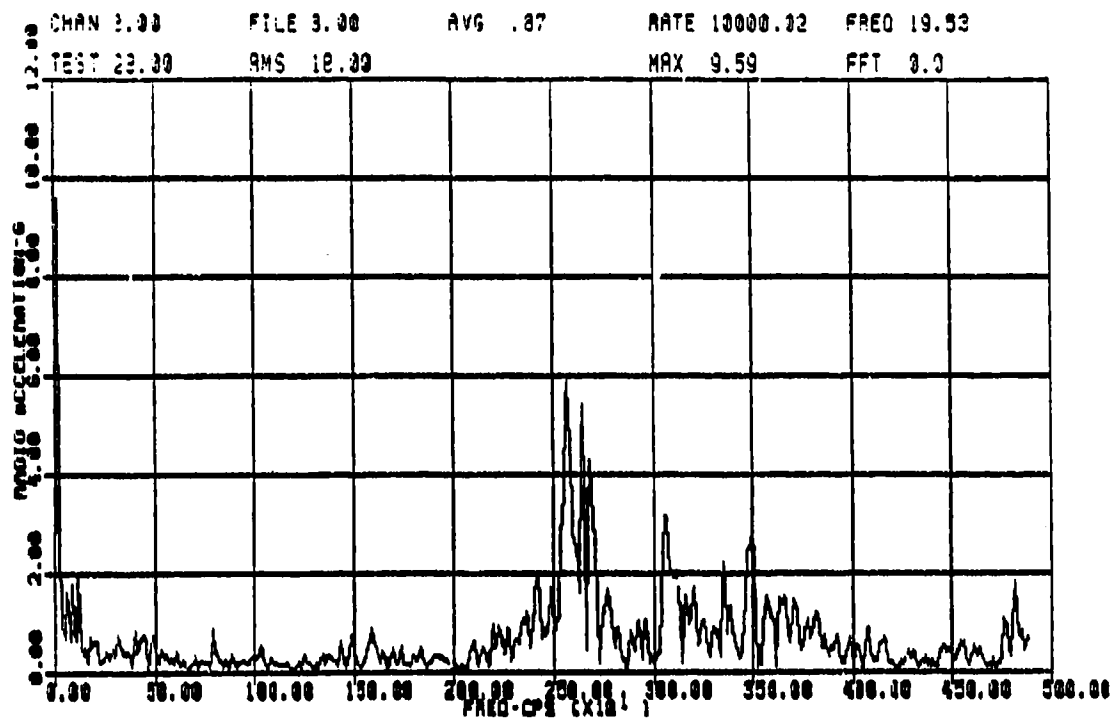


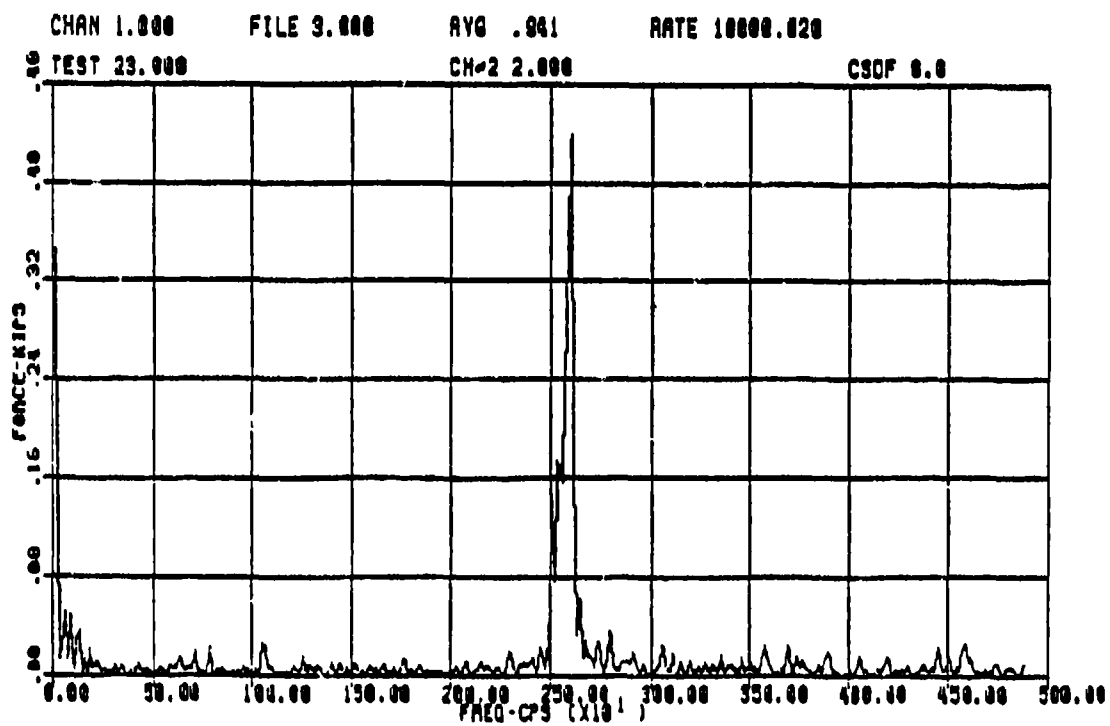
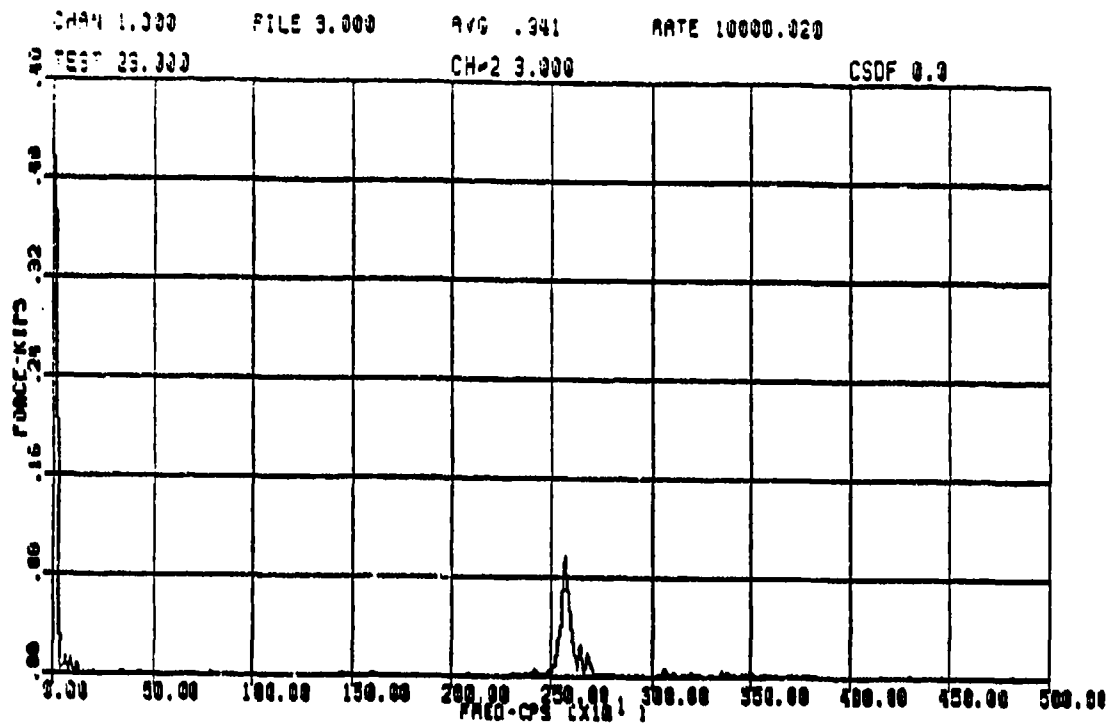


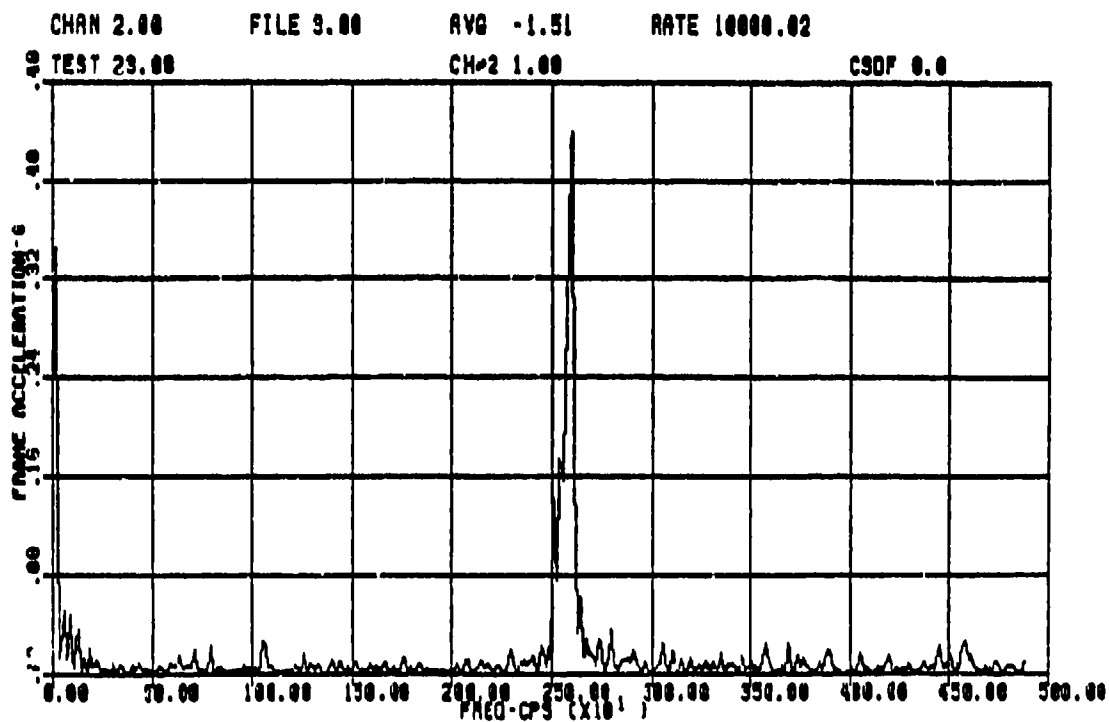
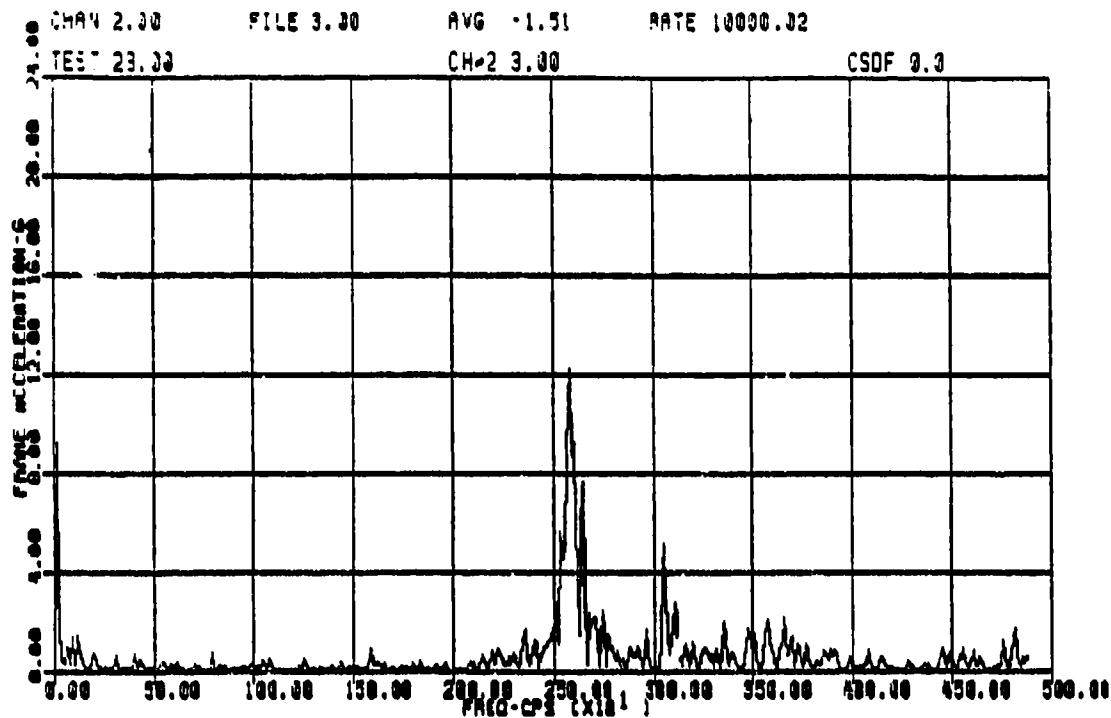


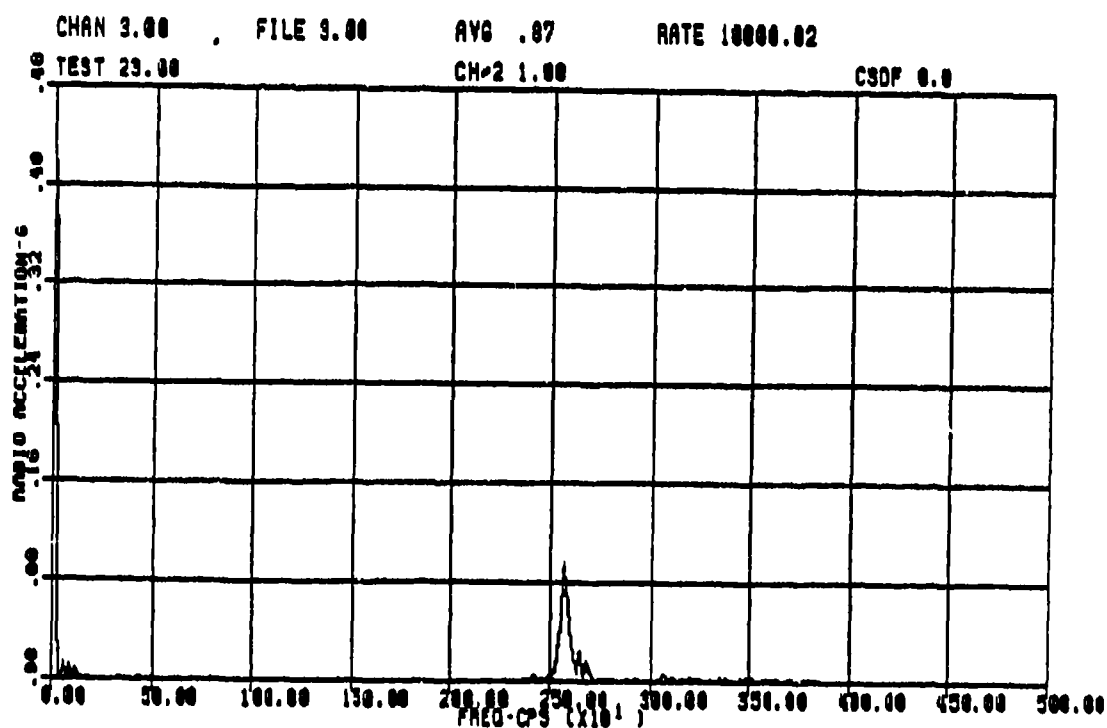
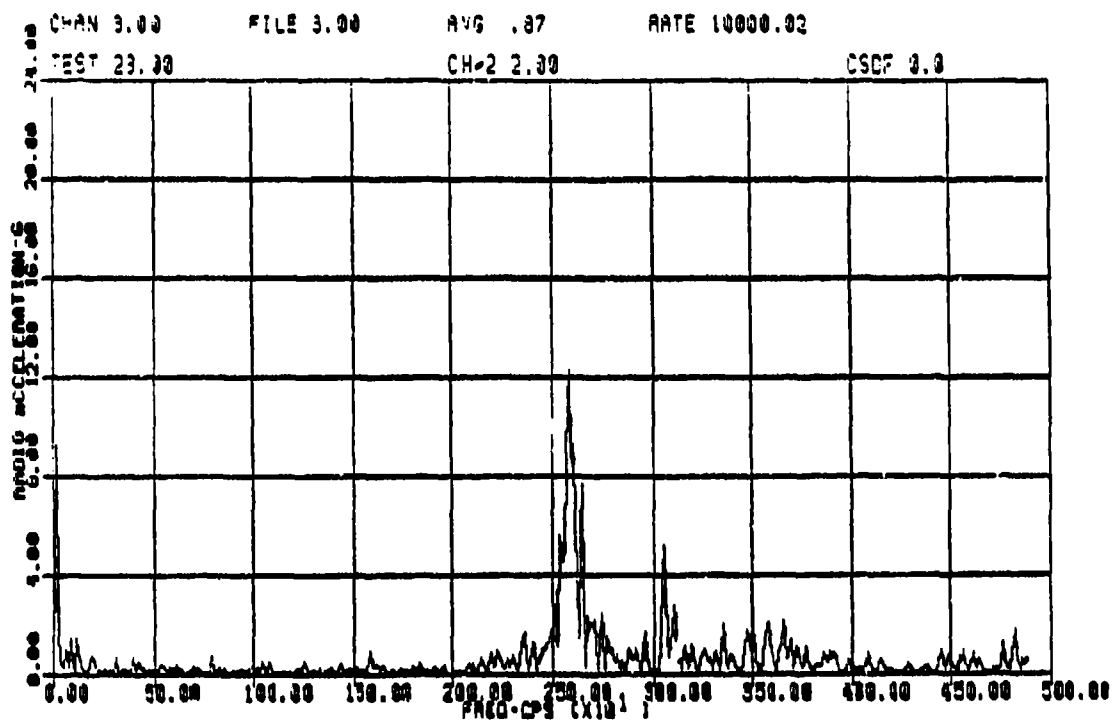


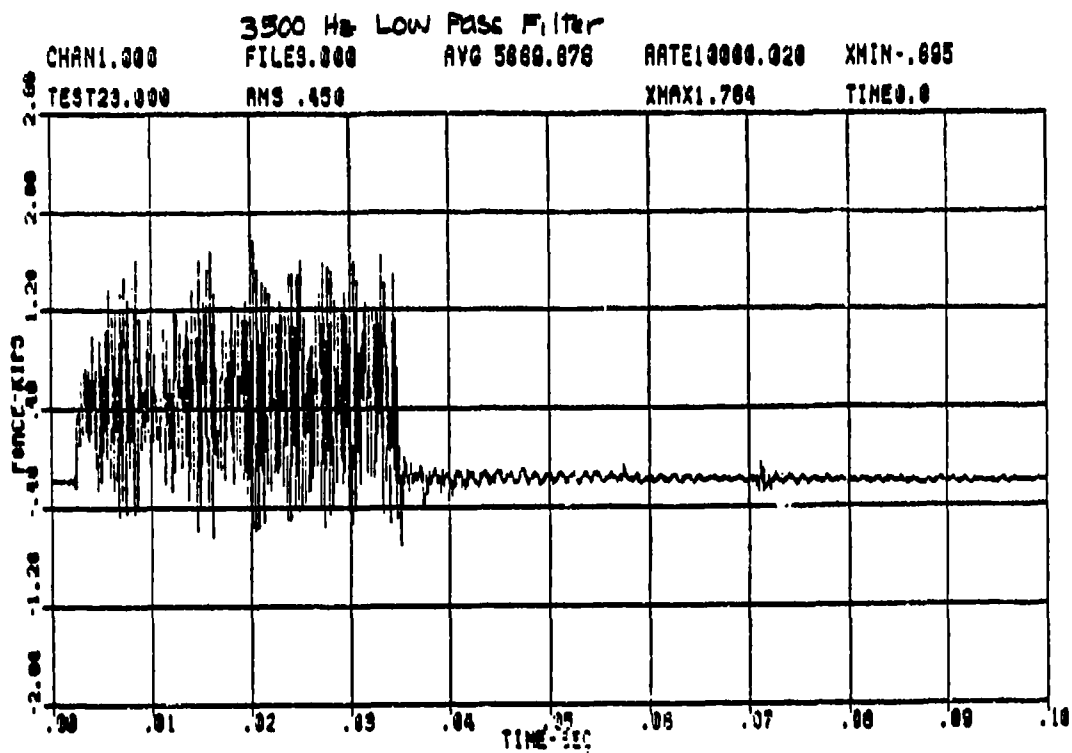
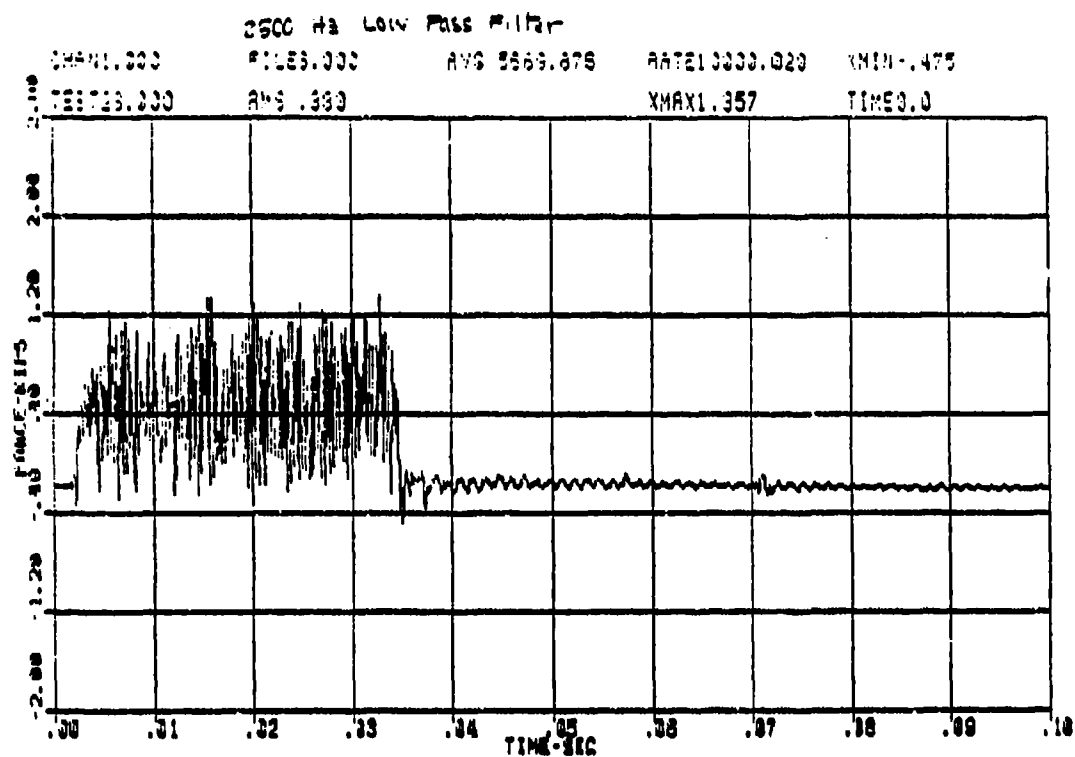




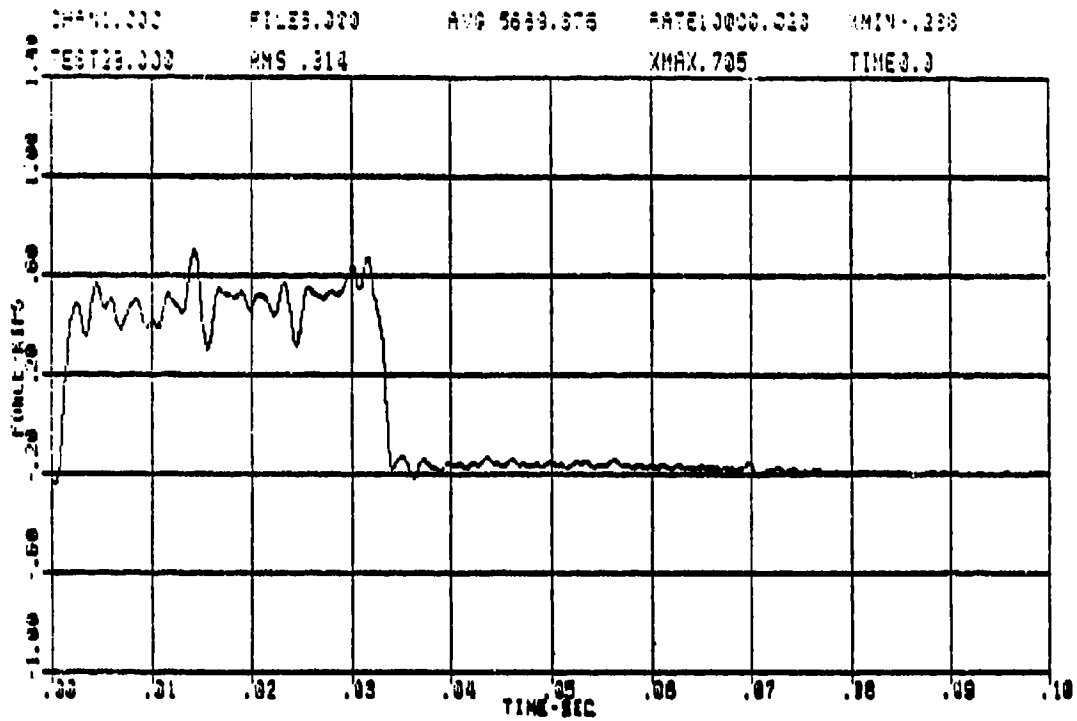




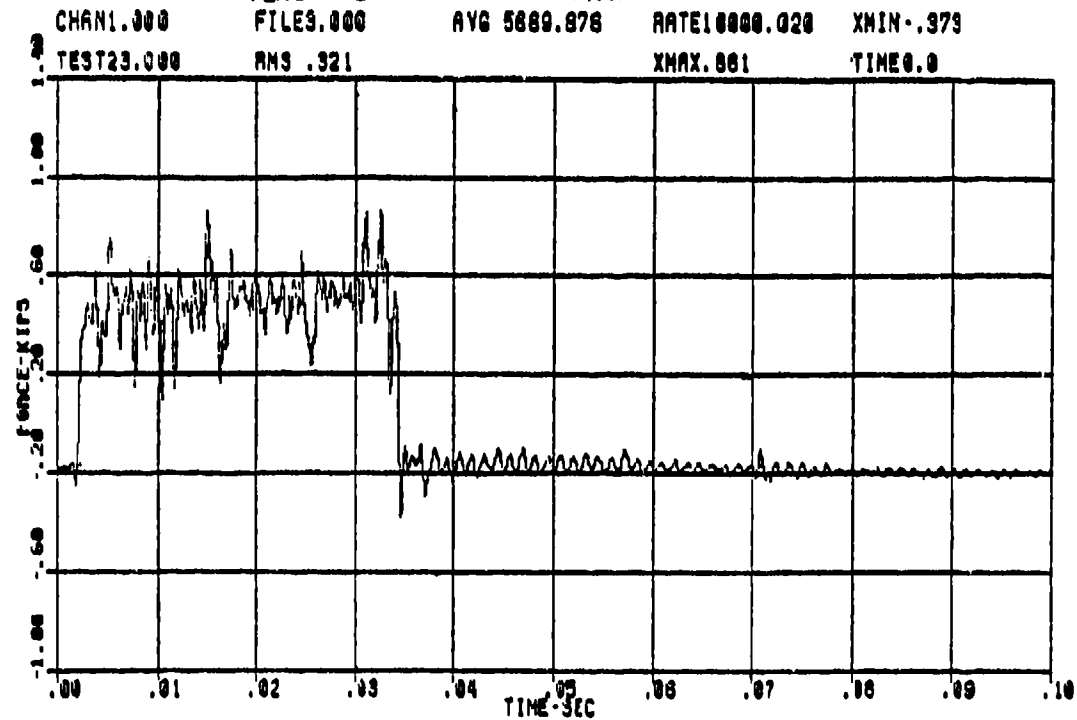


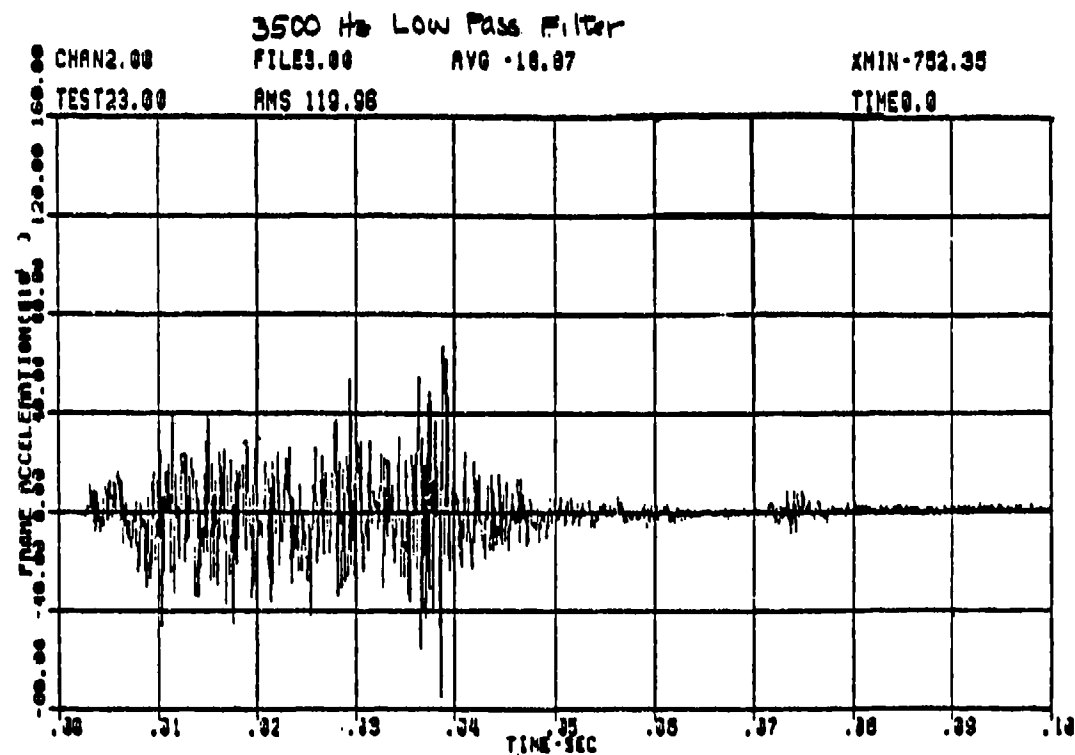
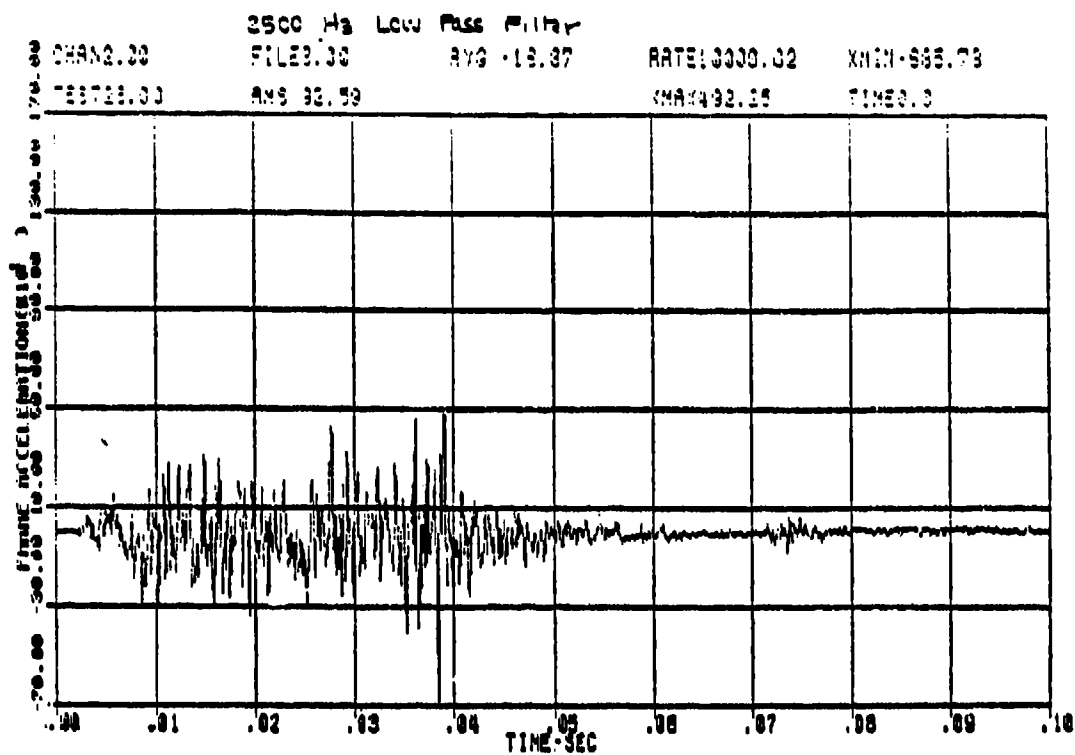


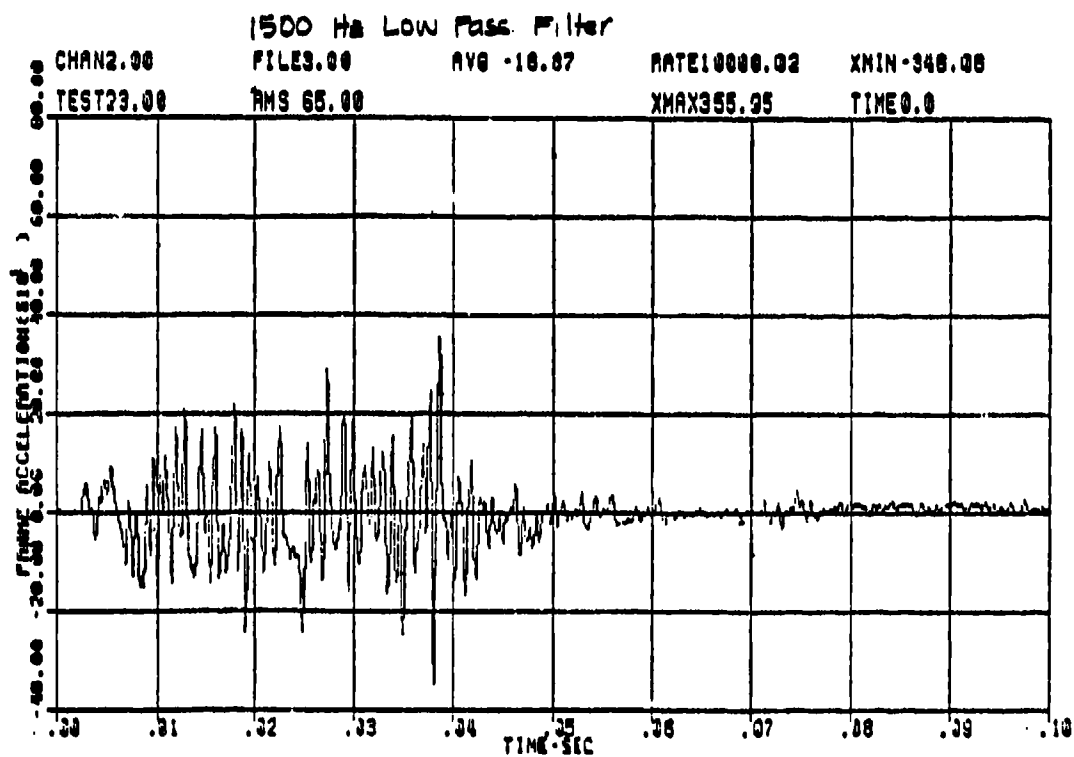
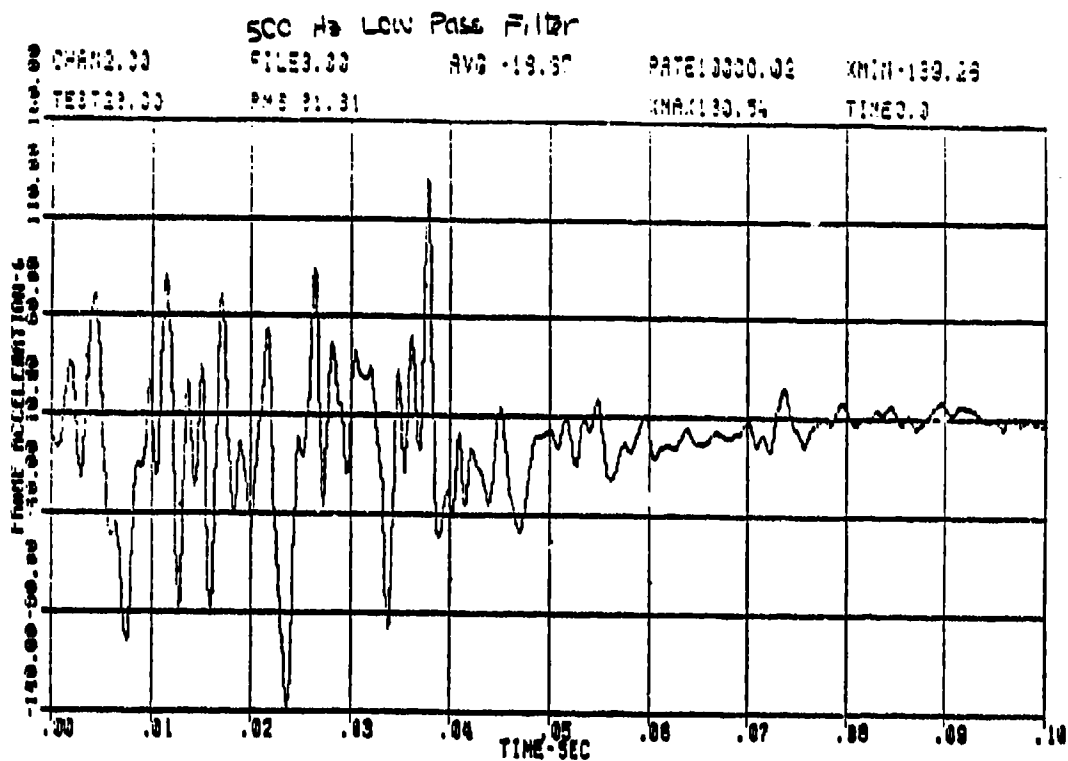
500 Hz Low Pass Filter

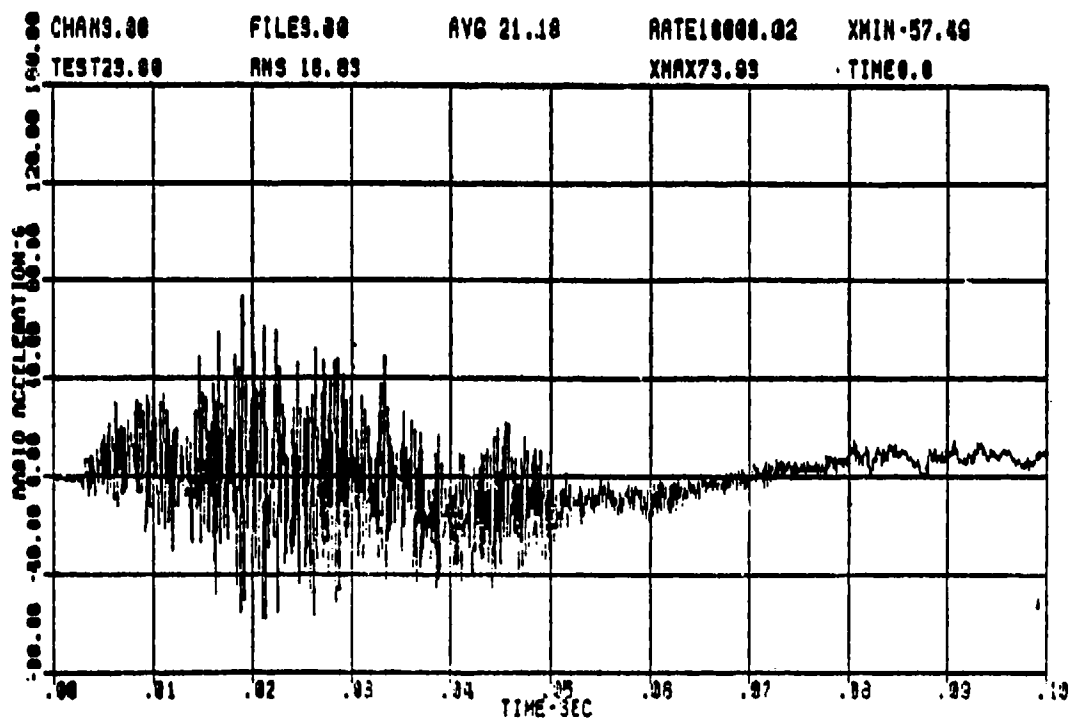
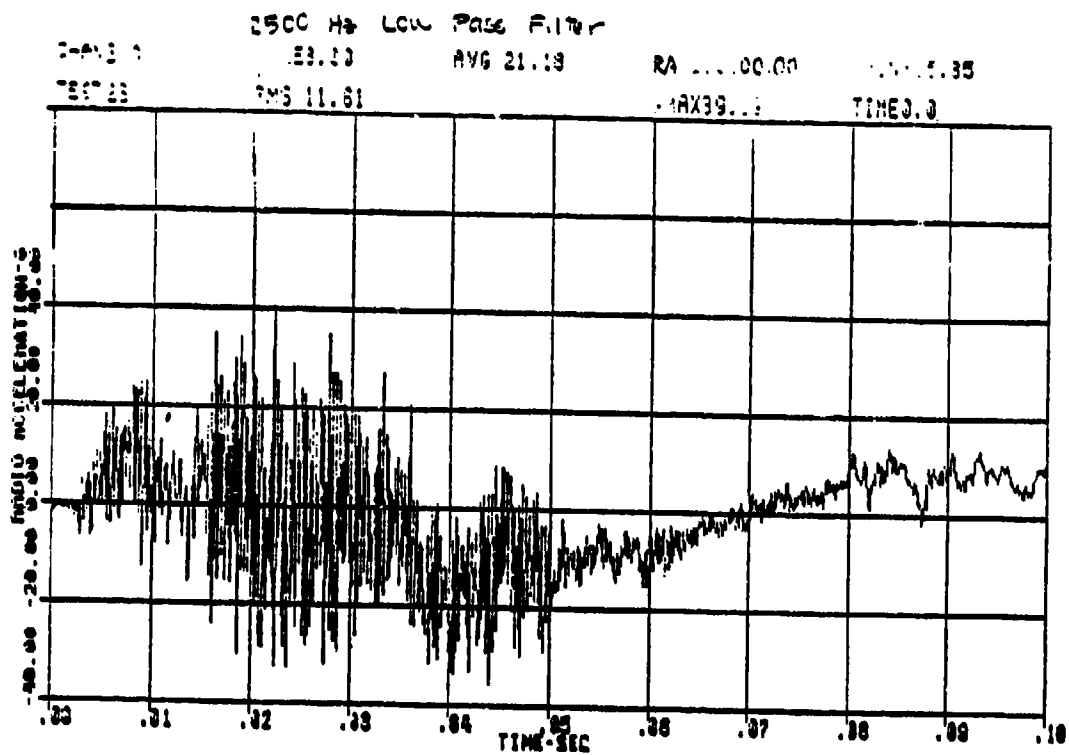


1500 Hz Low-Pass Filter

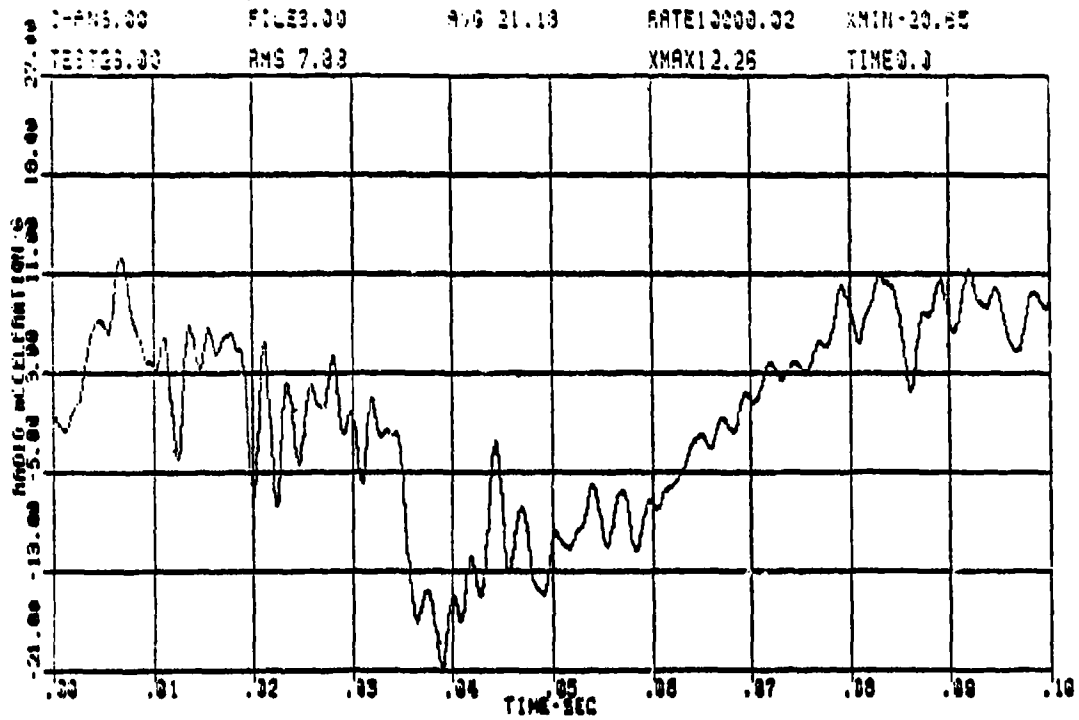




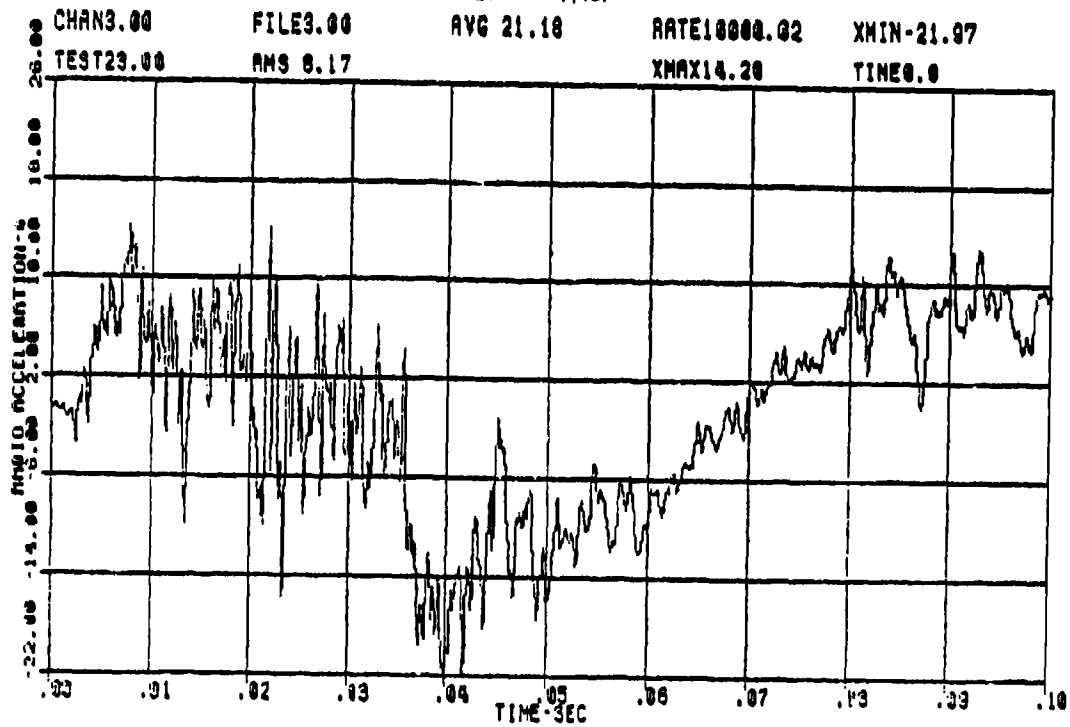




500 Hz Low Pass Filter

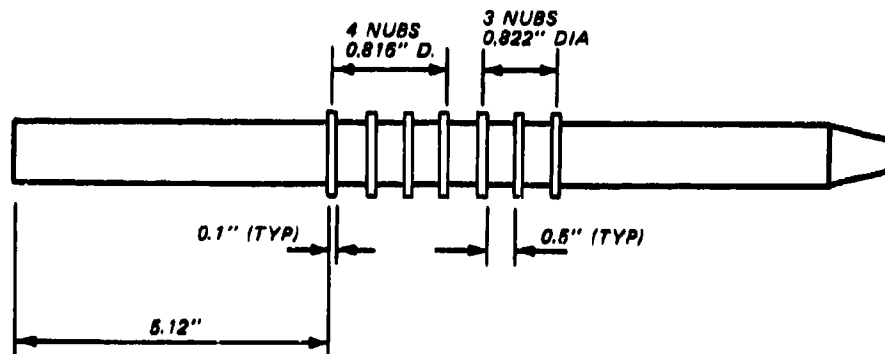


1500 Hz Low Pass Filter



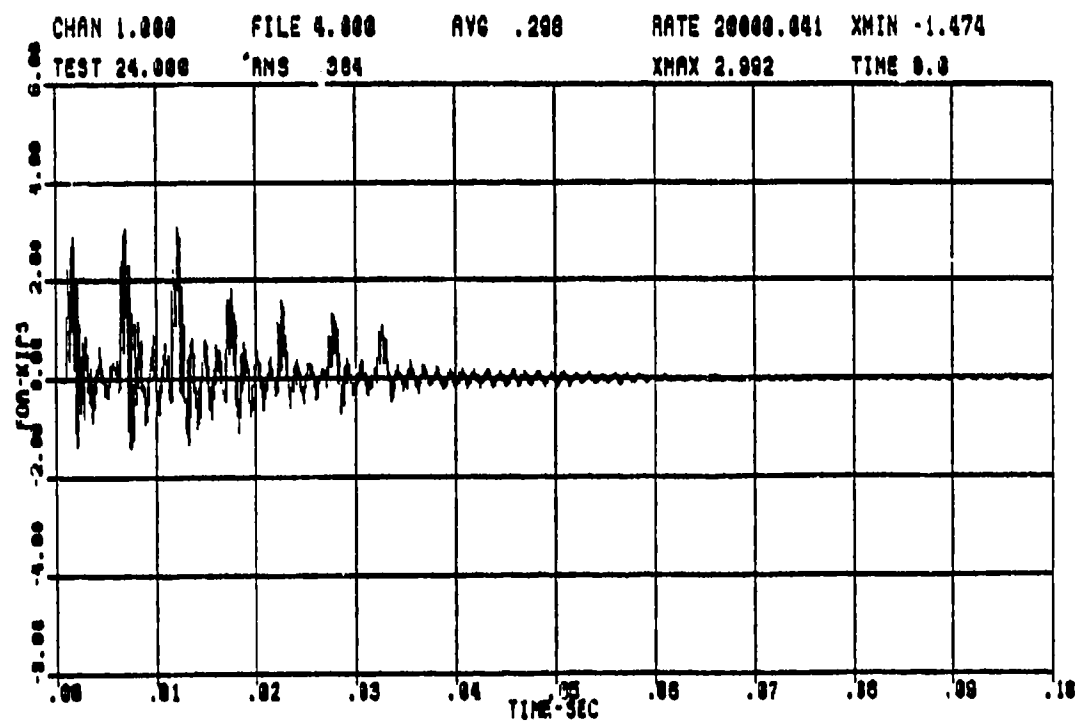
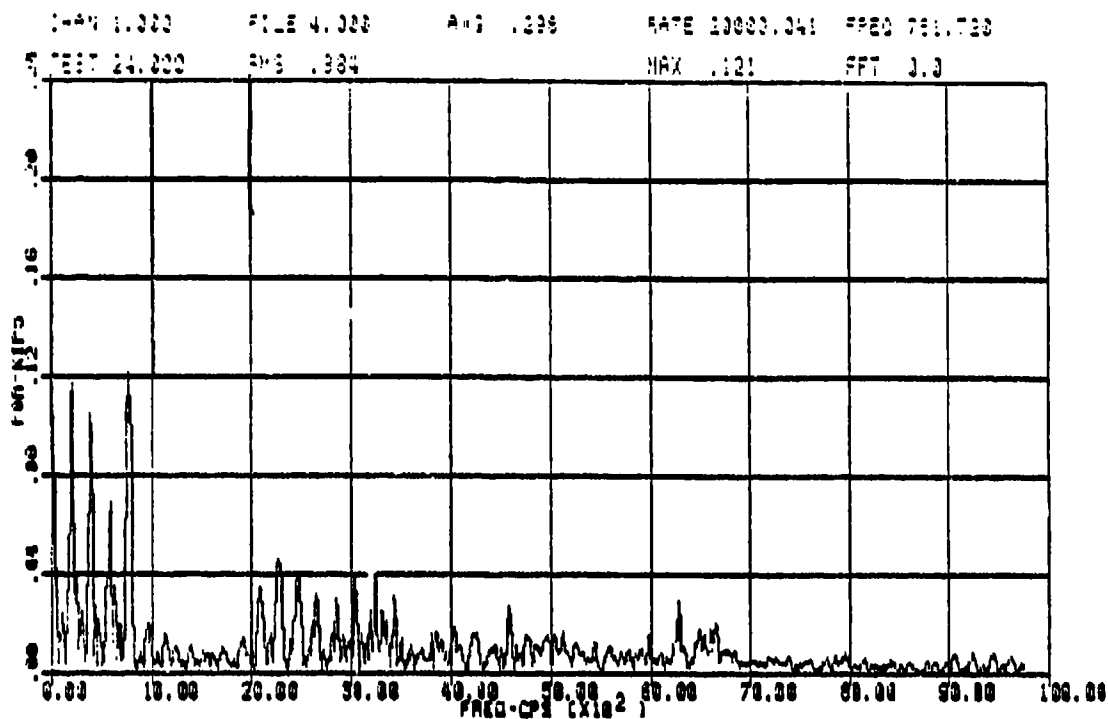
APPENDIX J: TEST 24 RESULTS

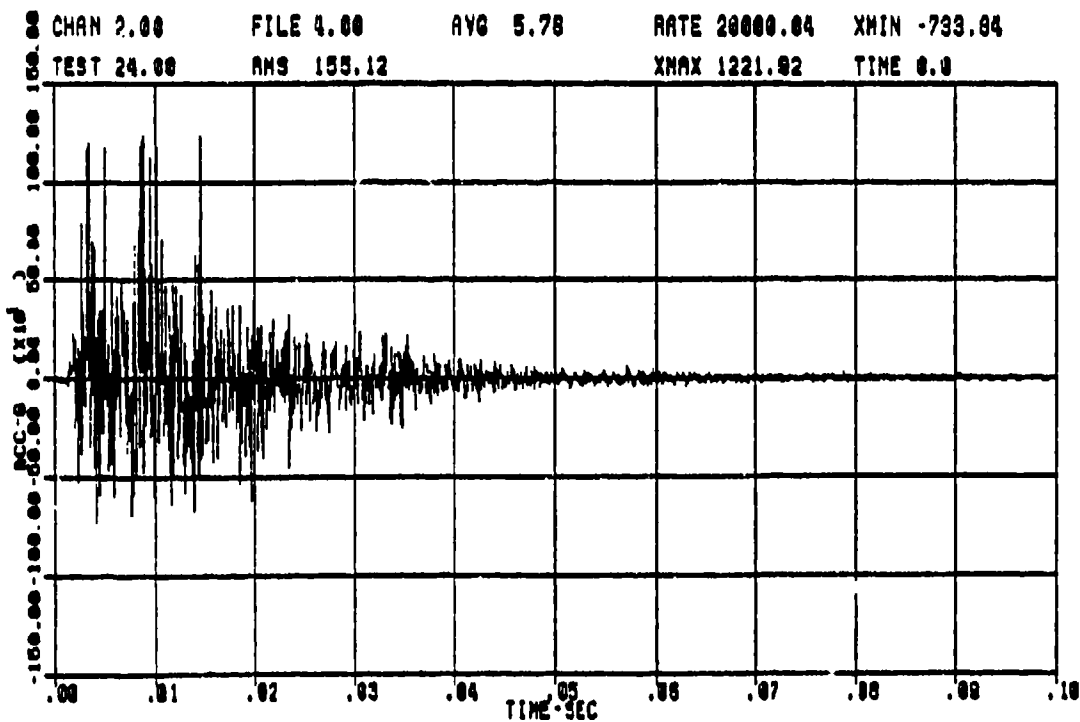
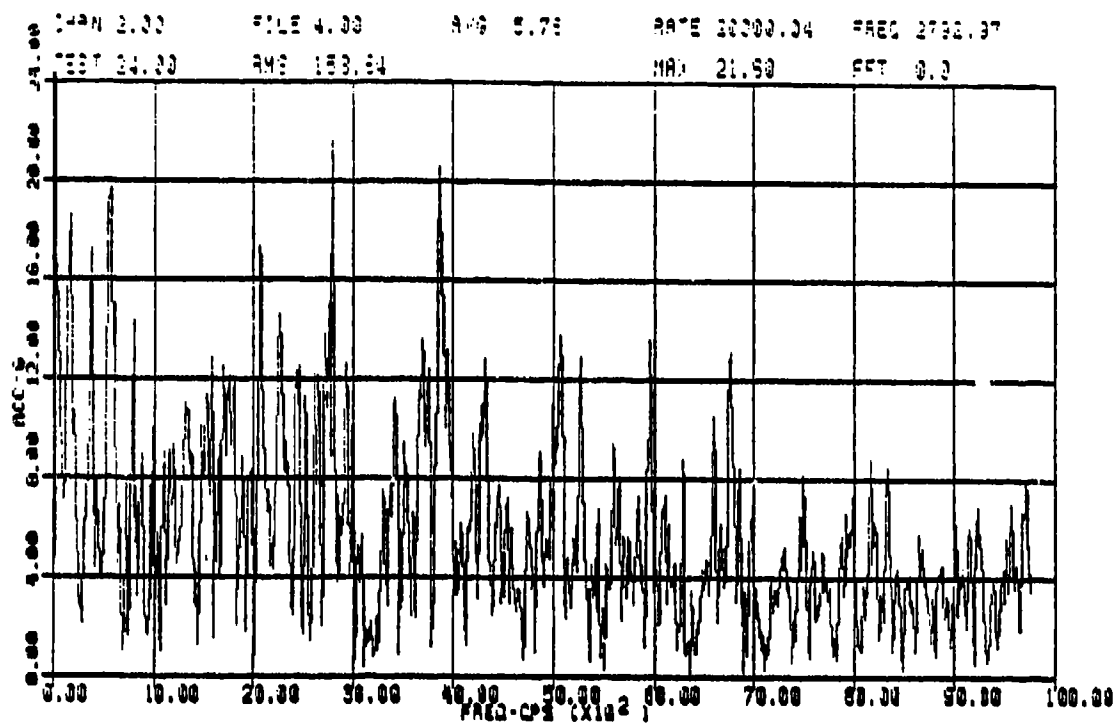
Test 24
Equipment Rack Soft-Mounted
AN/GRC-103 in Rack, Off-Line

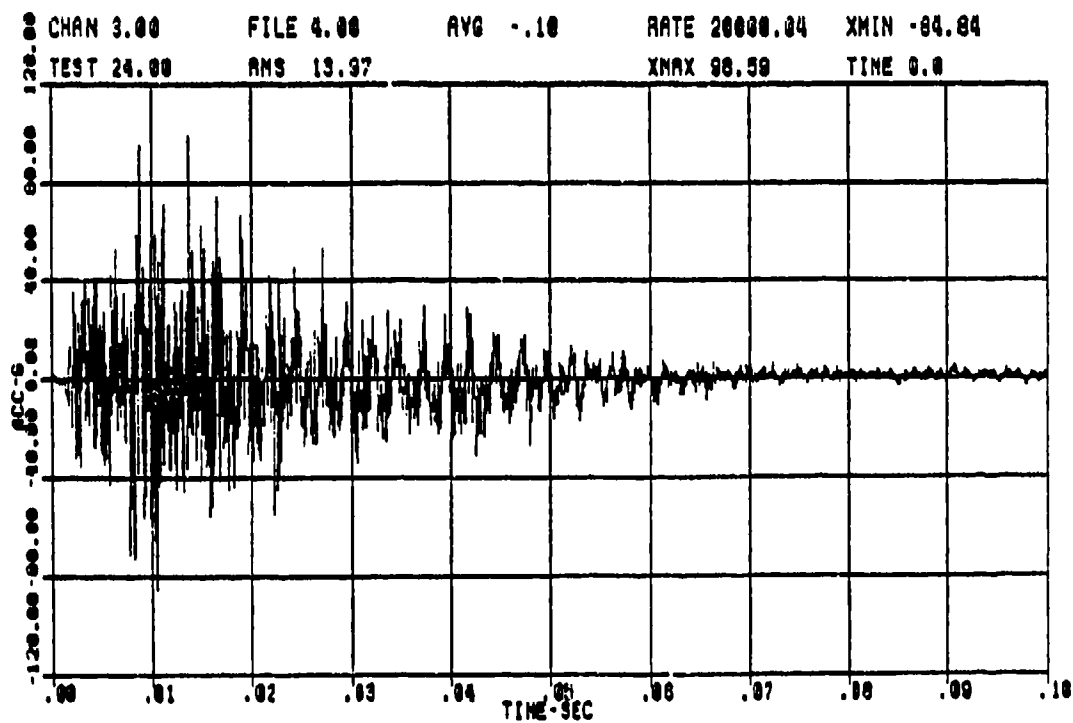
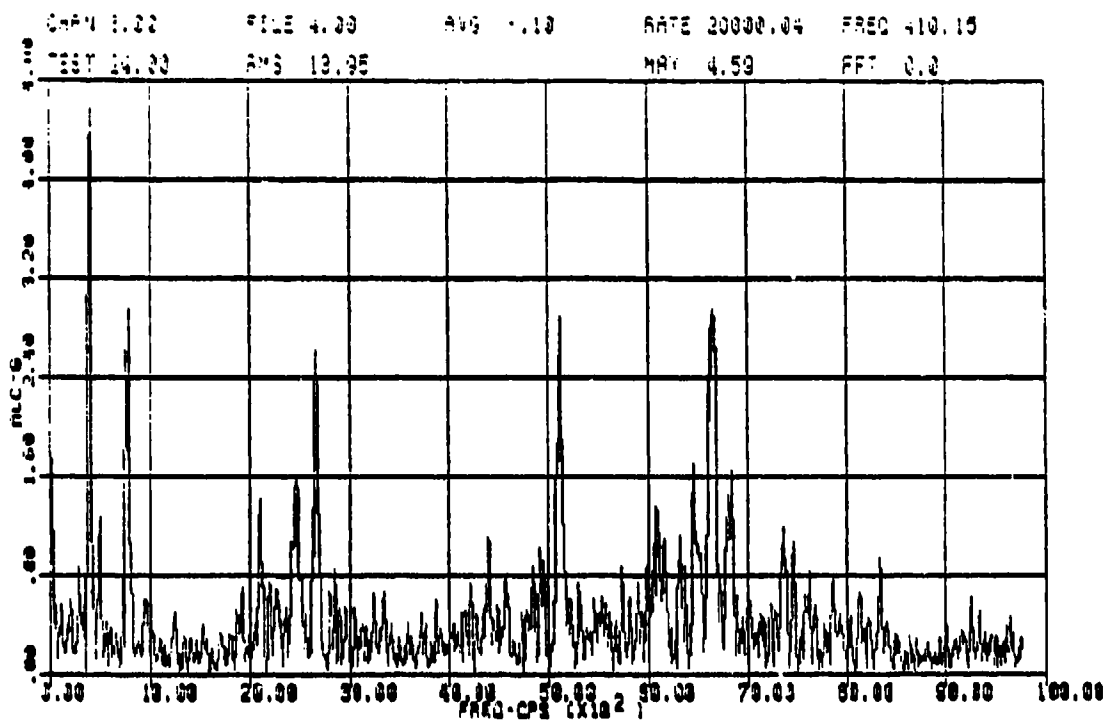


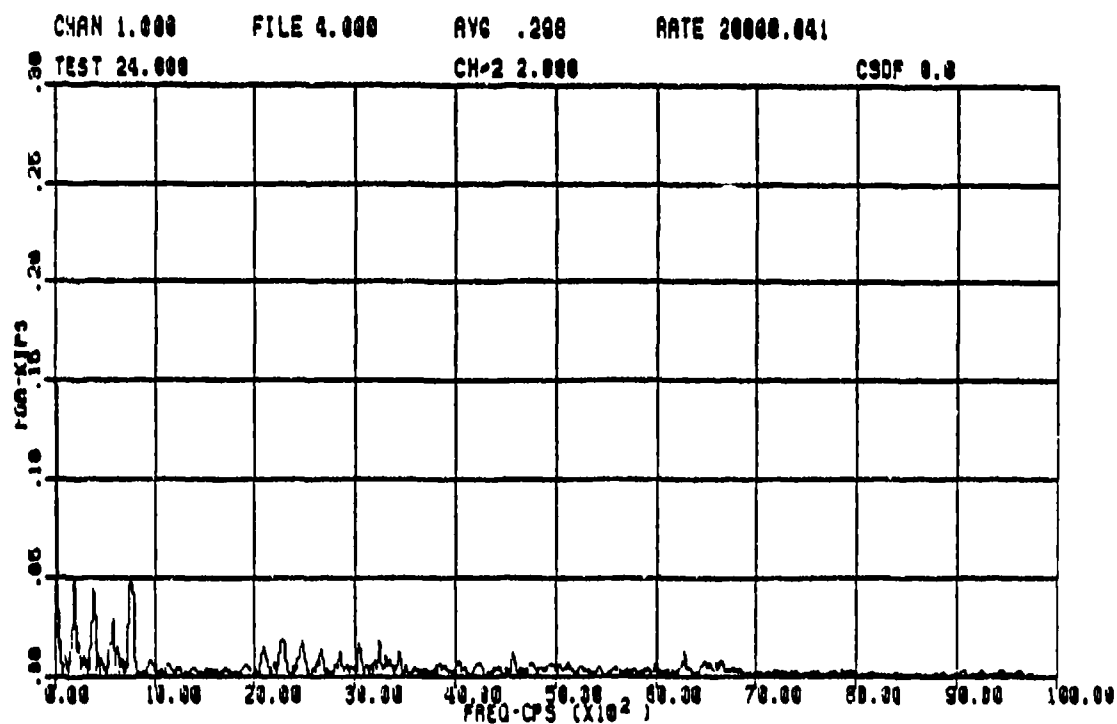
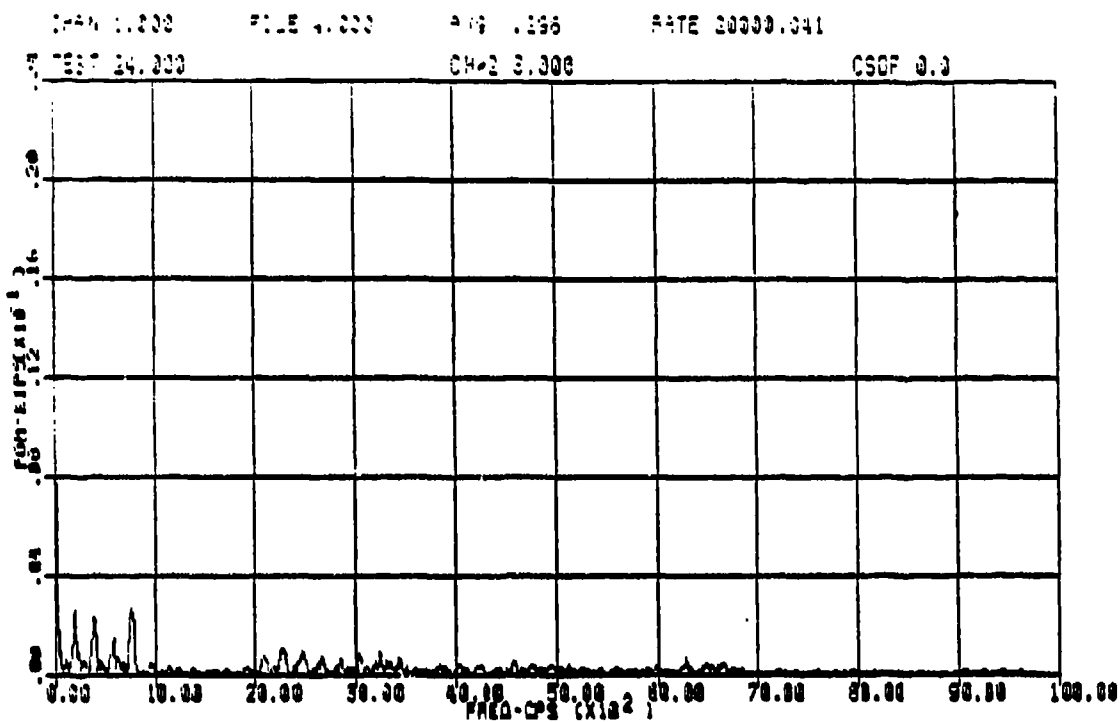
PULSE TRAIN - TEST 24

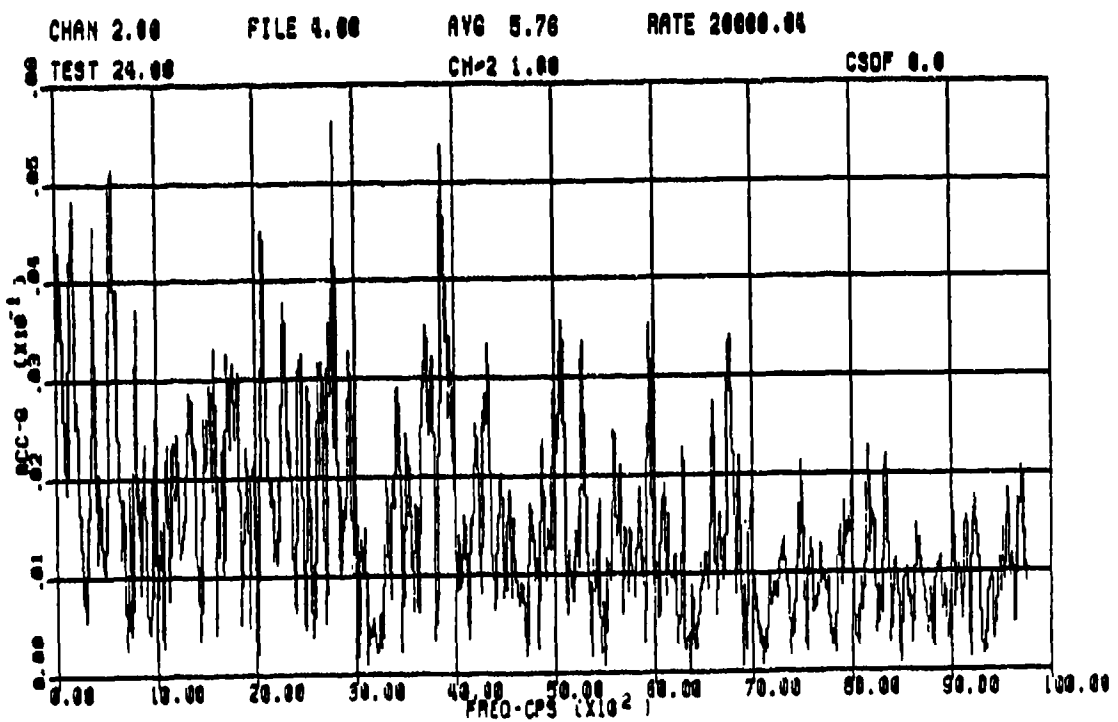
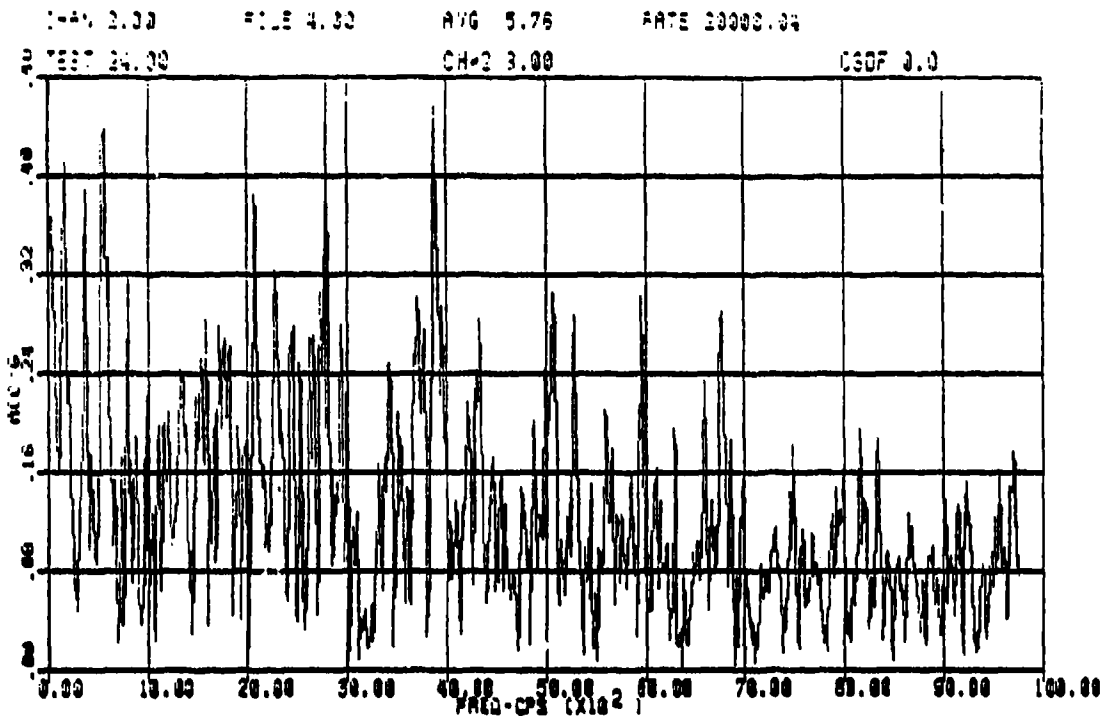
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #6%
AIR BAG PRESSURE = 70 PSI

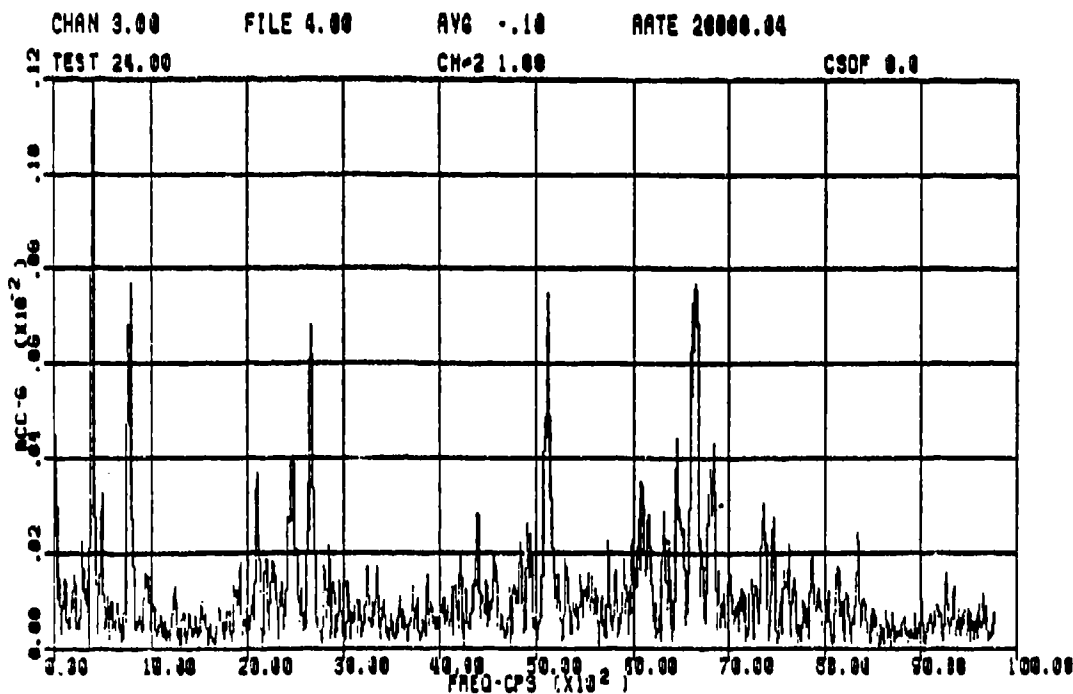
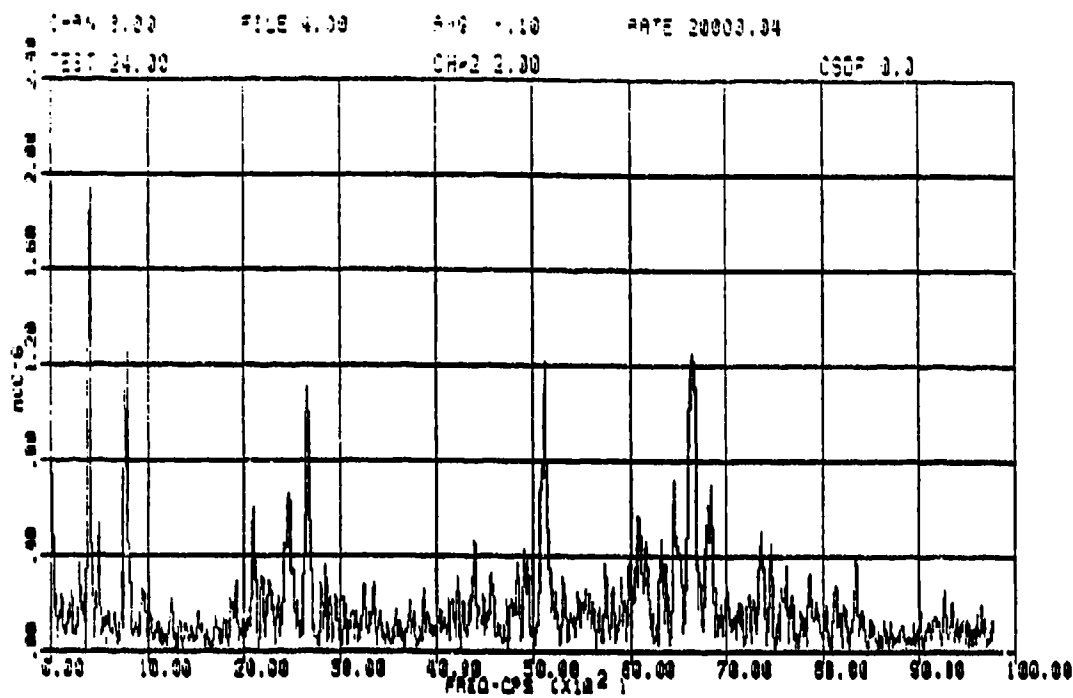


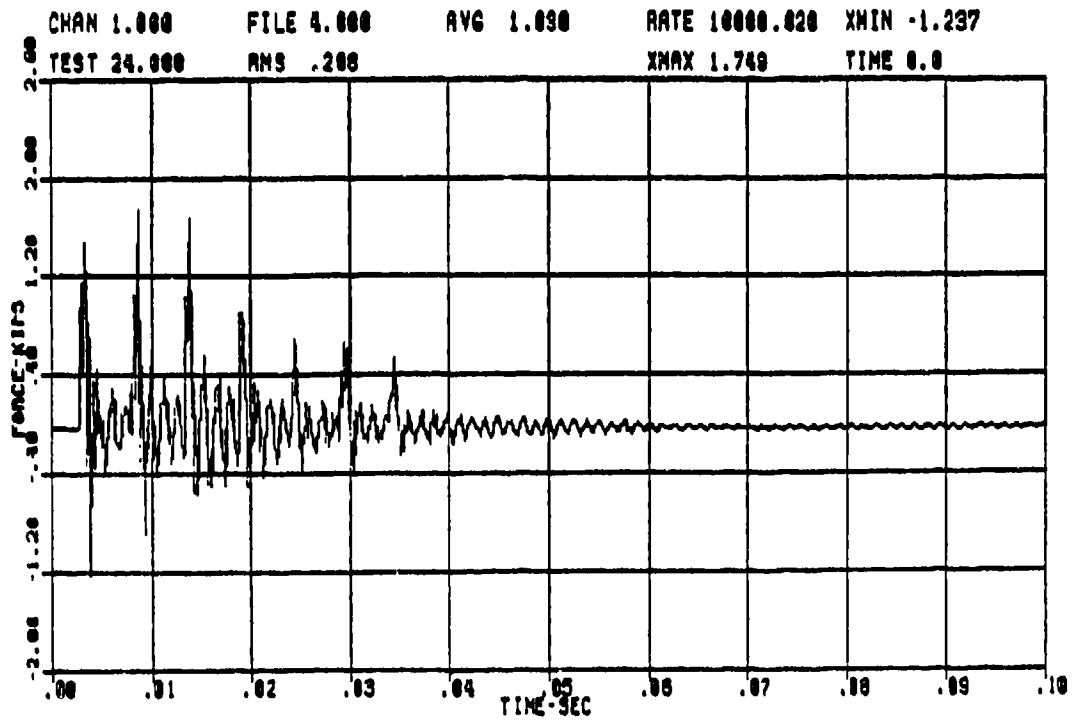
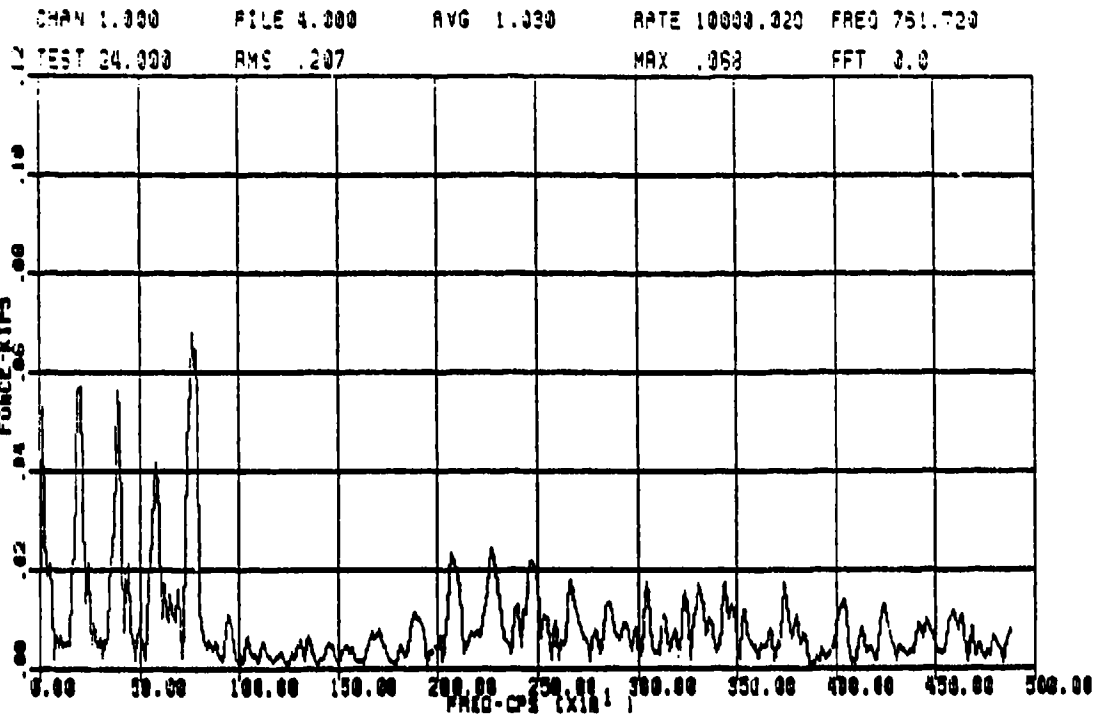


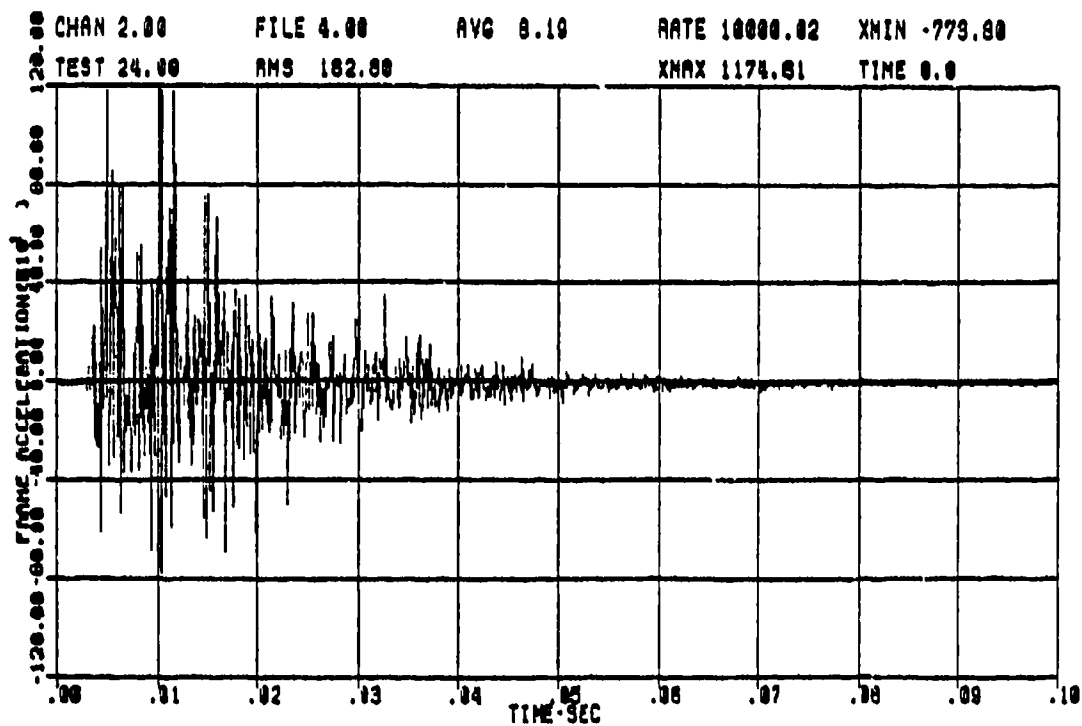
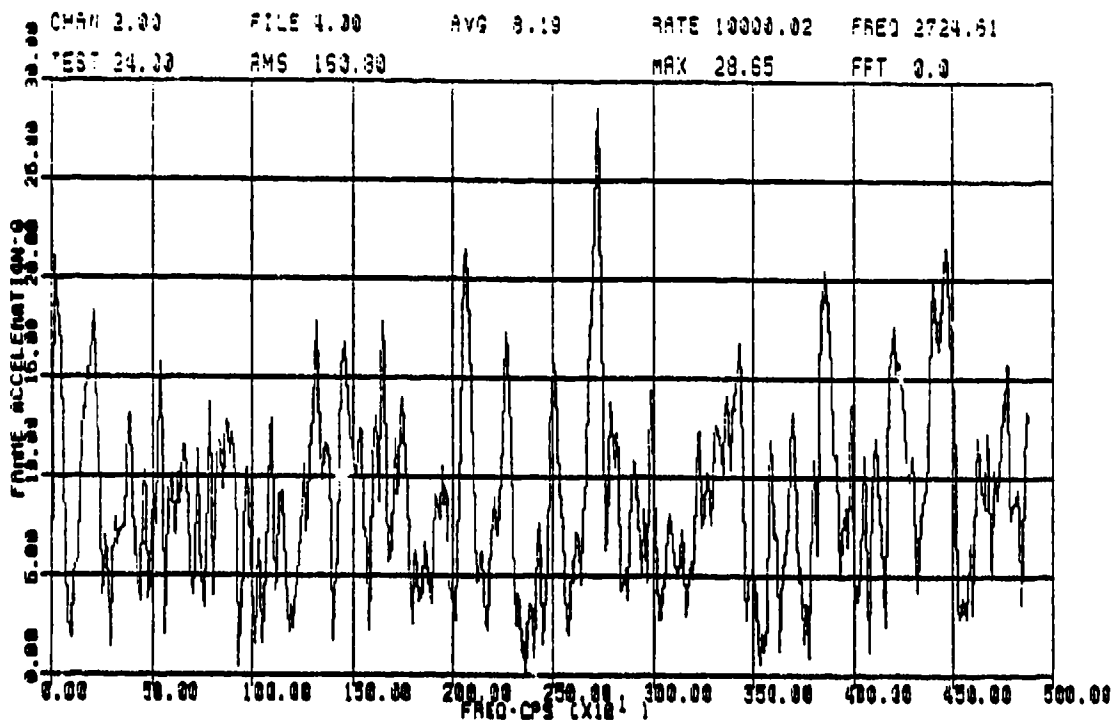


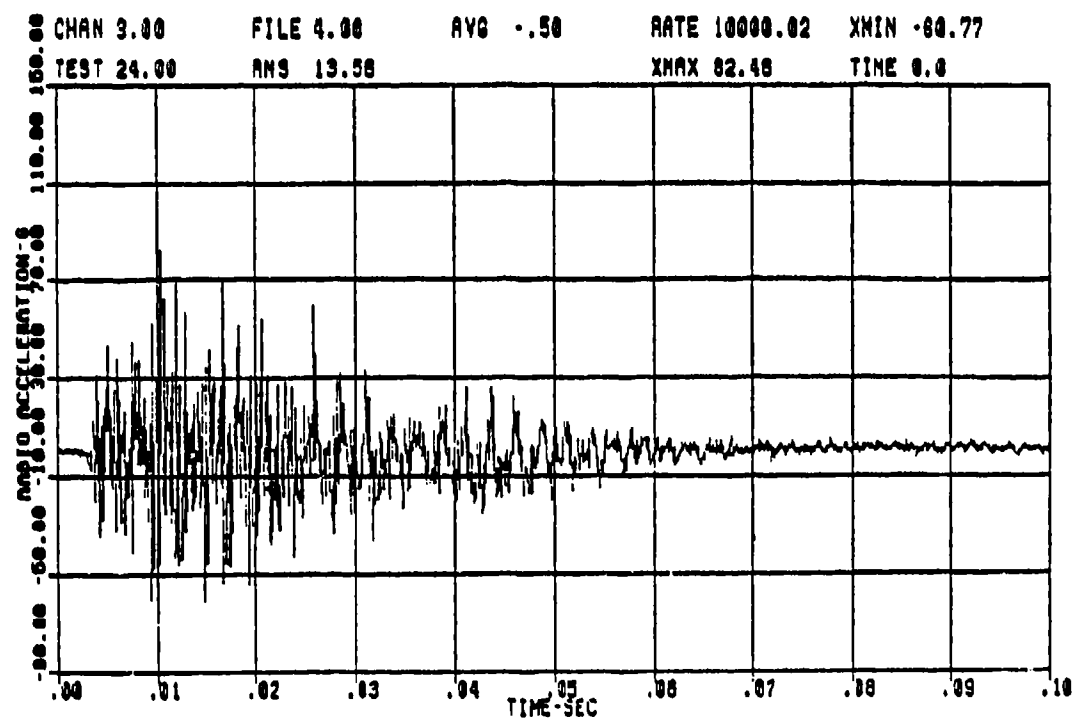
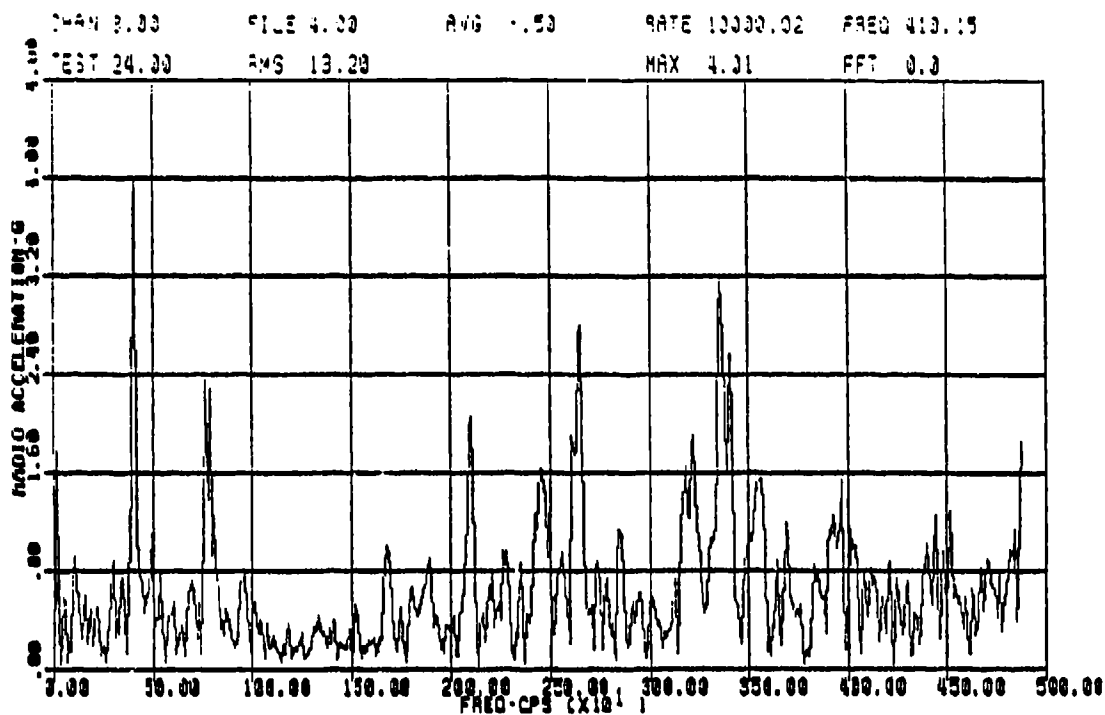


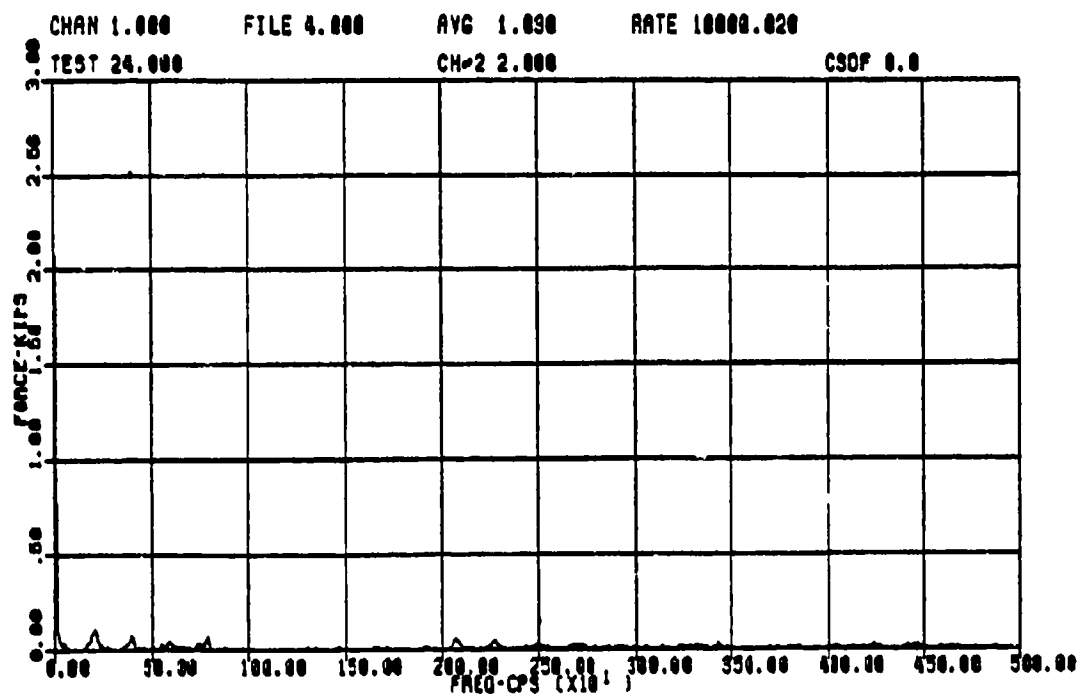
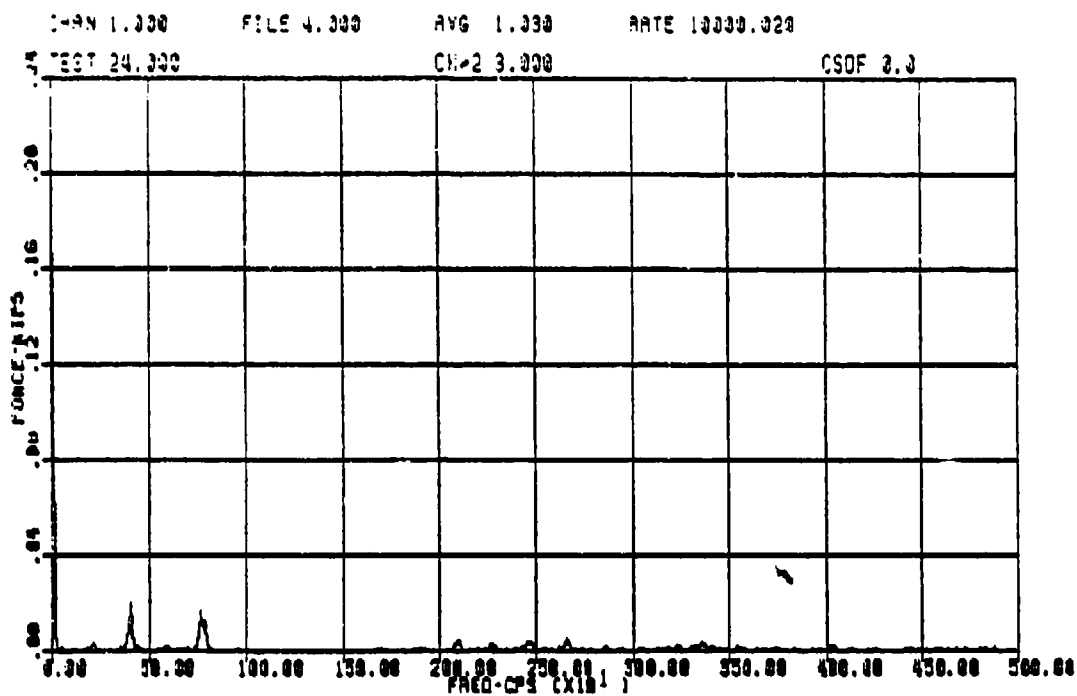


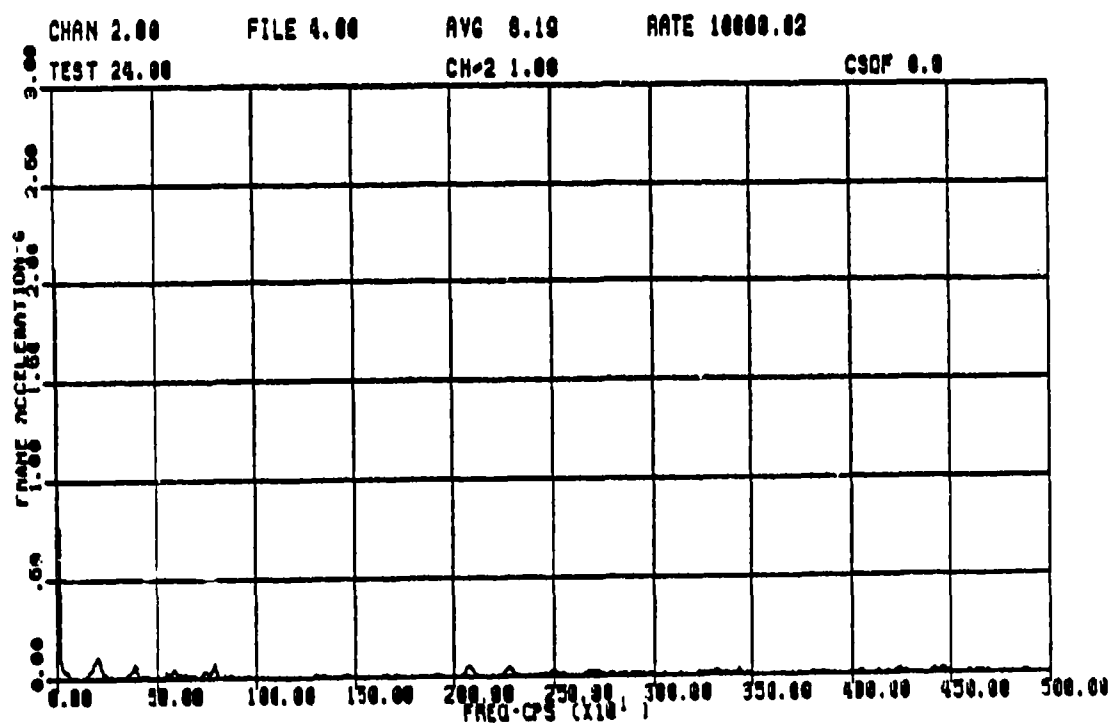
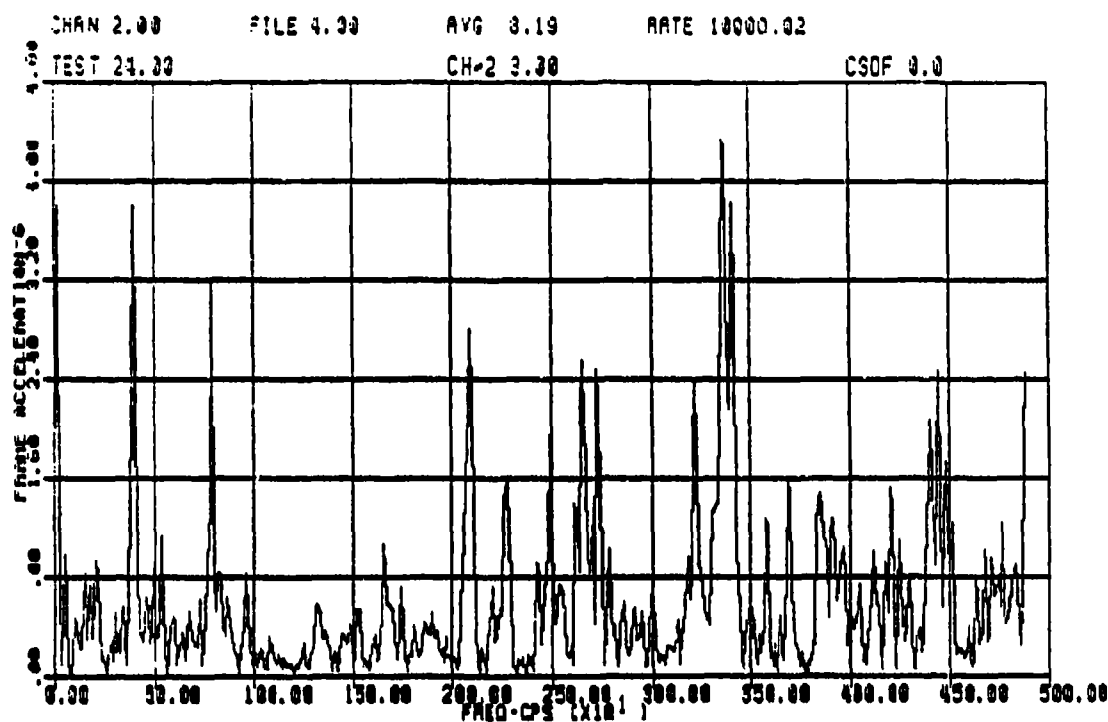


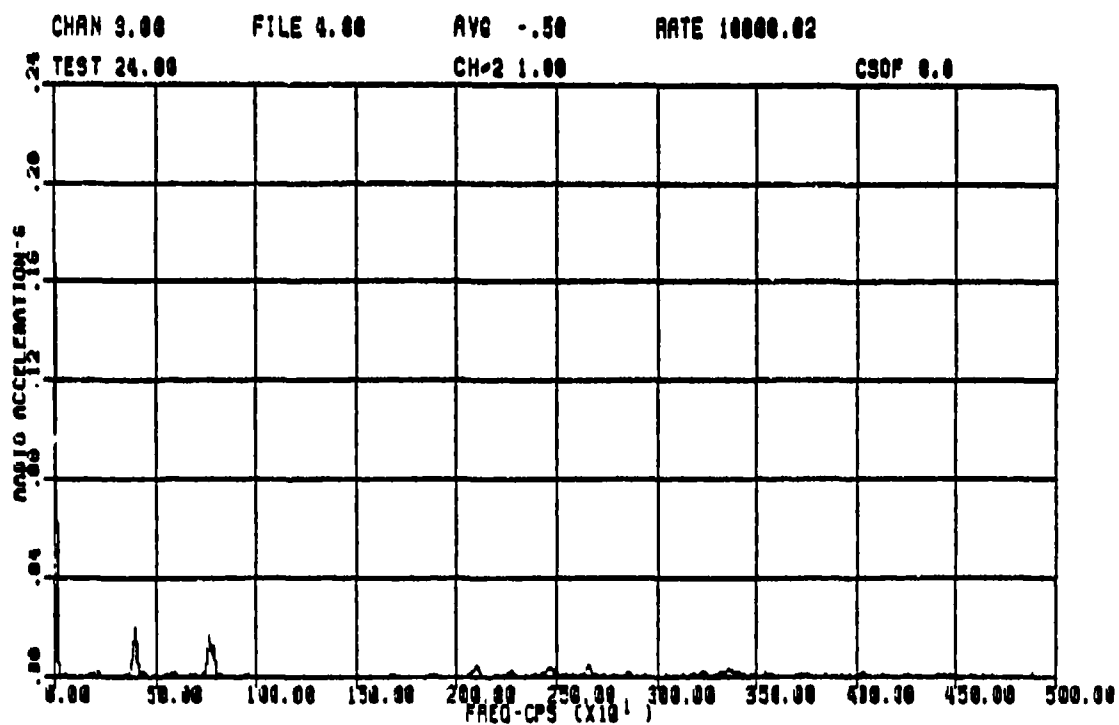
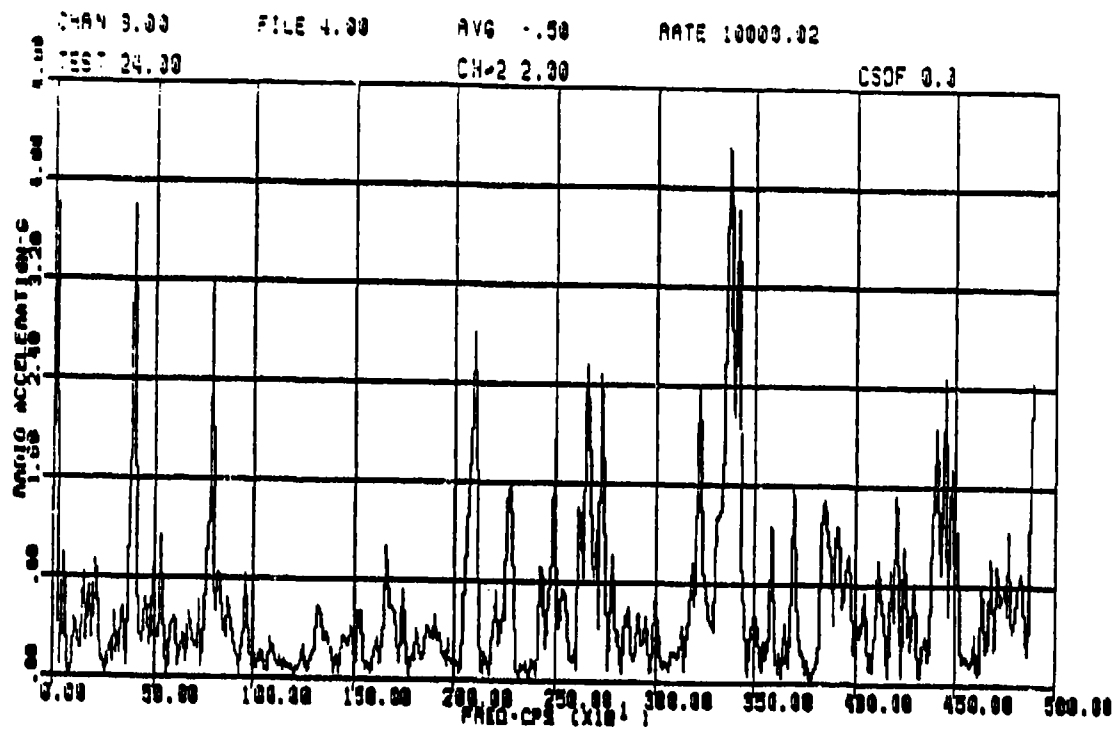




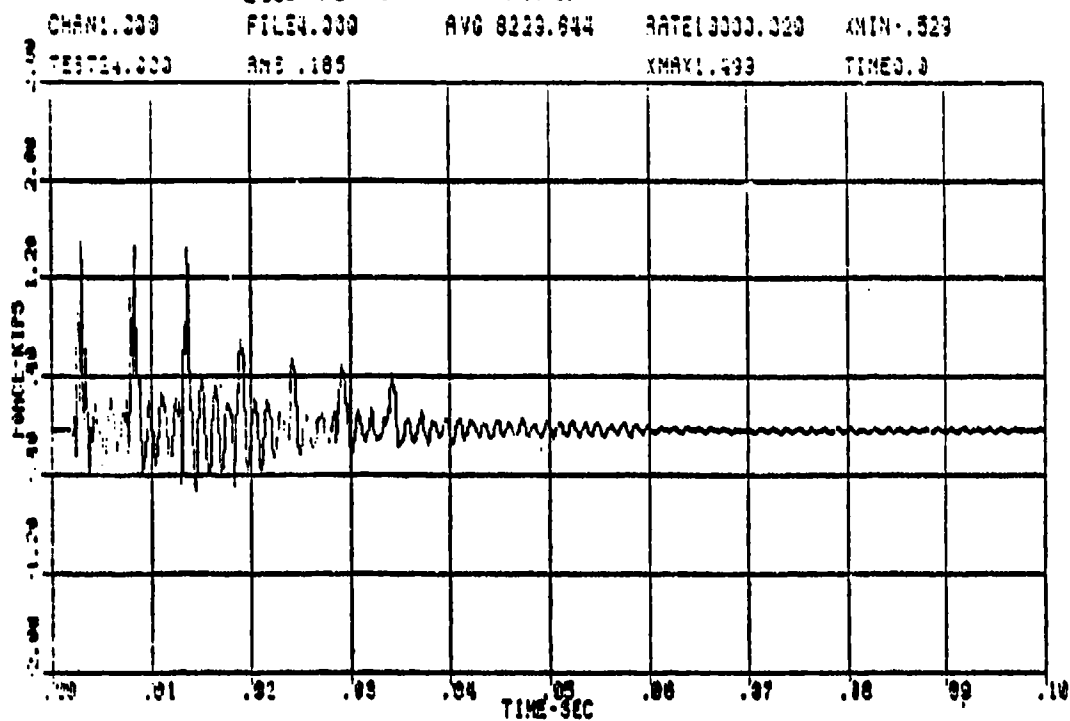




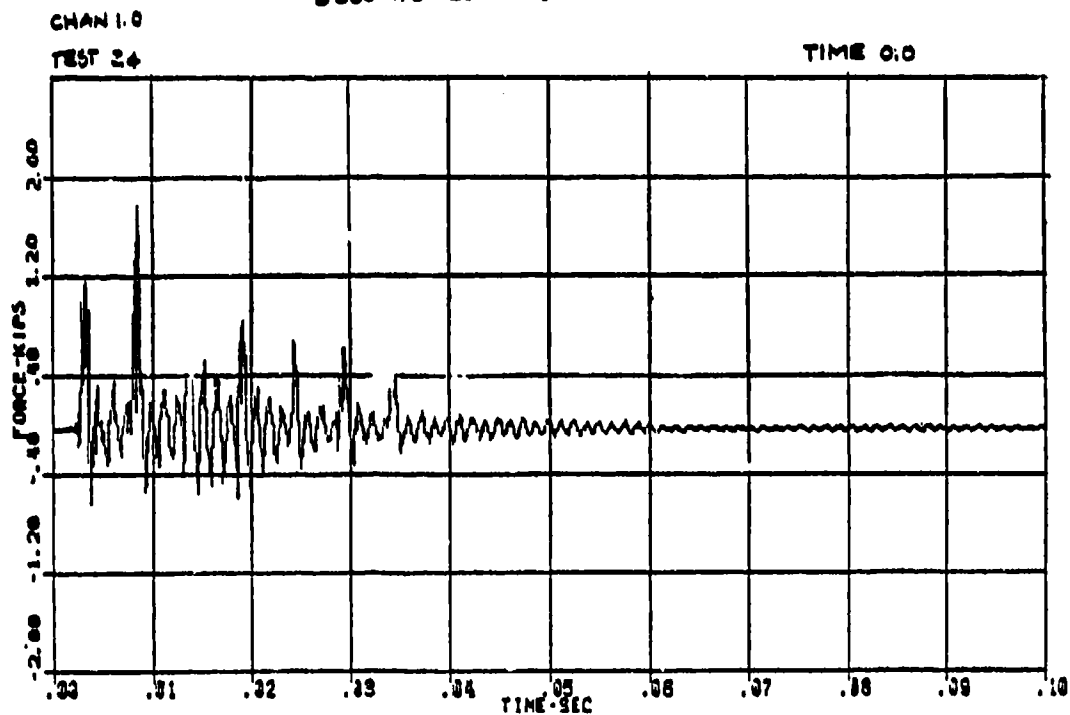




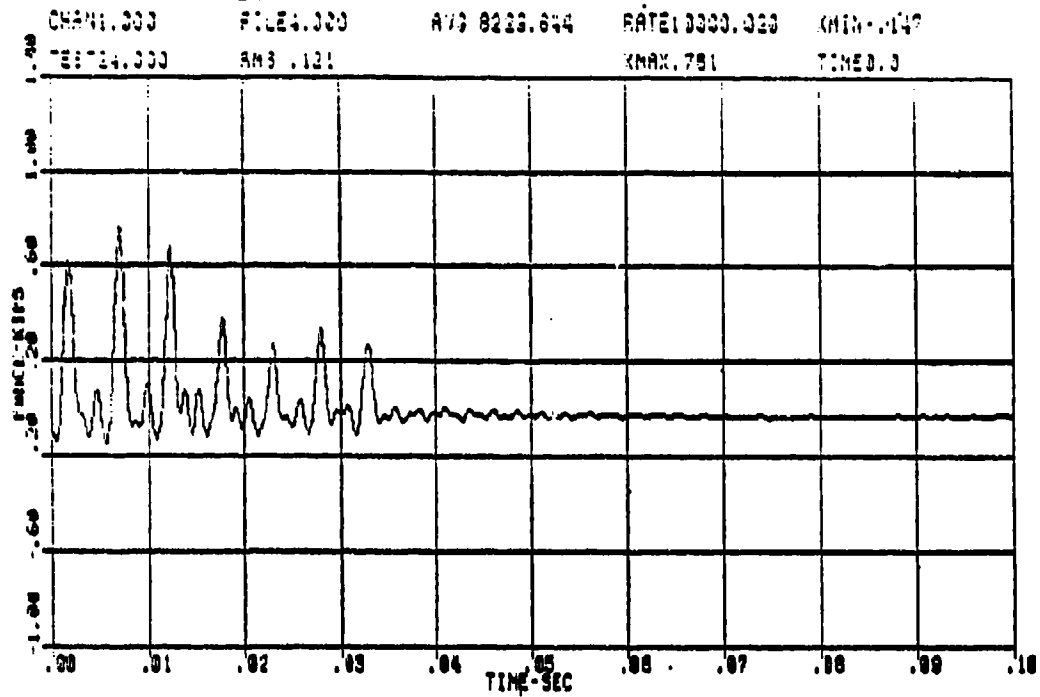
2500 Hz Low Pass Filter



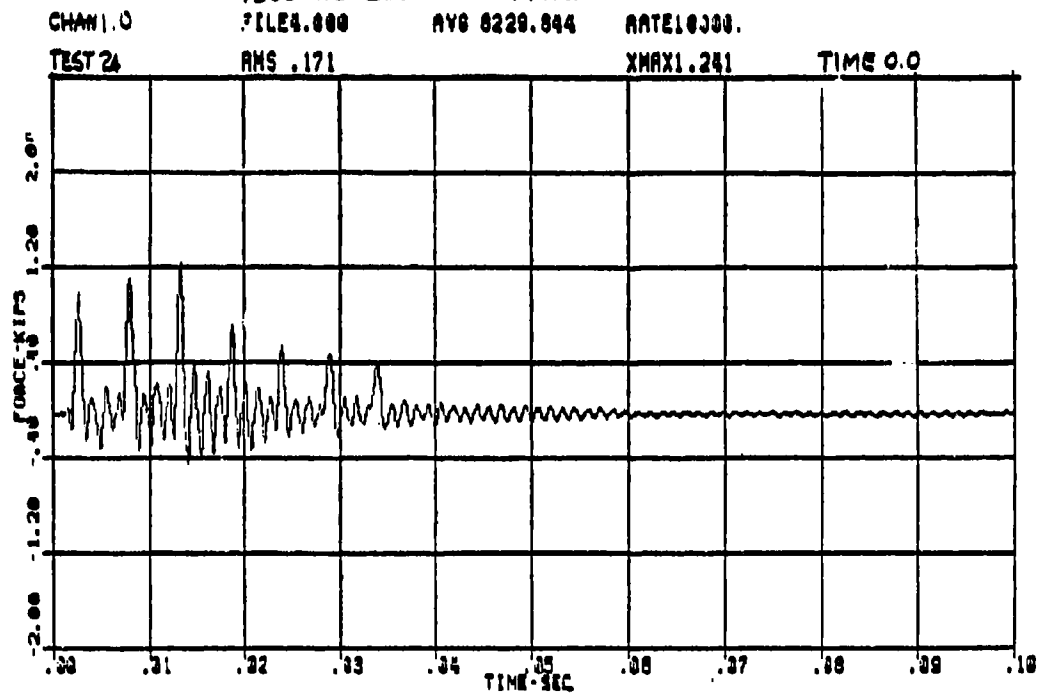
3500 Hz Low Pass Filter

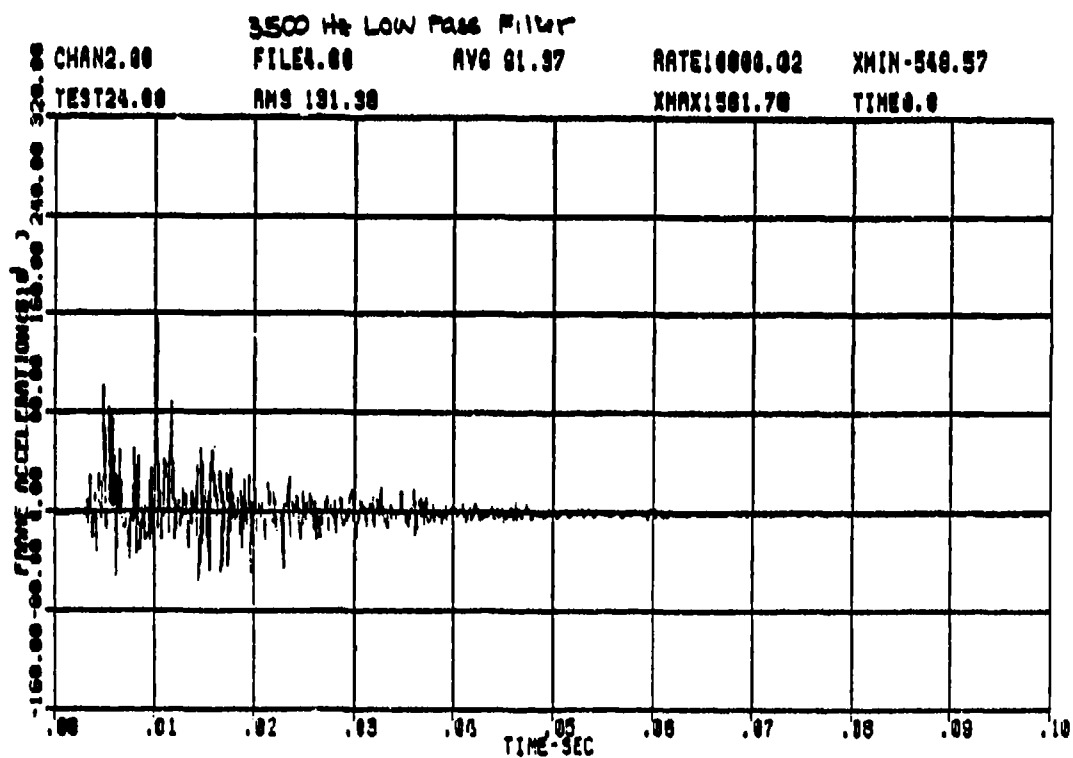
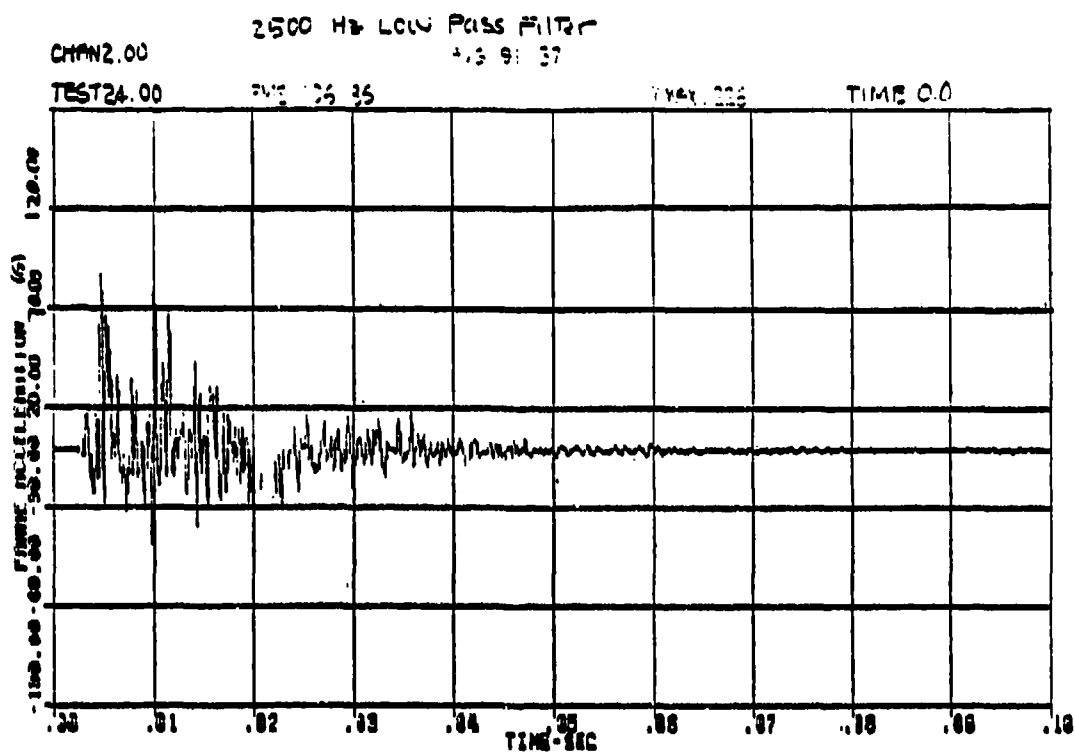


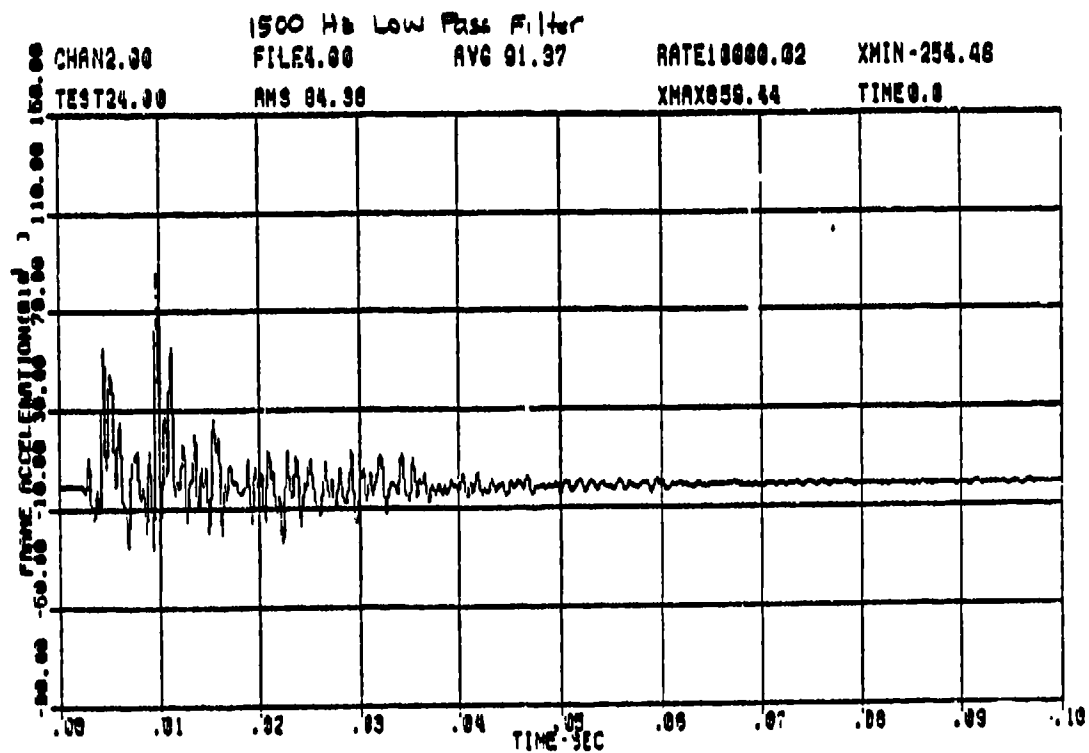
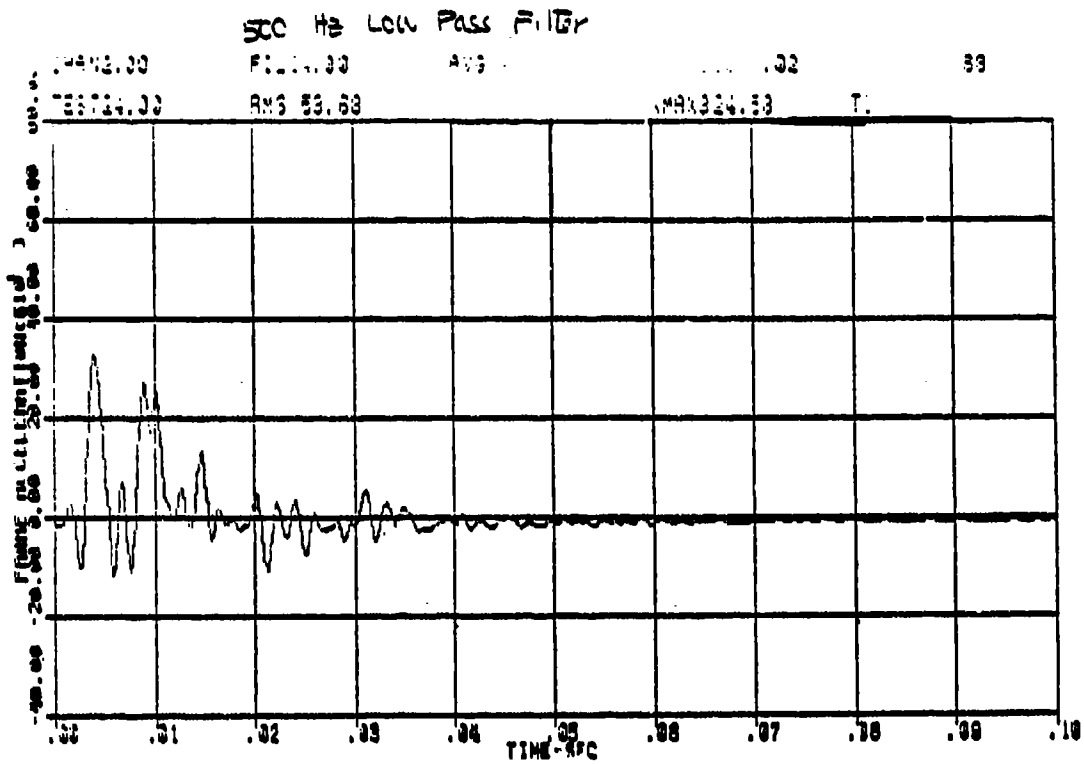
500 Hz Low Pass Filter

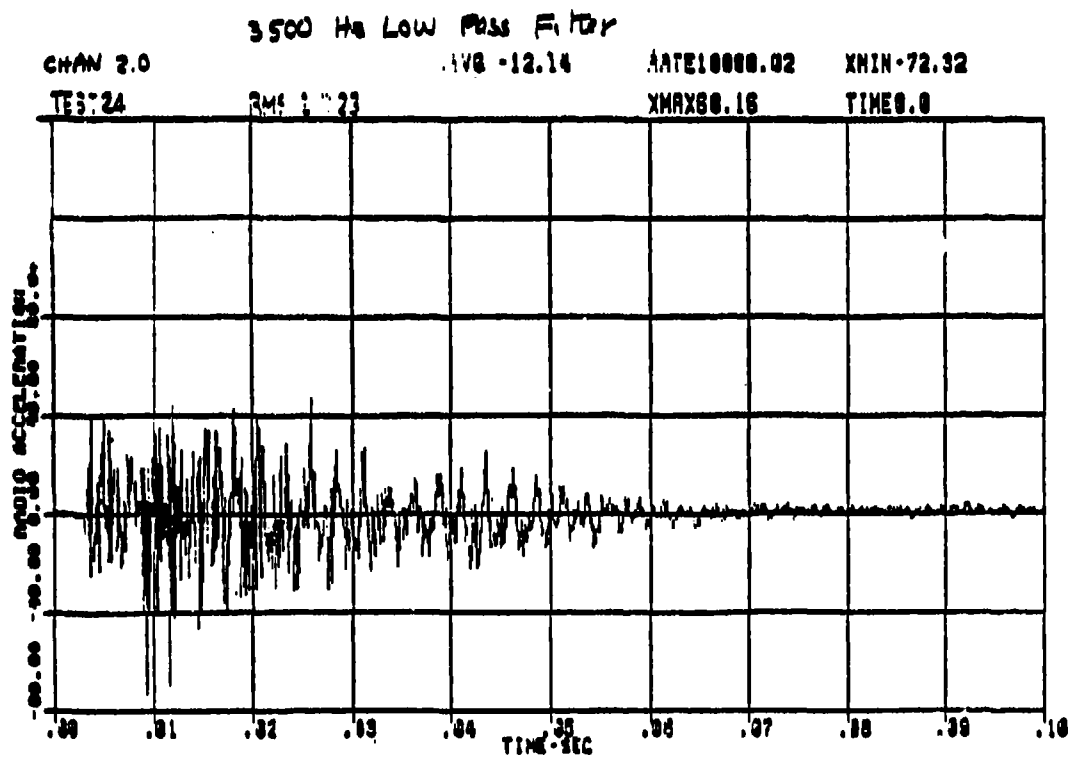
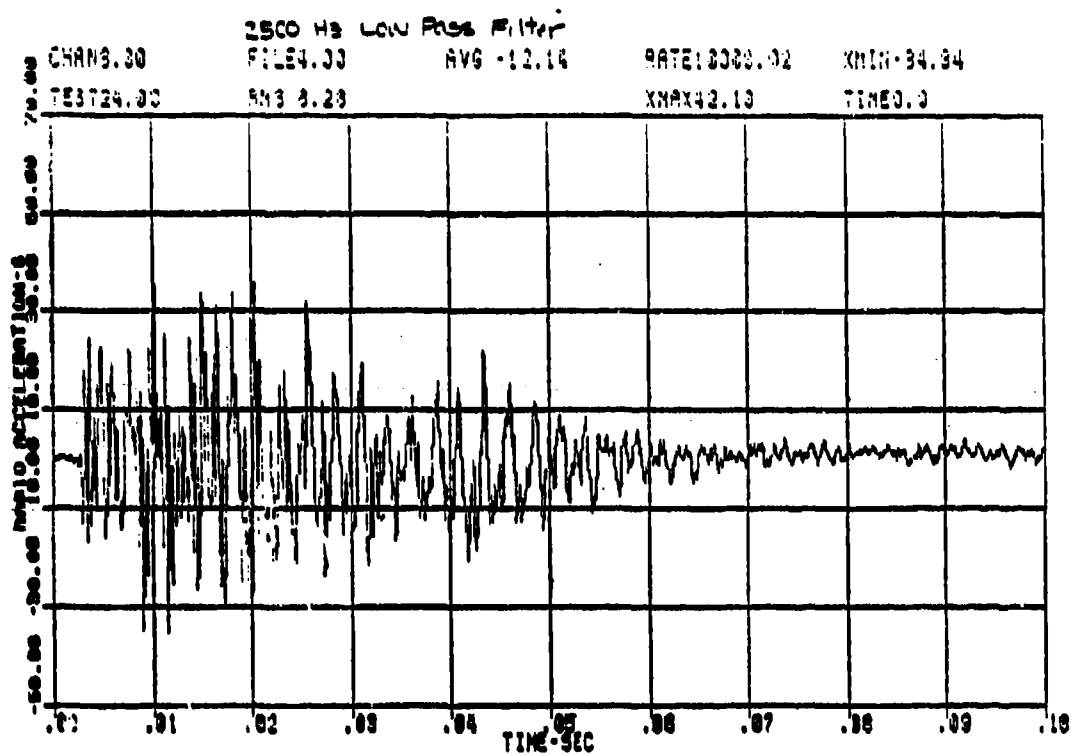


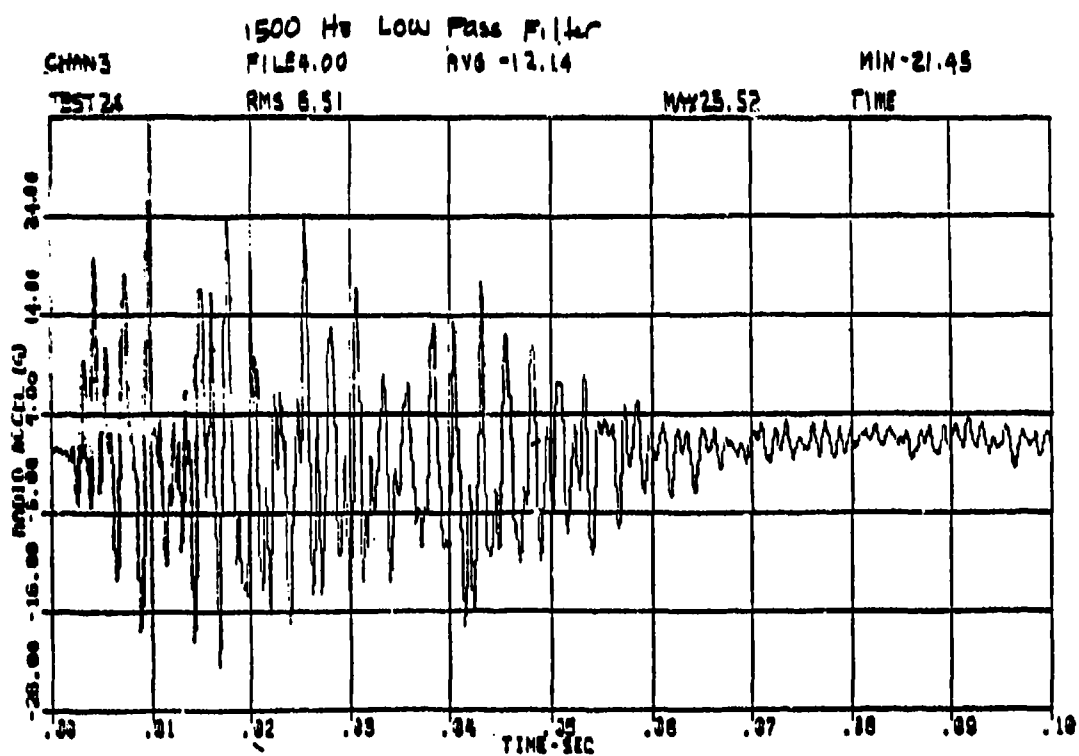
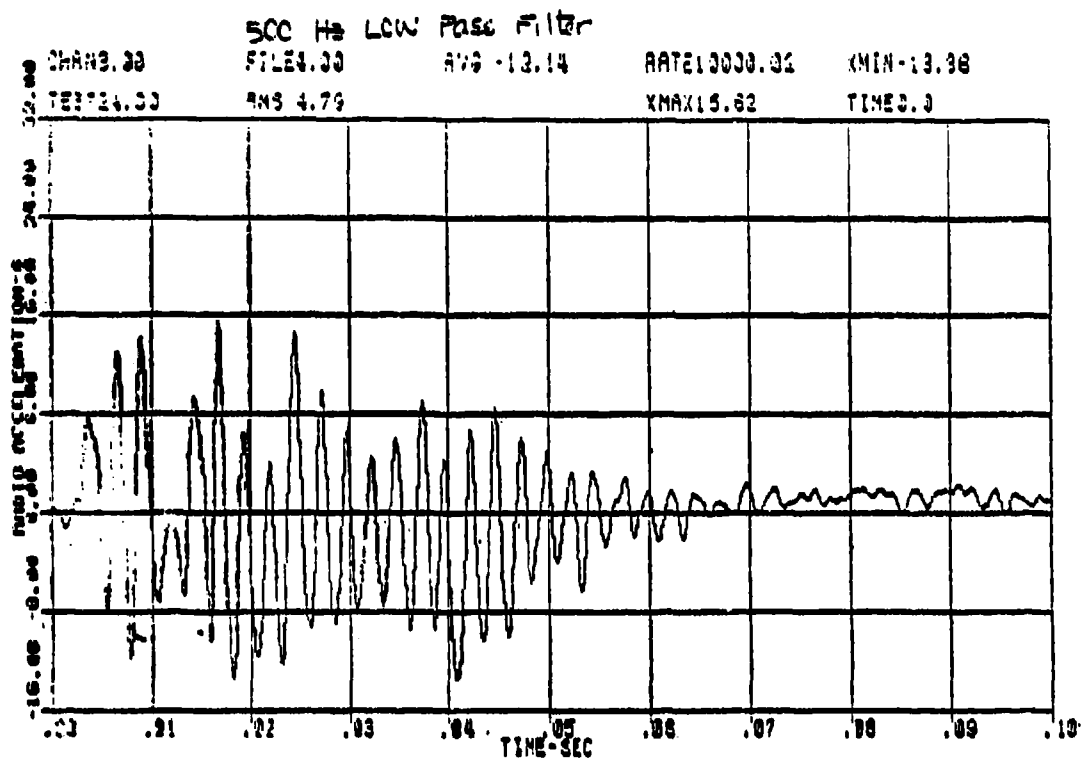
1500 Hz Low Pass Filter





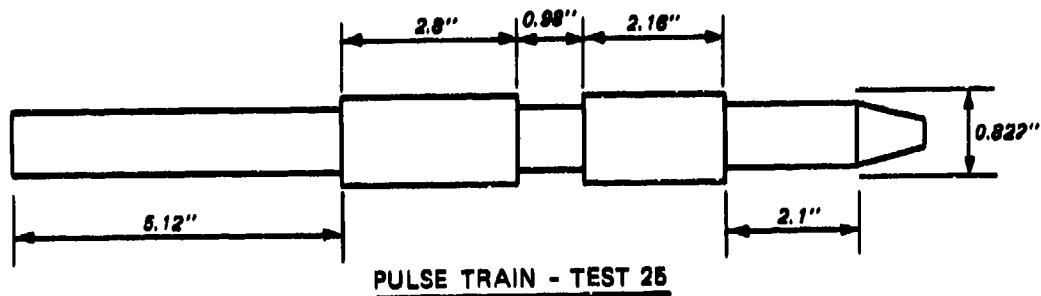




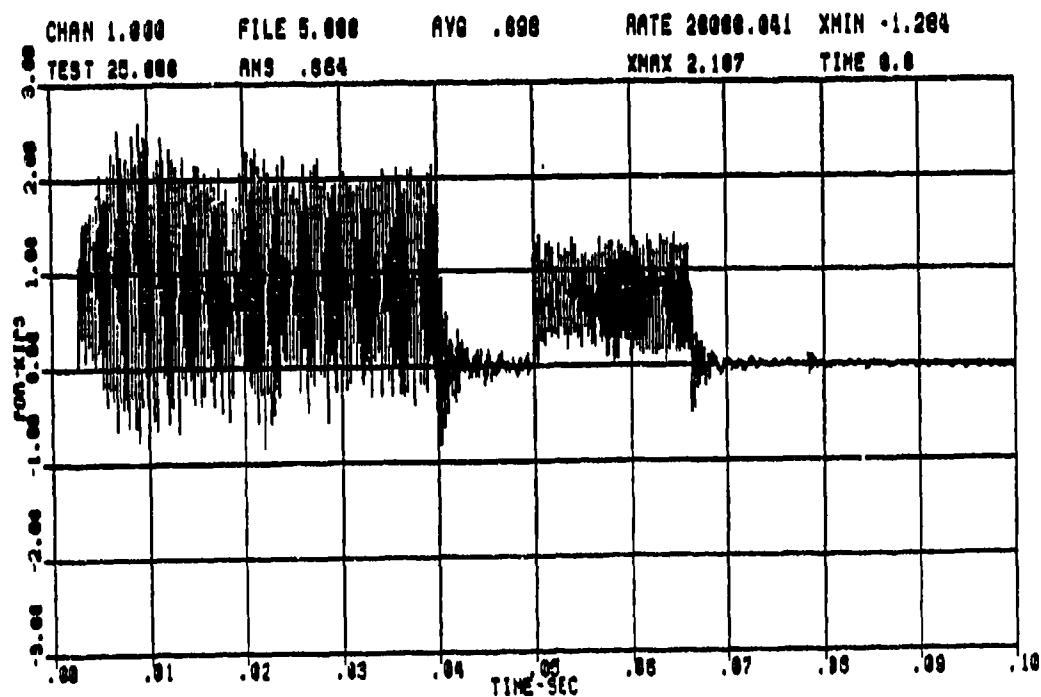
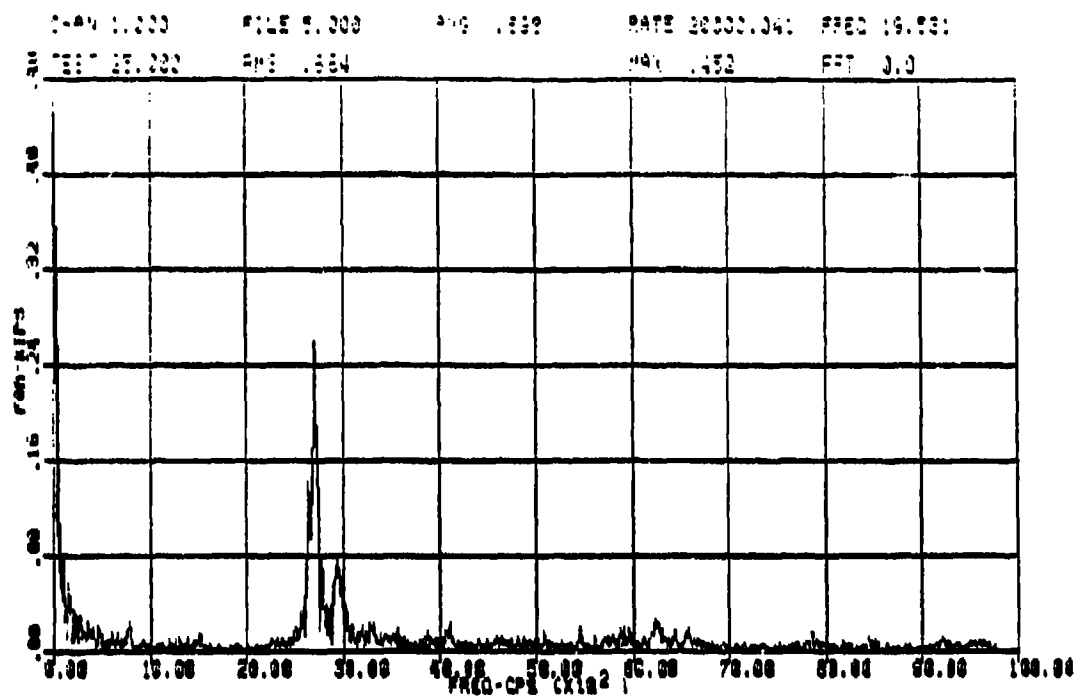


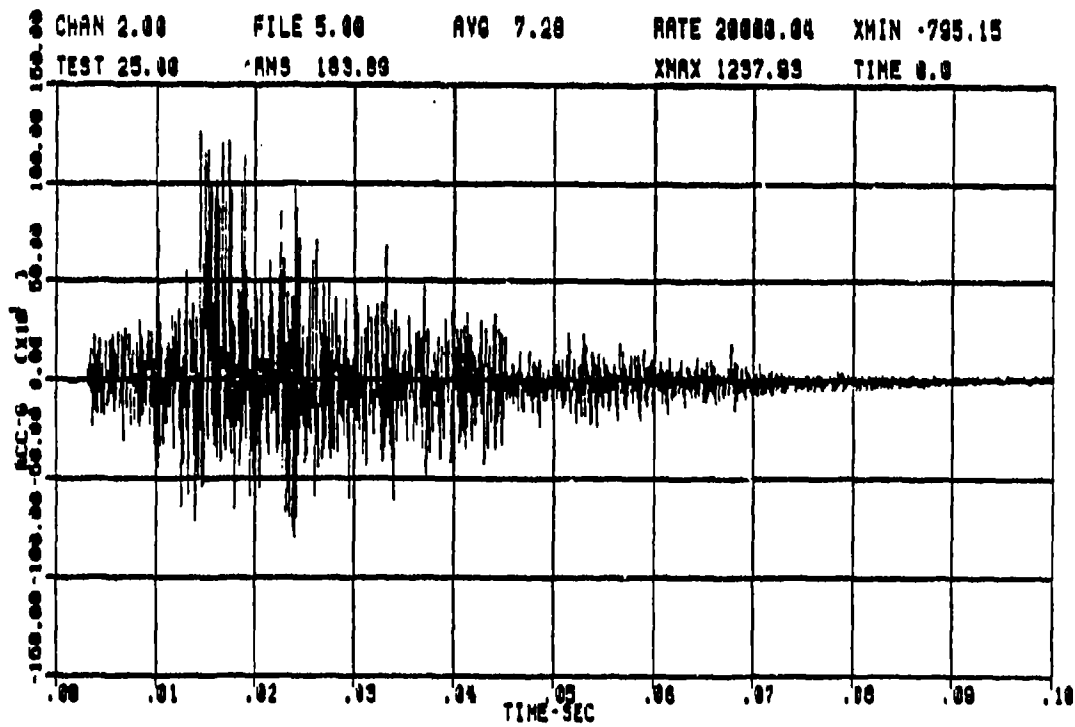
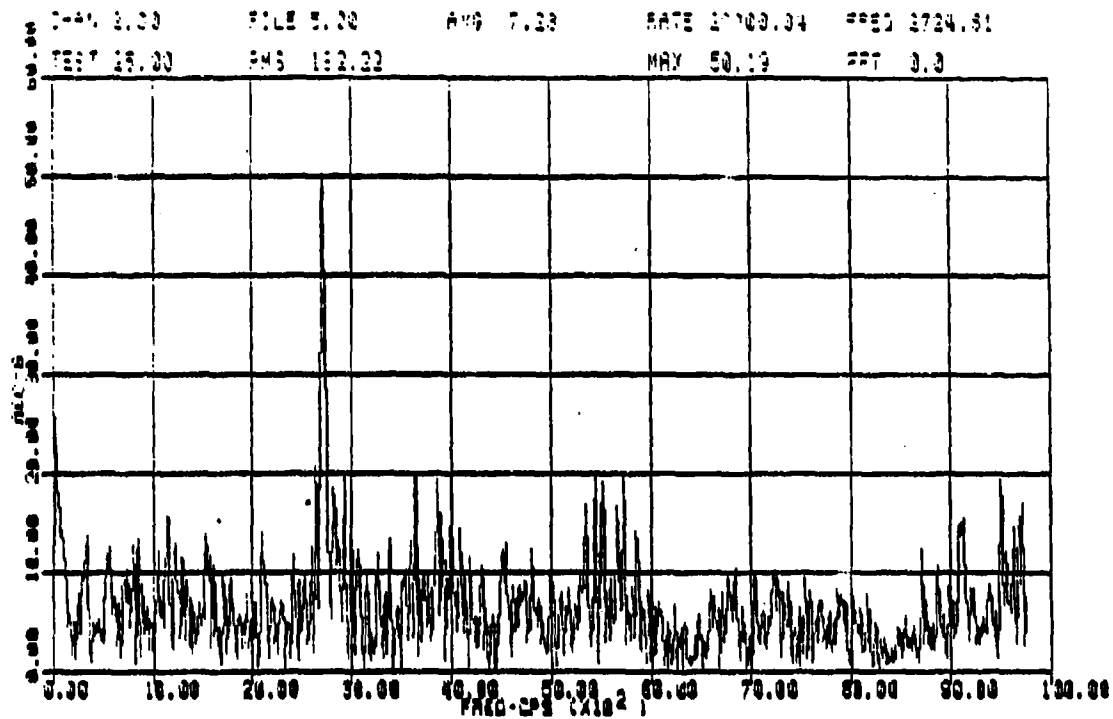
APPENDIX K: TEST 25 RESULTS

Test 25
Equipment Rack Soft-Mounted
AN/GRC-103 in Rack, Off-Line

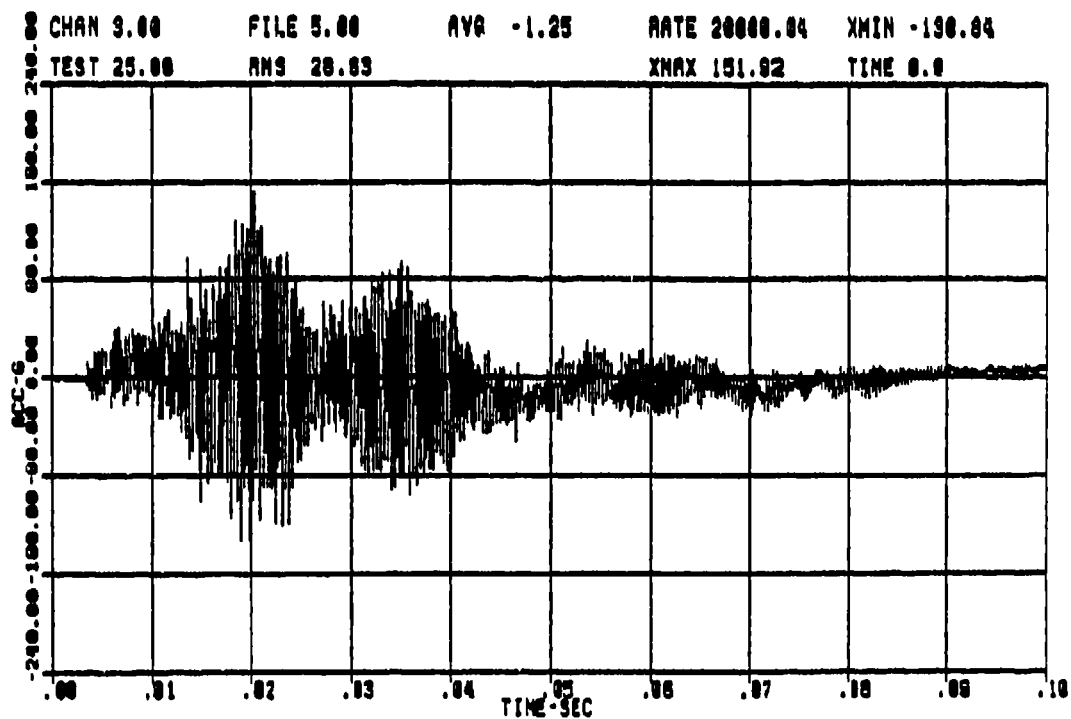
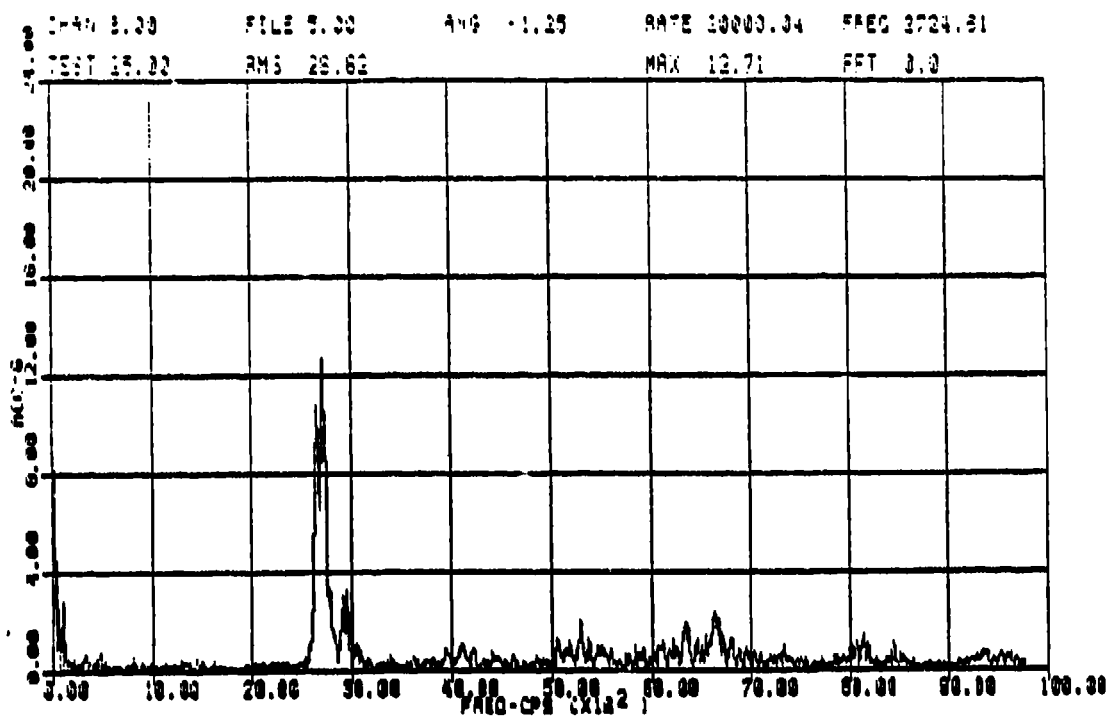


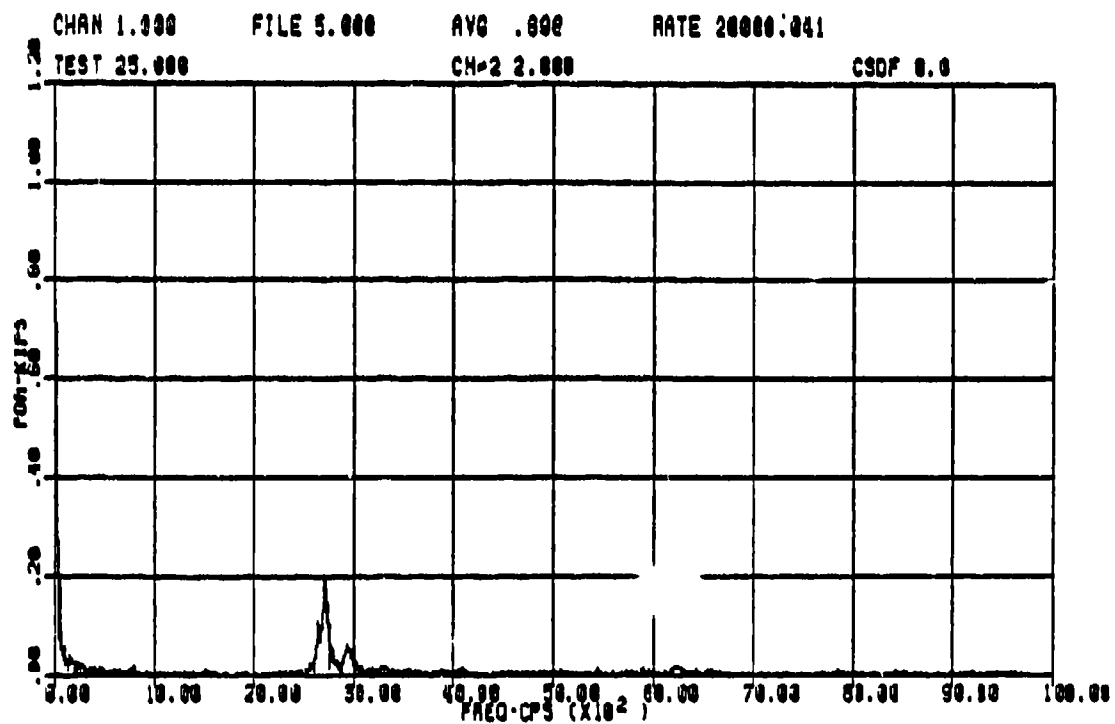
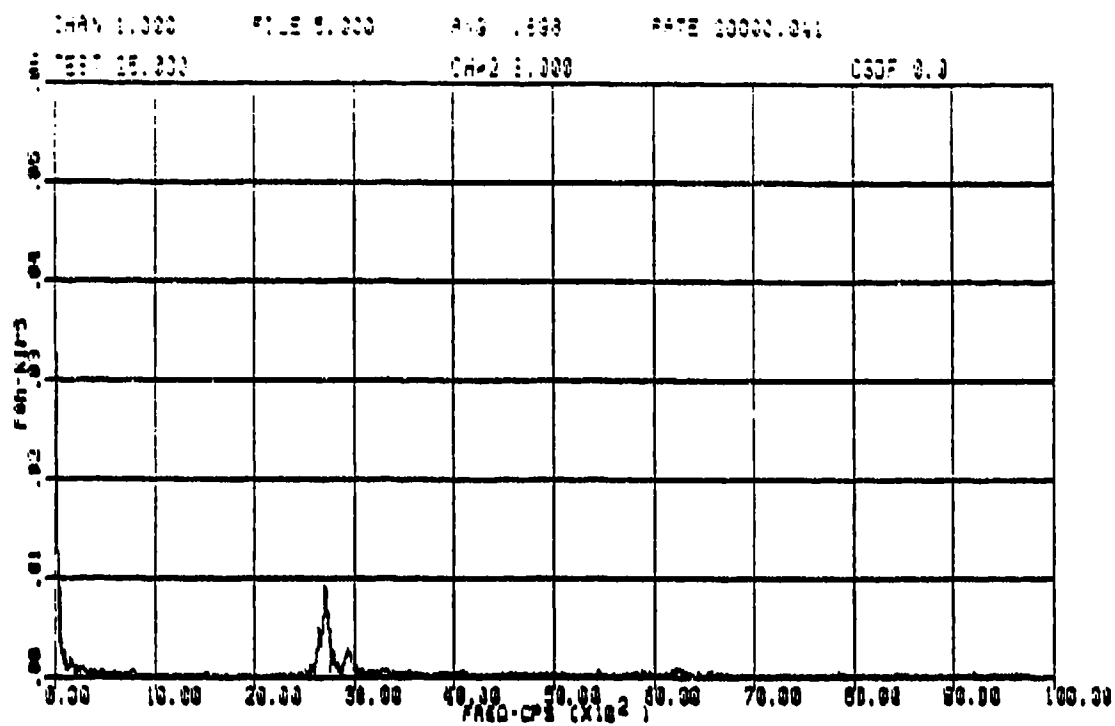
PRECHARGE PRESSURE = 1250 PSI
SYSTEM PRESSURE = 2000 PSI
FLOW CONTROL #8%
AIR BAG PRESSURE = 50 PSI

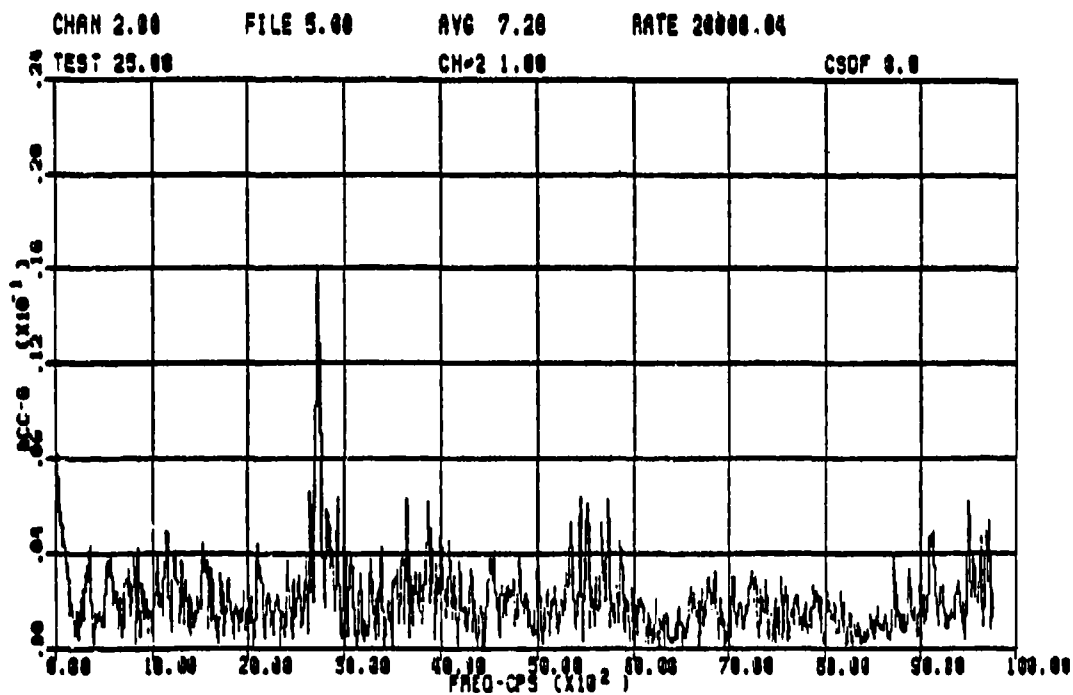
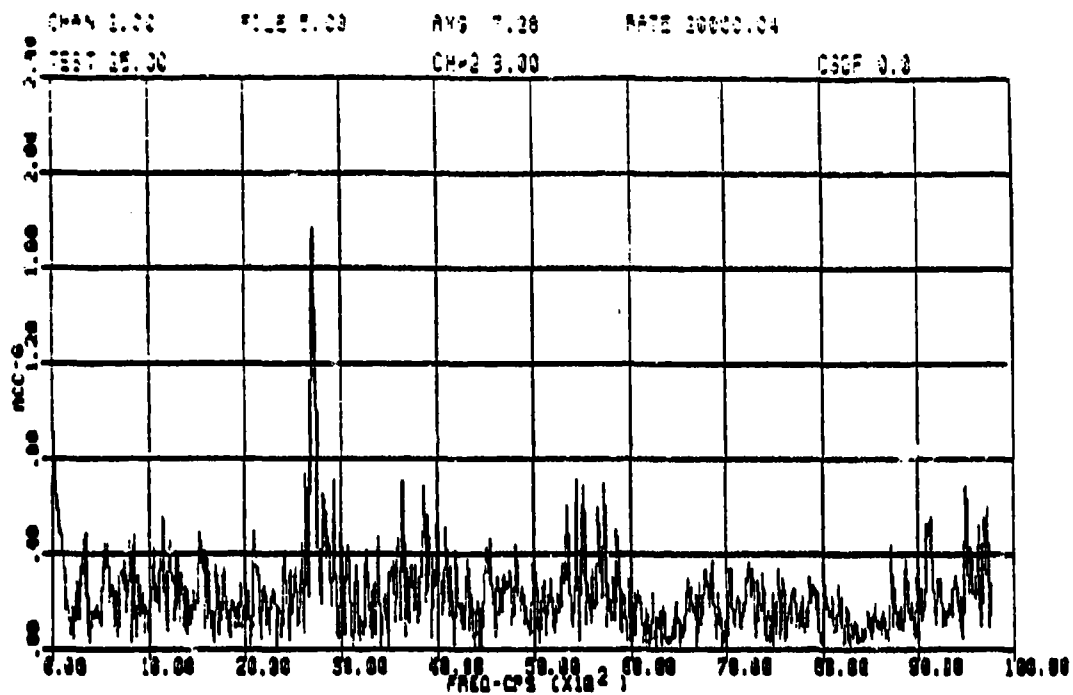


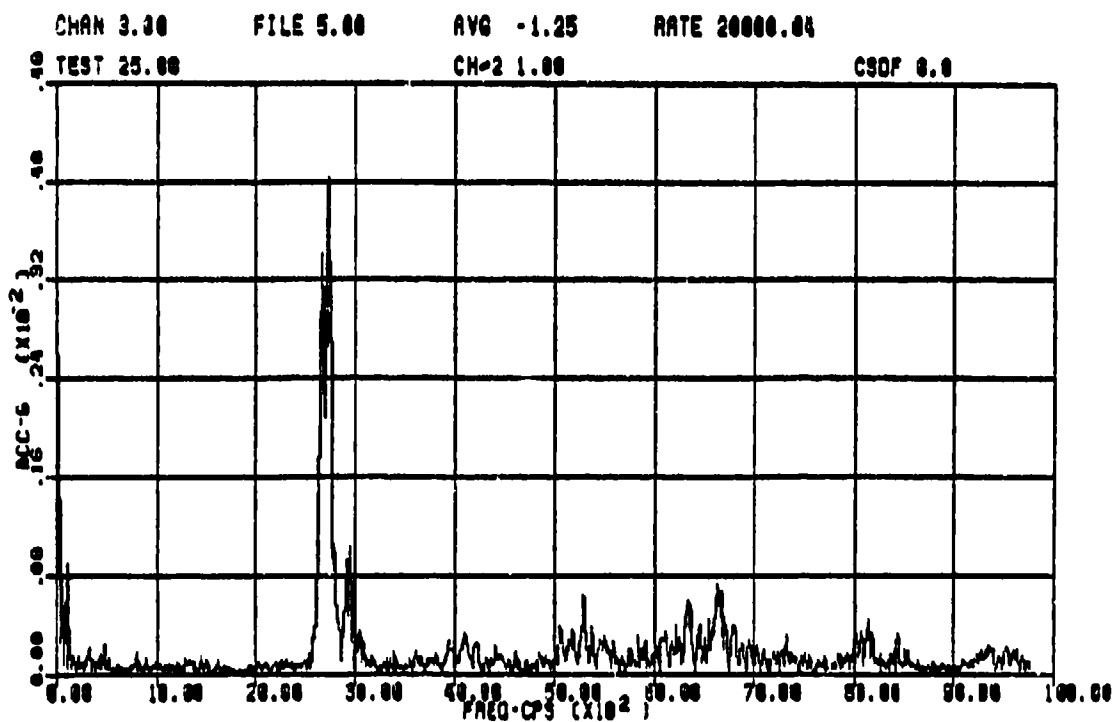
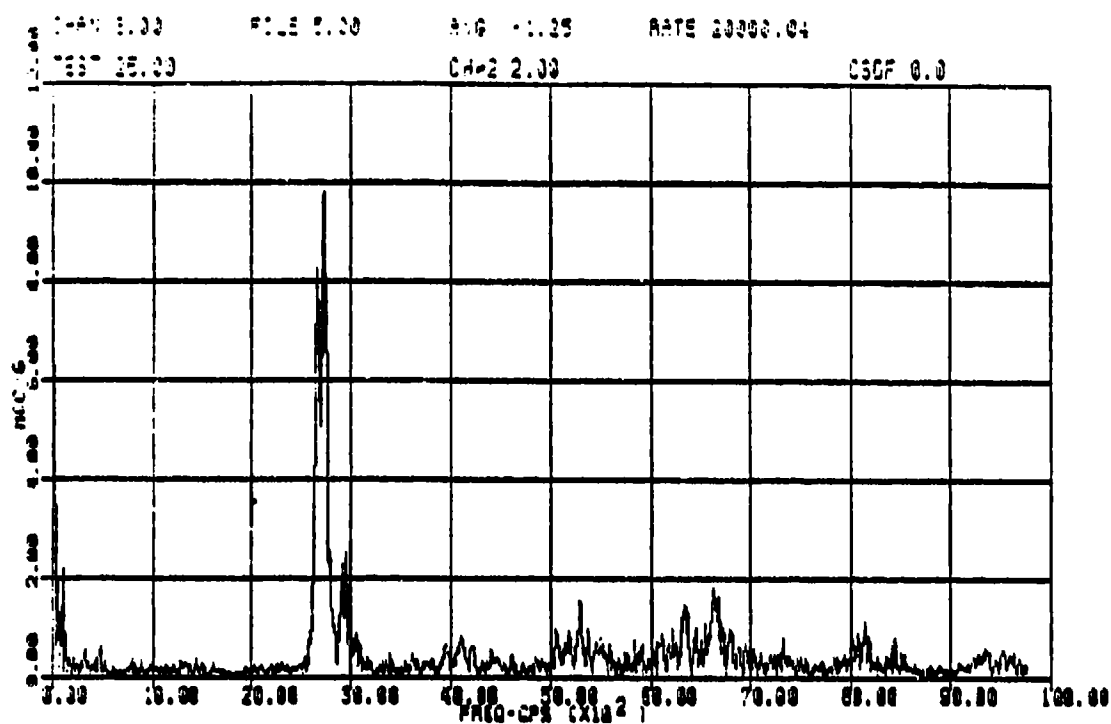


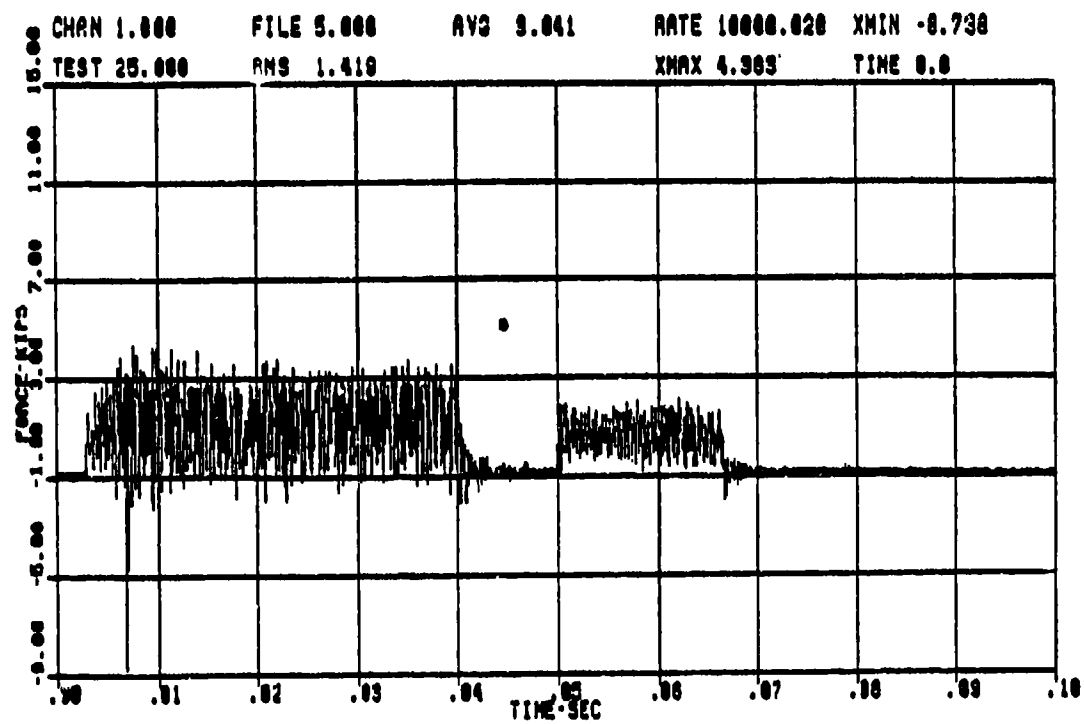
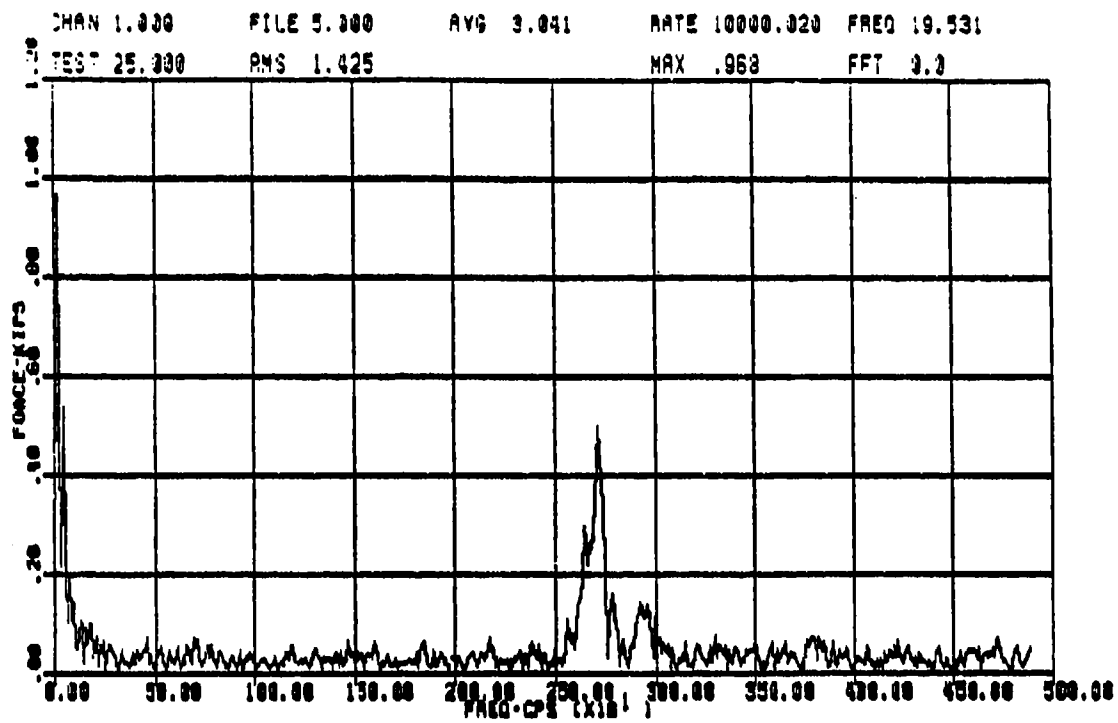
K3



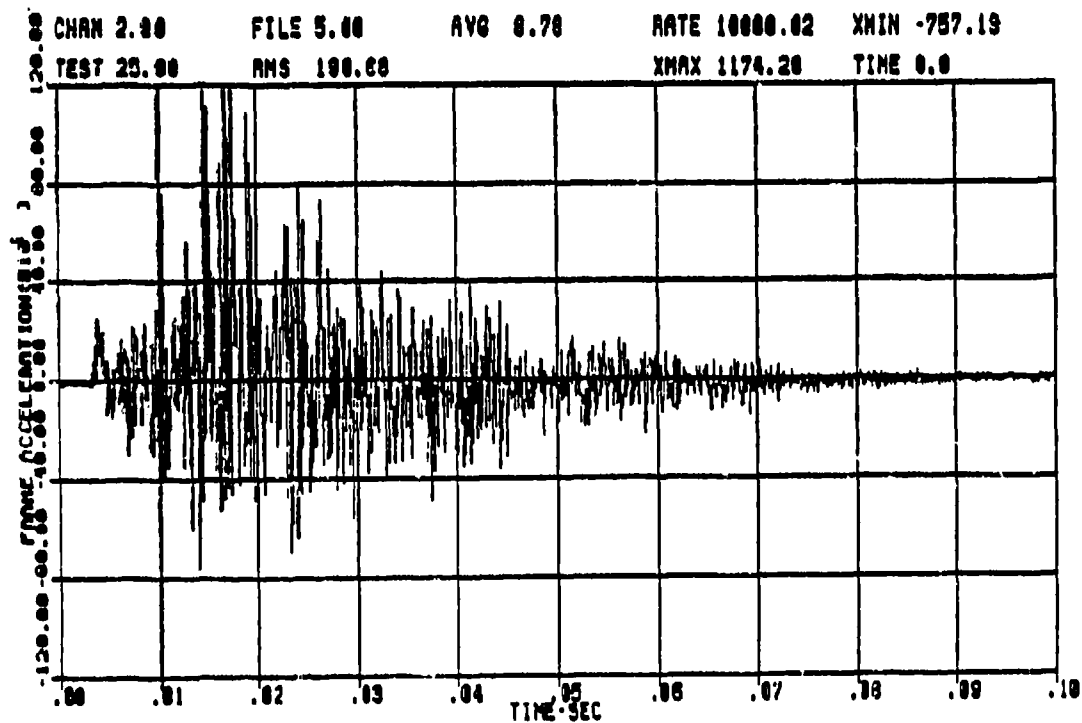
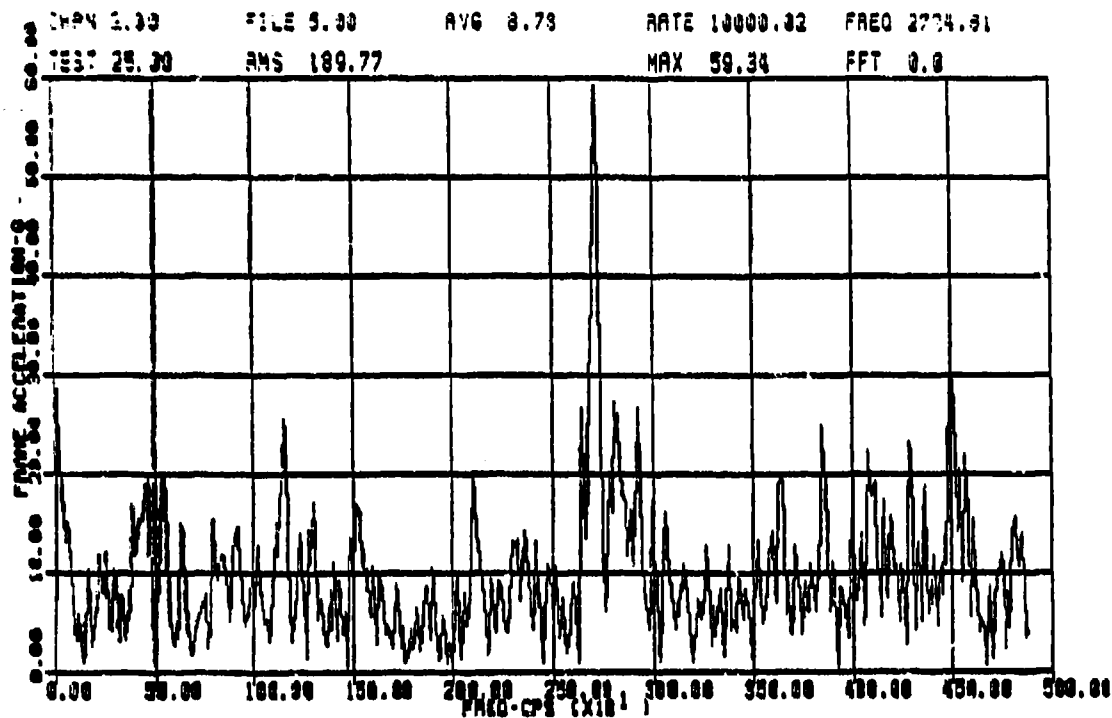


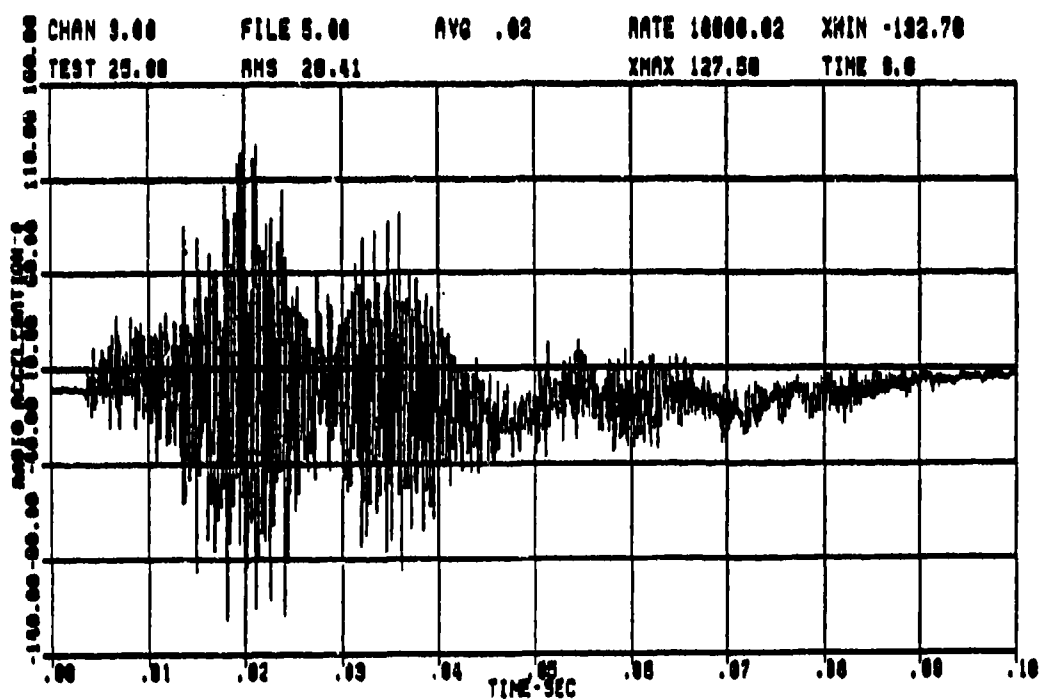
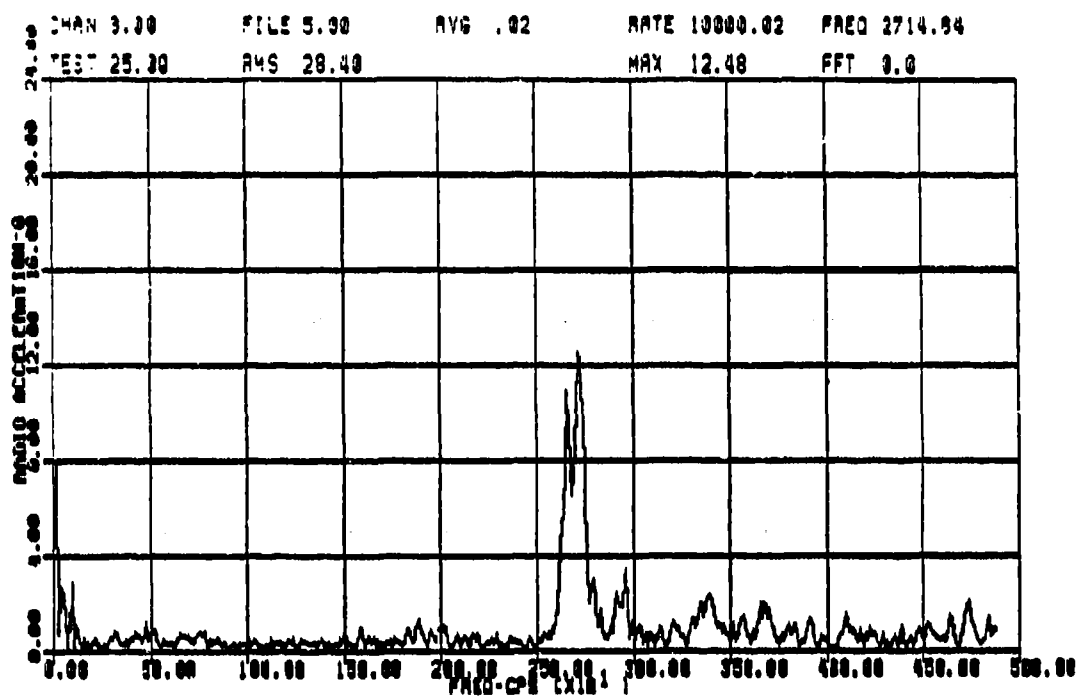




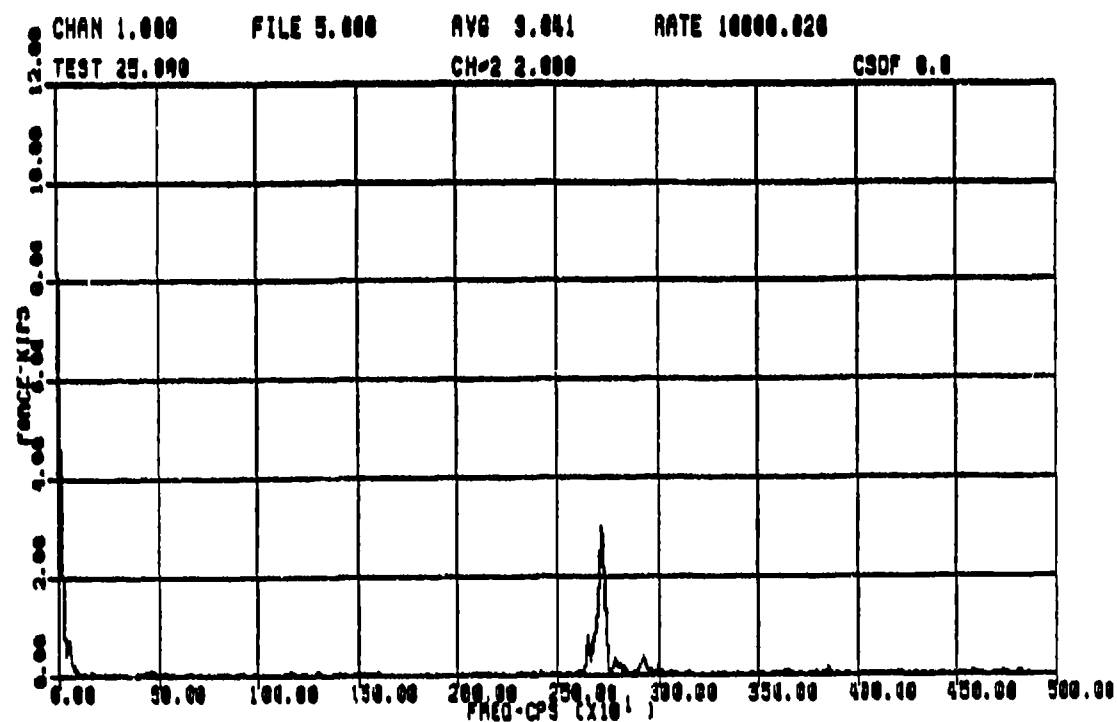
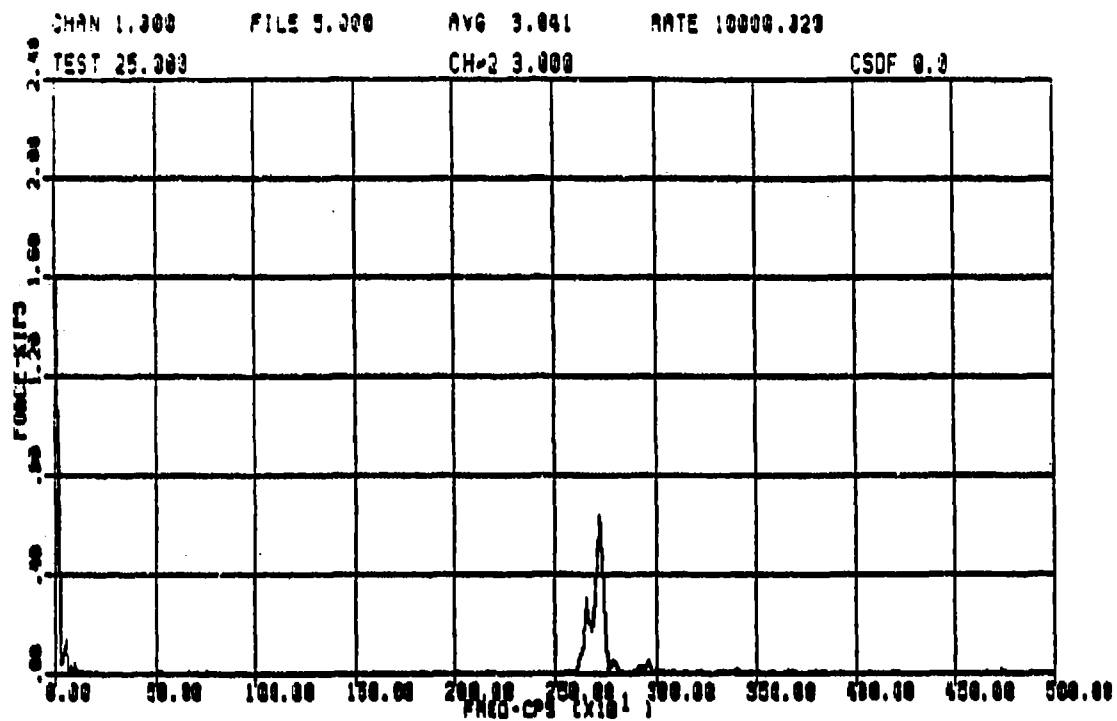


K8

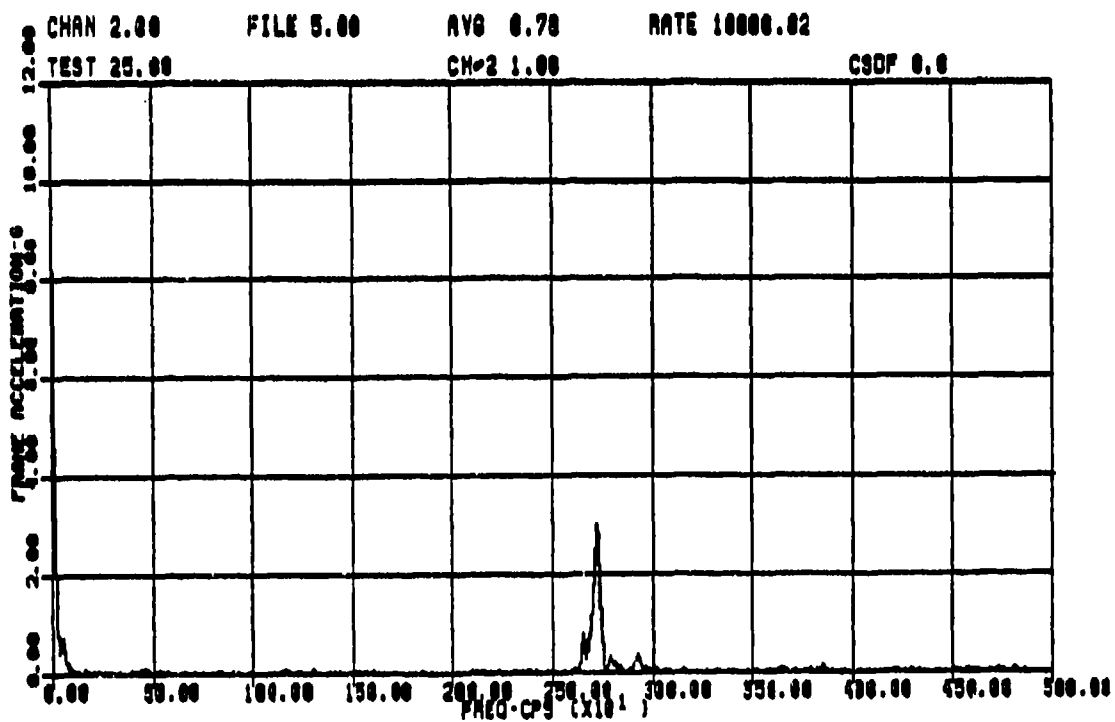
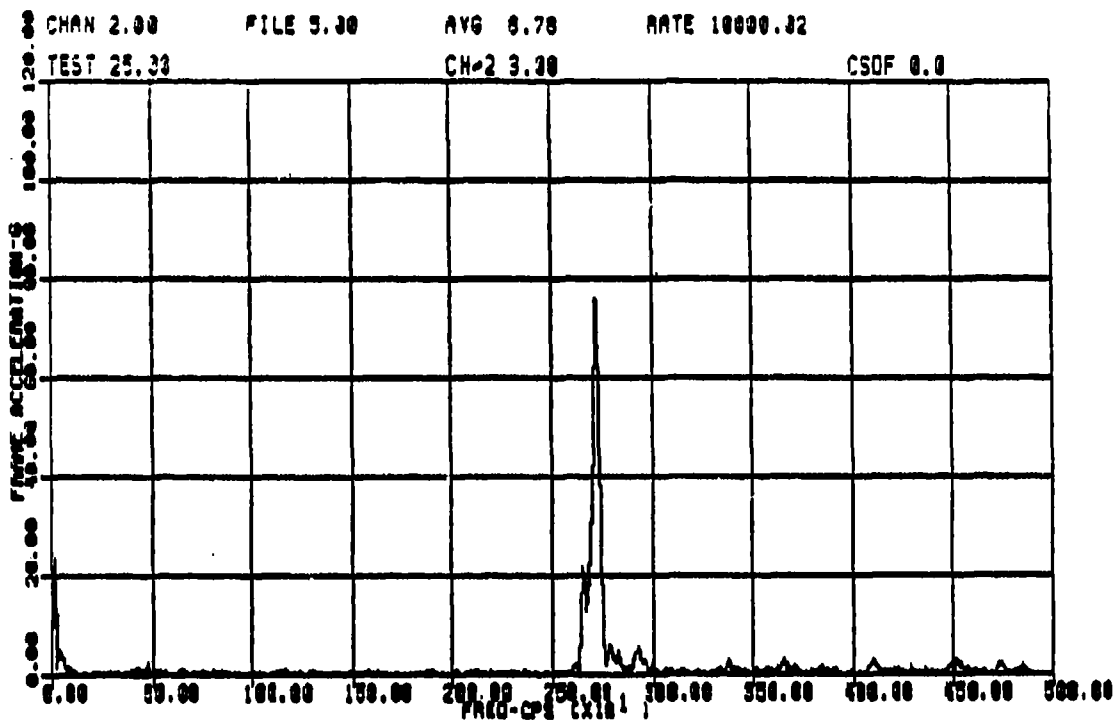




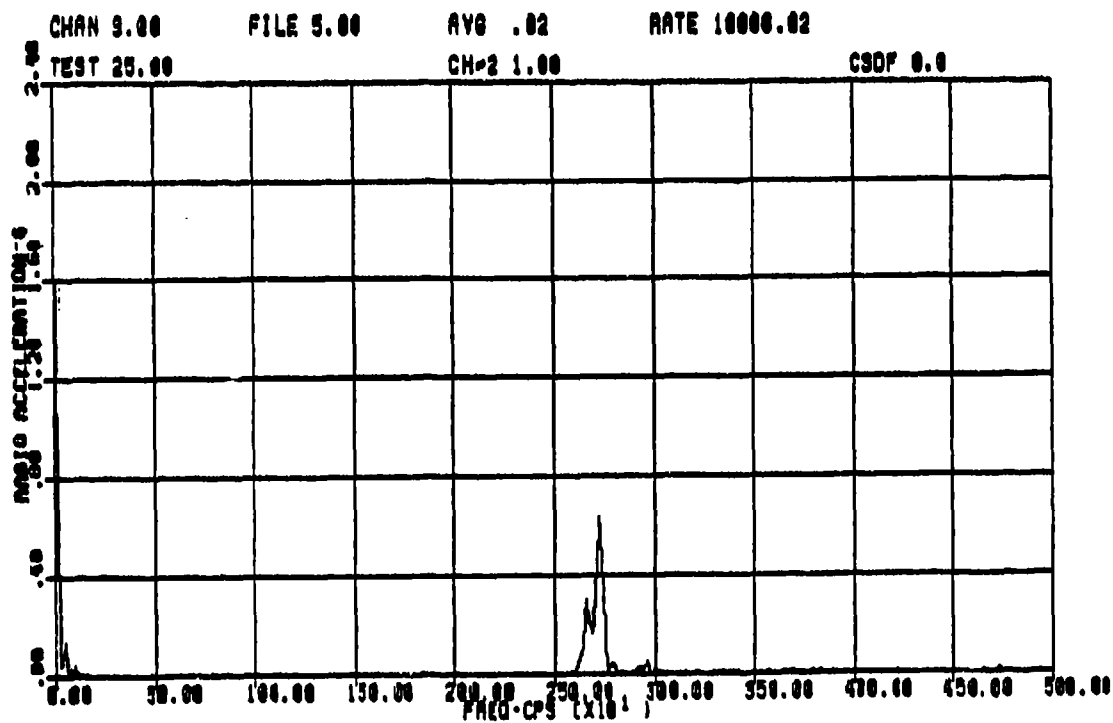
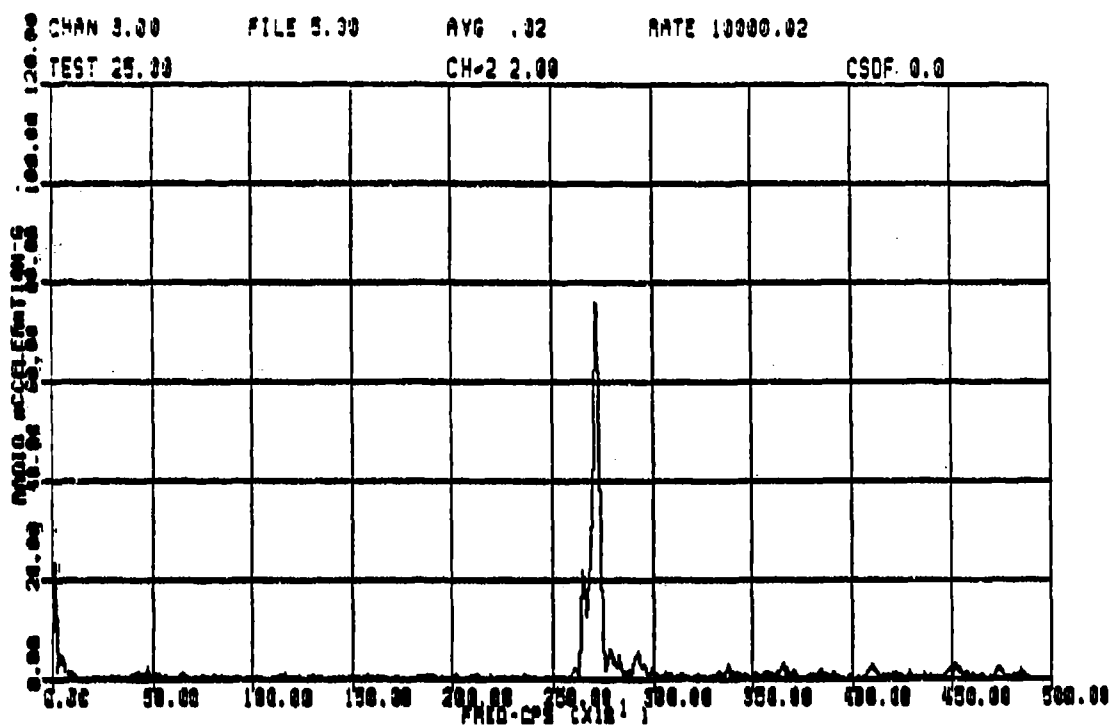
K10



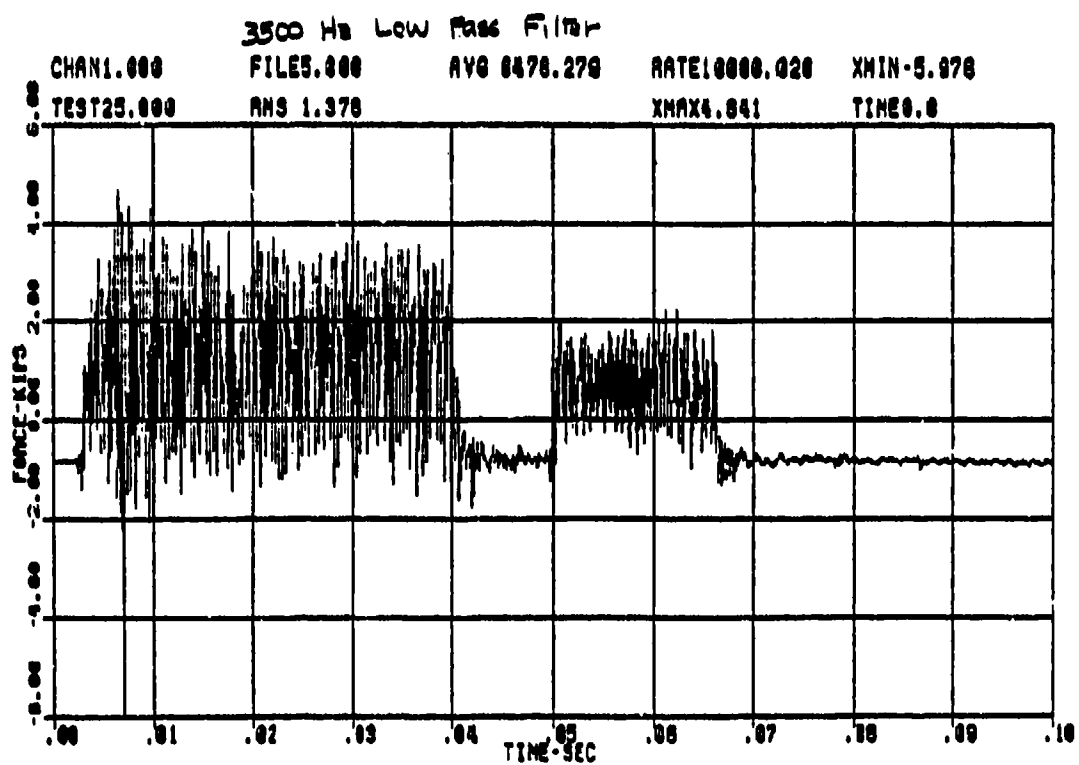
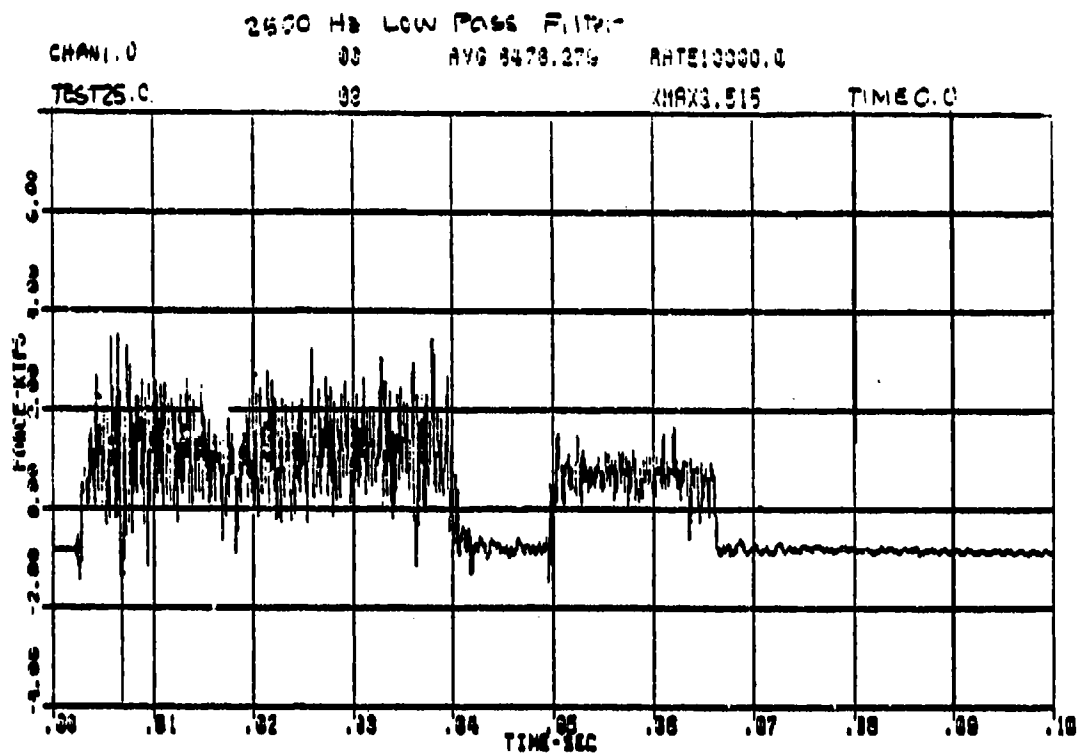
K11



K12



K13



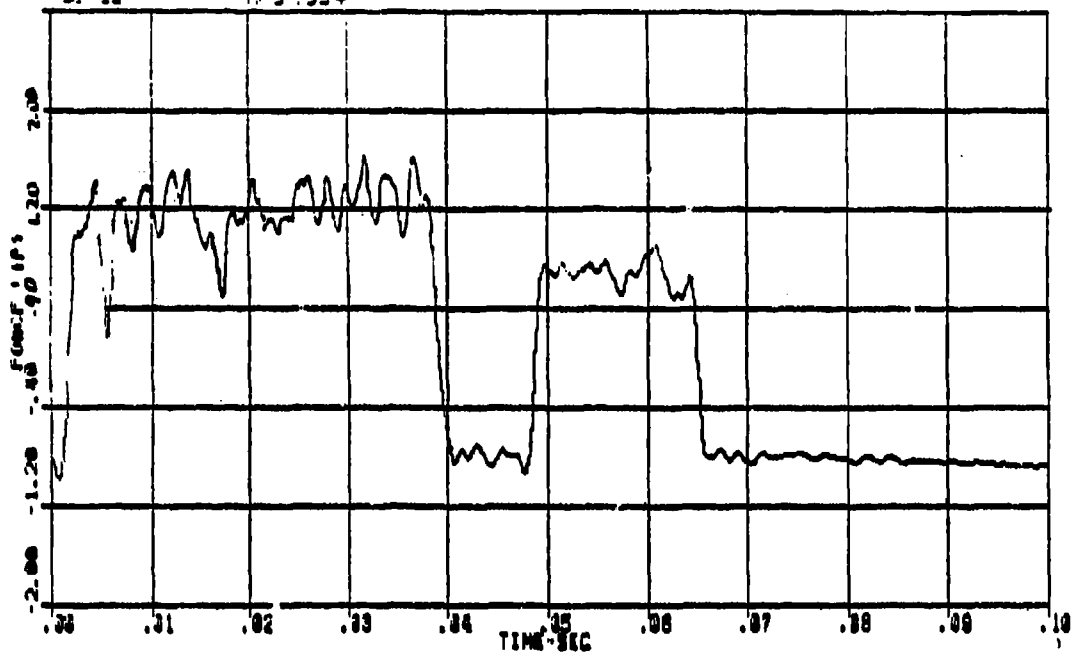
500 Hz Low Pass Filter

0-20.0

AVG 6-73.375

TEST 15

RMS .954



1500 Hz Low Pass Filter

CHAN1.000

FILE5.000

AVG 6478.279

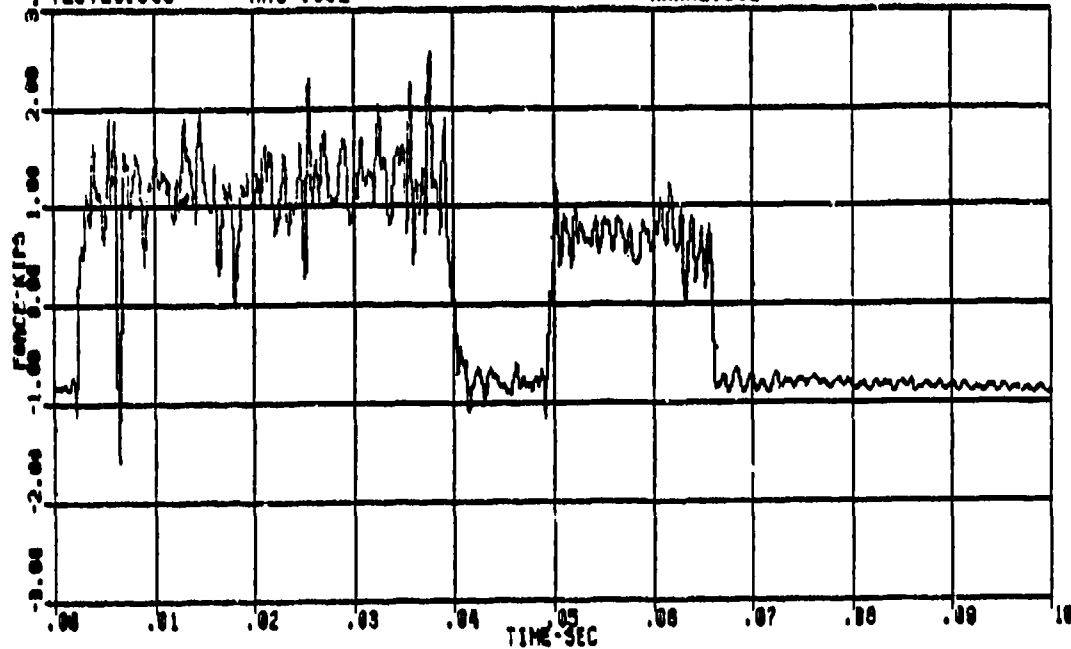
RATE10000.020. XMIN-1.579

TEST25.000

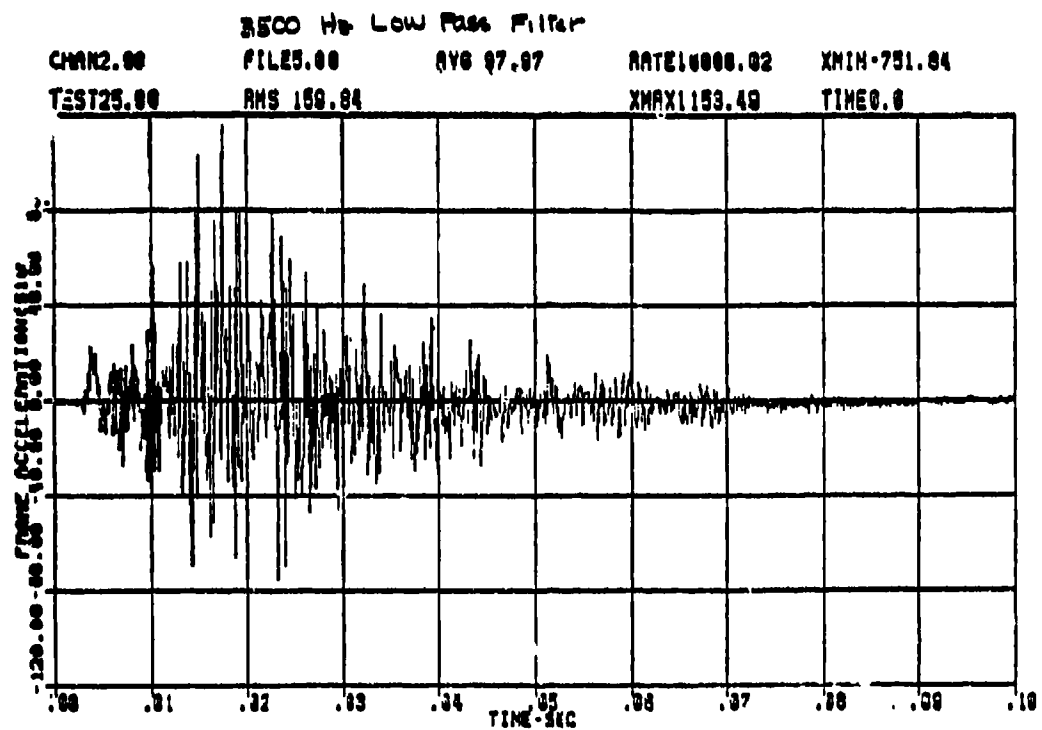
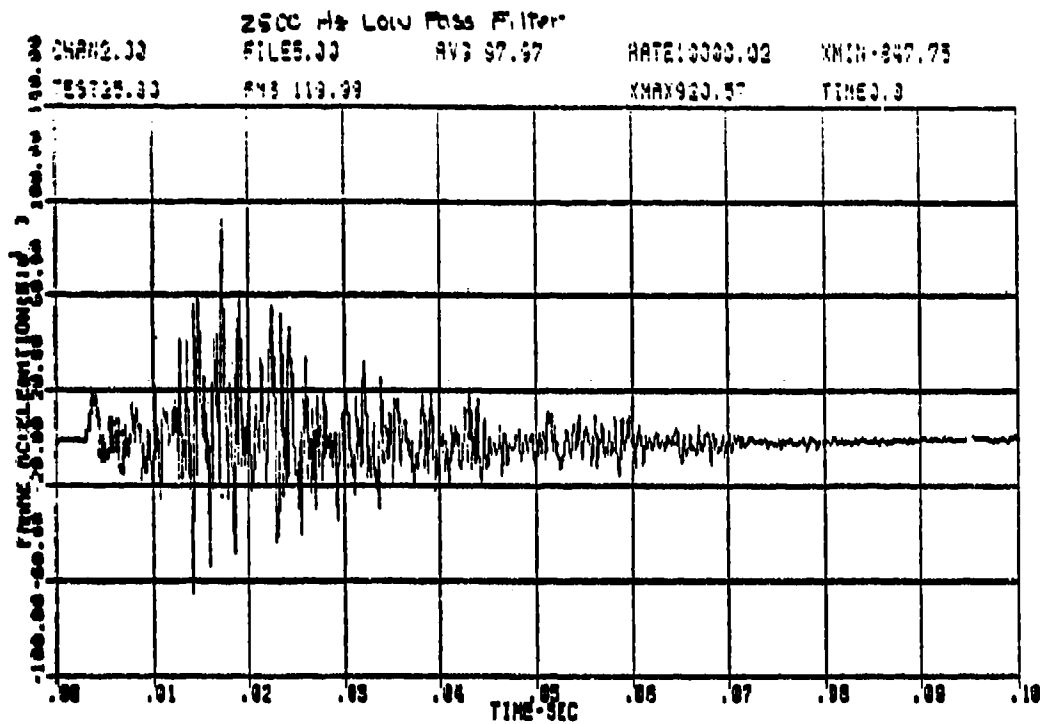
RMS .982

XMAX2.552

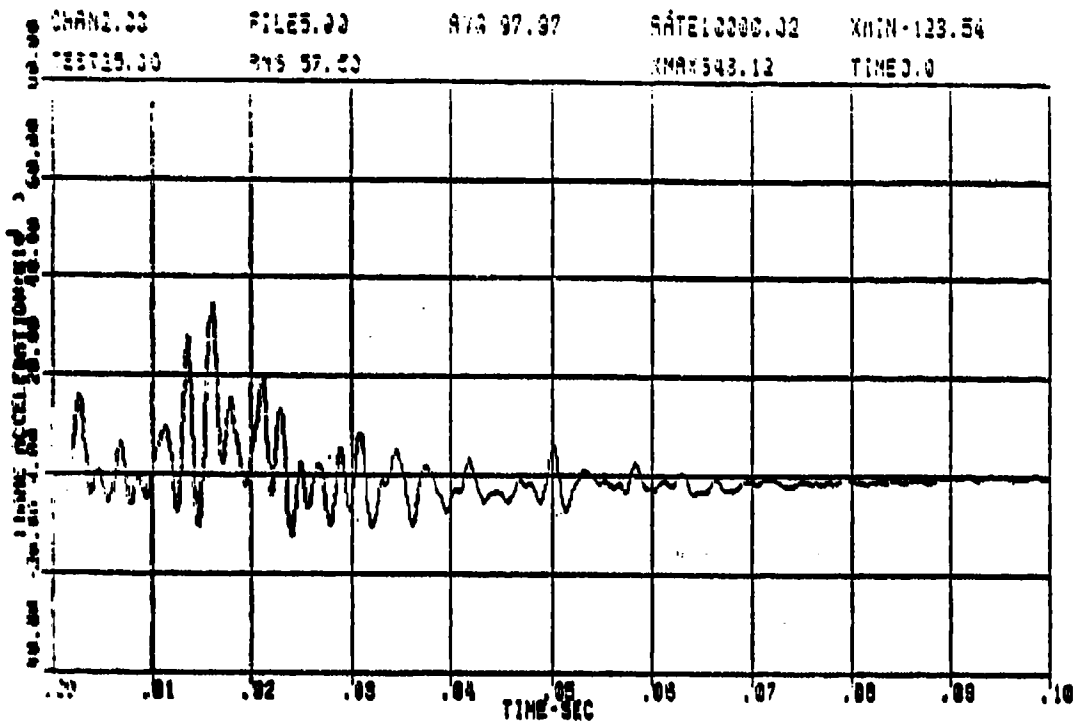
TIME0.0



K15



500 Hz Low Pass Filter



1500 Hz Low Pass Filter

